Master Thesis

Using chemical composition and grain size distribution of a palaeochannel-fill to identify Lower Rhine flood events and their origin in the catchment

Jochem Ypma BSc

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Dept. Physical Geography Utrecht University

> Supervision: Dr. M. van der Perk Dr. K.M. Cohen Dr. W.H.J. Toonen

Abstract

At this moment no long-term records are available that reveal the upstream origin of sediment deposited during flood events in the Rhine. Tracing flood deposits in the lower Rhine back to Rhine subcatchments would increase the ability to trace sources of pollution, of flood events, and to reconstruct geomorphological developments throughout the catchment. In this research a data set of fluvial deposits throughout the Rhine catchment was created, covering both the Lower Rhine, the Oberrhein and three main tributaries (Neckar, Main and Moselle rivers). The data set was built up by corings from the lower Rhine and its upstream subcatchments and surface samples from locations throughout the subcatchments. Grain size analysis was performed on these samples to identify flood events. A XRF scan was performed to obtain the chemical composition of the samples. Chemical composition data was used to investigate the distribution and propagation of trace elements. Grain size data and chemical composition data were combined to find a correlation between specific set of elements and grain size fractions. Based on data analysis combined with previous research, the Zr/Rb ratio was found to correlate with the sand fraction of the grain size data, and thus to act as a proxy for flood events. The Zr/Rb ratio was used to identify flood events in the chemical composition data, and to characterize the chemical composition of these flood events. The chemical composition of the corings and surface samples from the subcatchments were used to characterize the chemical composition of the subcatchments. Based on a combination of these characteristics an origin was suggested for some of the flood events. The 1671 and 1682 flood events are likely originate from the Oberrhein area. The 1726 and 1729 flood events are likely to originate from the Moselle area.

List of figures

Figure 2-1 Overview of the study area	10
Figure 4-1 Overview of the Rhine River catchment	18
Figure 4-2 Location of coring site along the Lower Rhine: Bienener Altrhein (Bienen)	19
Figure 4-3 Location of coring site along the Upper Rhine: Römerberg	20
Figure 4-4 Location of coring site along Neckar: Lauffen	21
Figure 4-5 Location of coring sites along Main: Sindlingen and Klein Krotzenburg	22
Figure 4-6 Location of coring site along Moselle: Kenn.	23
Figure 6-1 Depth plots of Bienener Altrhein core segments 3-10.	34
Figure 6-2 Basic correlation plots of Bienen 3	38
Figure 6-3 Basic correlation plots of Bienen 4	39
Figure 6-4 Basic correlation plots of Bienen 5	40
Figure 6-5 Basic correlation plots of Bienen 6	41
Figure 6-6 Basic correlation plots of Bienen 7	42
Figure 6-7 Basic correlation plots of Bienen 8	43
Figure 6-8 Basic correlation plots of Bienen 9	44
Figure 6-9 Basic correlation plots of Bienen 10	45
Figure 6-11 Correlation matrices for the Bienen cores	47
Figure 6-10 Graphs of the Zr and Rb counts	48
Figure 6-12 Element occurrence versus Rhine kilometers	50

List of Tables

Table 4-1 Overview of the sampling sites (corings)	25
Table 4-2 Overview of the samping sites (surface samples)	25
Table 6-1 Correlation of extreme flood events.	36
Table 6-2 Correlation matrix for Bienen 3. Original and shifted data	38
Table 6-3 Correlation matrix for Bienen 4	39
Table 6-4 Correlation matrix for Bienen 5. Original, shifted and upper part data	40
Table 6-5 Correlation matrix for Bienen 6	41
Table 6-6 Correlation matrix for Bienen 7	42
Table 6-7 Correlation matrix for Bienen 8. Original and shifted data	43
Table 6-8 Correlation matrix for Bienen 9	44
Table 6-9 Correlation matrix for Bienen 10	45
Table 6-10 Correlation coefficients of Al with grain size (clay) classes.	48
Table 6-11 Occurrences of trace elements in subcatchments	51
Table 6-12 Selection of flood events	52
Table 6-13 Chemical composition of selected flood events	53
Table 6-14 Occurrence of trace elements in flood events	53

List of appendices

Appendix 1 (A-H) Raw data from grain size and XRF scans (sorted by segment)	. 63
Appendix 2 Normalized counts of selected elements	. 63
Appendix 3 Sampling locations	. 63
Appendix 4 Handheld XRF elemental counts	. 63
Appendix 5 Normalized and standardized data for subcatchment cores	. 63
Appendix 6 Al standardization Bienen Cores	. 63
Appendix 7 Flood event data	. 63
Appendix 8 Correlation of grain size with Zr/Rb ratio (Bienen)	. 63
Appendix 9 Correlation of grain size with Zr/Rb ratio (Subcatchments)	. 63
Appendix 10 Standardized elemental data Bienen	. 63
Appendix 11 XRF settings	. 63
Appendix 12 Geological map of the Rhine catchment	. 64
Appendix 13 Distributive regions of the Rhine catchment	. 65

Table of contents

Ał	ostract		2		
1.	l. Introduction7				
2.	Stu	dy area	10		
	2.1.	The Rhine River	10		
	2.2.	Lower Rhine	11		
	2.3.	Subcatchments			
3.	Fac	tors controlling sediment deposition and composition in the Rhine River			
	3.1.	Flood events			
	3.2.	Sediment deposition			
	3.3.	Sediment composition			
4.	Fiel	dwork and core collection	17		
	4.1.	Site selection	17		
	4.2.	Sampling sites			
	4.3.	Sample collection	23		
5.	Lab	oratory methods and data analysis			
	5.1.	Laboratory methods			
	5.2.	Data Analysis	29		
6.	Res	ults and discussion			
	6.1.	Identification of flood events			
	6.2.	Correlating grain size and chemical composition data			
	6.3.	Correction of clay content			
	6.4.	Fingerprinting upstream catchments			
	6.5.	Tracing flood origin	52		
_					
7.	Cor	clusions and recommendations	55		
7. Ac	Cor knowl	clusions and recommendations	55 58		
7. Ac Re	Cor knowle ferenc	edgements es	55 58 59		

1. Introduction

Discharge records of the Rhine River in the Netherlands and upstream locations go back to 1900 A.D. and before. Descriptions of recent flooding (Disse & Engel, 2001) and historical records (e.g. Buisman, 2000) indicate that the origin of lower Rhine floods is highly variable, with both the High Rhine and the Middle Rhine producing peak discharges. For flood risk assessments it is important to understand the origin of flood pulses, generated throughout the catchment, because this would increase the ability to identify important regions for pollution. It has been suggested that floods in catchments affected by pollution result in the remobilization of contaminated sediment (Foulds et al., 2014). This poses a significant threat for ecology and agriculture along the floodplains. By analyzing (postindustrial revolution) deposits in up- and downstream locations along the Rhine River, pollution propagation throughout the catchment can be monitored, sources of pollution can be traced, and subsequently measures can be taken. Allocating the origin of floods is also of great social importance; resulting information can be used to research flood genesis and source areas in past and present situations. This information can be used to develop a system that predicts the peak discharge of flood events in the Lower Rhine. Moreover these data can be used to determine the most beneficial location to construction local flood reservoirs to intercept peak discharges in both downstream and upstream parts of the catchment. Besides of the above-mentioned applications, the unraveling of the origin of palaeo-floods can also be used; in the reconstruction of (long term) geomorphologic developments, research in flood sensitivity to changing land use, climate research, and in (more accurate) flood risk predictions.

A complex set of factors, including upstream geology, a large-scale catchment, varying flood parameters (discharge, duration) and floodplain storage, determine the chemical composition of flood deposits deposited along the Lower Rhine. The Upper Rhine from the Alpine region, and three main tributaries to the Middle Rhine, the Neckar, Main and Moselle Rivers, mainly determine the chemical composition of sediment transported and deposited by the downstream Rhine River. The relative discharge and sediment contribution of these tributaries during a flood event is thought to determine the chemical composition of the sediments deposited during the same flood event in the Lower Rhine region. Middelkoop (1997; 2002) found that there is a close relation between the amount of sediment transported and deposited, and the discharge and durance of a flood event; the higher the discharge, the more sediment can be transported. Previous research also indicates that the variation in grain size of flood event deposits can be used to identify single flood event layers (Middelkoop et al., 2010; Toonen et al., 2012). Other studies have correlated Lower Rhine flood event layers with historical flood events by making use of historical records (e.g. Winkels, 2011;

Aloserij, 2013; Toonen, 2013). Previous research conclude that chemical composition data can be used to acquire grain size information (e.g. Dypvyk and Harris, 2001). The use of such a geochemical proxy in small scale catchments has shown that the chemical composition of flood layers can be used to trace the upstream origin of sediment by making use of the characteristic chemical composition of tributary rivers (E.g. Passmore and Macklin, 1994; Jones et al., 2009). The same methods have, at this moment not been tested in large river systems with a complex catchment configuration and with considerable mixing of sediments (also with temporarily stored floodplain deposits (e.g. Erkens, 2009)), which may complicate traditional fingerprinting of upstream catchments. No study has yet combined these approaches and applied these on a large catchment, such as that of the Rhine River.

The main goal of this study is to find out whether we can use the relation between the grain size and the chemical composition of floodplain deposits to identify flood events and to trace Lower Rhine River flood events back to upstream Rhine subcatchments. The first objective of this study is the creation of an inventory of flood deposits found in cores from upstream and downstream locations in the Rhine catchment. To enable a catchment-wide correlation, flooding events need to be identified in a sedimentary sequence (and dated) throughout the catchment by performing grain analysis (Winkels, 2011; Aloserij, 2013; Toonen, 2013). The next objective is to find a chemical proxy that can be used to link grain size data with chemical composition data, and subsequently to identify flood events within the chemical composition data (Walling, 2005; Macklin et al., 2006). This chemical proxy will also be used to find a method to correct for the clay content in the flood deposits. The latter is needed to enable a catchment-wide comparison of cores. The next objective involves the construction of a series of fingerprints of each of the subcatchments, and a characterization of a series of flood events. Eventually, the aim is to unravel the contribution (quantitative or qualitative) of each of the subcatchment to the selected flood events.

To achieve our main goal, the following research questions are specified:

- Can flood events be identified in grain size data and chemical composition data?
- Can chemical composition data be corrected for clay content?
- Can a characteristic fingerprint be set up for individual Rhine subcatchments?
- Can the above-mentioned fingerprints be used to trace the (mixed) origin of Lower Rhine flood events?

To answer these questions we applied a series of sedimentary and statistical approaches. First an overview of the study area and its hydrologic background is provided in chapter 2. Here the local settings of the source areas are also described. Chapter 3 describes the processes that occur from the source area towards the deposition of sediment in the floodplains along the Lower Rhine. The local settings of flood depositions also are described here. Chapter 4 describes the process of core selection and present the sampling sites. Samples were collected from suitable locations in both the Lower Rhine (sedimentary sink) and the upstream subcatchments (sedimentary sources). Chapter 5 describes laboratory and analytical methods. Grain size distributions of flood layers and chemical composition data were analyzed and compared to distinguish flood layers and correlate these throughout the Rhine catchment. The latter involved a series of research steps, of which (preliminary) results are provided in the appendices.

2. Study area

2.1. The Rhine River

The Rhine River originates in the Swiss Alps where its headwaters confluence, at Lake Constance these form the Alpine Rhine or High Rhine (Fig 2-1). After the joining of the river Aare and crossing the Swiss-German national border, it is named the Upper Rhine. further downstream, the Rhine River confluences with several tributaries, of which the Neckar (at Mannheim) and the Main (at Mainz) are the most important (Fig. 2-1). In central Germany the Middle Rhine flows through the Rhenish Massif (Schiefergebirge) which is characterized by a narrow bed-rock canyon. At Koblenz the Middle Rhine is joined by the Moselle River. Downstream from Bonn the Rhine River is named the Lower Rhine. The apex of the Rhine delta is roughly located at the Dutch-German national border. A few kilometres downstream, the Rhine River splits into the Waal River and the Pannerdens Kanaal, Nederrijn, and Lek branches. At Arnhem, another distributary, the IJssel River, splits from the Nederrijn River (Fig. 2-1).



Figure 2-1 Overview of the study area.

Map of the course of the River Rhine, from the Swiss Alps to the North Sea. In blue the High Rhine (Hochrhein, including the Alpine Rhine), in green the Upper Rhine (Upper Rhine), in yellow the Middle Rhine (Mittelrhein, and in orange the Lower Rhine (Niederrhein) and deltaic distributaries.

The Rhine River drains approximately 185000 km2 of NW-Europe and its main river channel stretches ~1320 km (Middelkoop, 1997). Its hydrological regime varies from glacial in the upstream, to pluvial in the downstream parts of the catchment. At the Lower Rhine the mean annual discharge is 2200 m³/s. Most floodplains are inundated when discharge exceeds 6000 – 7000 m³/s while largest measured floods occurred in 1926 A.D. and 1995 A.D. with discharges of ~12000 m³/s (Middelkoop, 1997). Most peak discharges occur between December and April as a results of extensive snow melt and increased precipitation. Highest magnitudes of flood discharges in the Lower Rhine occur when flood pulses from the main tributaries enter the Rhine River simultaneously.

2.2. Lower Rhine

During the Holocene the Lower Rhine developed a meandering course. During the last ~3000 years the Lower Rhine has been transformed into the Rhine delta apex (Berendsen and Stouthamer, 2001). Throughout the Holocene several phases of fluvial activities have resulted in palaeo-channels and meander cut-offs of varying ages. These slack-water environments are located at lower lying areas in embanked floodplains and are characterized high sedimentation rates. Moreover, some dike breach ponds and cut-off channels are currently being filled in.

2.3. Subcatchments

Upper Rhine

In this report we use the name Upper Rhine for the part of the Rhine River upstream from the confluence with the Neckar. Main tributaries confluencing downstream from this point to form the Rhine River include the Neckar, Main and Moselle rivers (Figure 2-1). A large canalization project took place just after the start of the industrial revolution, during the period between 1820 and 1860 (Beeger, 1990; Herget et al, 2005).

The geology of the Upper Rhine region is characterized by the Jurassic source rocks of the Aare and Birs rivers and other tributaries in Switzerland. Both the Aare and the Birs provinces (Appendix 212) are formed by minerals from the Molasse foreland basin (Oligocenen/Miocene) and the Alps. Characterizing minerals are garnet, epidote (silicate of aluminium, iron and calcium), hornblende, staurolite and Rhine-alterites (Van Andel. 1958). The Black Forest-Vosges province, geologically characterized as granite and crystalline schists (Appendix 12) has several mineral associations of which the principles are garnet and hornblende. Furthermore, some typical minerals like augite, sillimanite and barite are found, these are derived from the rocks of the Black Forest (Eocene) and the Vosges mountains (Eocene).

Neckar

The Neckar drains a watershed of about 14.000 km² of South-west Germany. It originates in the Black Forest, in the Swabian scarplands. Nearby the city of Mannheim the Neckar confluences with the Upper Rhine (428 km). From here on downstream it is called the Rhine River. In the upstream part, south of Stuttgart, the drainage area of the Neckar is densely populated and highly industrialized. Then, after passing Stuttgart it meanders through a landscape built up of Triassic and Pleistocene limestones; an area built up of carbonates (Hantke, 1993). More mineral associations from the Neckar backland are monazite (phosphate mineral containing rare earth metals), from Bohemia, garnet (Triassic) and tourmalite, zirconium silicates and rutile (titanium), from the Bunter sandstone (Triassic) of the Zorn province (13) (Van Andel, 1950). Moreover, minerals from the volcanic rocks are also found in the south-eastern part of the Neckar catchment.

In 1976 Abadian and Lippman studied heavy metals in the Upper Neckar river to determine the amount of industrial pollution. XRF analysis was used to detect elements and corresponding minerals. The occurrence of brushite was said to be a mineralogical indicator of pollution. Phosphate, one of the components of brushite, is used in fertilizers, detergents, industrial waste waters and more (Abadian, 1976). Moreover, an important industrial signal can be found back in the abundance of Cadmium. Due to the metal working industry along the tributary Enz river, high amounts of Cadmium were emitted and deposited along the Neckar. Cadmium is bound with fine grained sediment. These heavy metals emissions depleted after the 1970's (Gerbersdorf et al, 2005).

Main

The Main confluences with the Rhine River near the city of Mainz (497 km). It originates from the German state of Bavaria, and before it meets the Rhine River, it flows through the industrial zone of Frankfurt am Main. The backland of the Main resembles that of the Neckar. It is also built up from Triassic and Pleistocene limestones. Specific mineral associations are monazite, garnet, tourmalite, zirconium silicates and rutile (titanium) from the Bunter sandstone (Triassic) of the Zorn province (Appendix 213) (Van Andel, 1950). In the Main region there might also be found some minerals from the eastern part of the catchment, these include augite, titanite (including rare earth metals), clinozoisite (calcium and aluminium) and (basaltic) hornblende (Van Andel 1950). These are all derived from the Bohemian, Keuper (Triassic) and Rhaetic (Triassic) massifs (Appendix 12). Moreover, aeolian deposits (loess) is found in this area which will be reflected in the chemical composition signal of the sediment coming from the Main river (Van Andel, 1950). Besides of that, there is the Staurolite province (Appendix 13), which supplies the Rhine and the Main with staurolites, derived from Mayence Basin (Oligocene).

Moselle

In contrast to the other tributaries, the Moselle originates in the area west of the Upper Rhine. It confluences with the Rhine River nearby Koblenz (592 km). The Moselle originates in a Tertiary and Mesozoic carbonate area, and flows through crystalline and Palaeozoïc rocks in the Vosges, where it encounters garnet, blue-green and brown hornblende (Van Andel, 1950). After that it flows through the Eifel and Hunsrück (Appendix 12) where it encounters quaternary volcanic rocks of the Rhenish Massif (Volcanic province, Appendix 13). This results in a signal of specific elements originating from volcanic minerals including augite, basaltic hornblende and titanite (Edel & Fluck, 1989; Van Andel, 1950). In the downstream part of the Moselle River, it is extremely incised into the Rhenish massive. As a result, the floodplains are small and narrow and there are no Holocene cut-off-meanders.

3. Factors controlling sediment deposition and composition in the Rhine River

3.1. Flood events

Patterns of flooding of the Rhine River have been documented throughout the Holocene and through historical records for the past 500-100 years (Brázdil et al., 1999). The last severe floods occurred in December 1993 and January 1995, at these moments the discharge increased up to ~ 12000 m³/s. Only in 1926 a higher discharge (~ 12600 m³/s) has been recorded. From the 1950s onward hydraulic modelling has resulted in an design discharge with a recurrence interval of 1/1250 years. Whereas this design discharge was initially forecasted at 15000 m³/s for the 1990s, this number has been adapted to 16800 m³/s for the year 2100 (Silva et al., 2001). This forecast of rare events (1/1250 years) is based on a record of only 100 years. Recent research has focused on extending the discharge data set of the Lower Rhine, based on historical and sedimentary information, in order to asses current flood risk (Toonen, 2013). Contributing research mainly includes the construction of a discharge data set throughout the Rhine river catchment. Multiple analytical approaches can consequently be used to identify flood events and their characteristics.

3.2. Sediment deposition

During flood events, sediment, which mainly consists of silt and clay, is deposited in the floodplain areas. Depositional processes during and after flood events are influenced by both upstream and local factors. Upstream factors include flood characteristics, including differences in flood magnitude and frequency, and the characteristics of the suspended sediment in a flood, including differences in composition, grain size, and heavy metal concentration, and are strongly interrelated (Thonon, 2006). The latter are described in section 3.3.

Upstream factors

The sediment yield of a large river as the Rhine River is controlled by several factors. First, it depends on the amount of weathering and soil erosion that takes place in the hinterland. The Rhine River catchment has different erosion characteristics in forest areas, hills with loess, and agricultural areas (for example covered with vineyards). Several models can be used to determine the amount of soil erosion (Asselman, 1997). Another factor is the sediment delivery ratio (SDR), which is the ratio between the amount of transported and eroded soil at the outlet of the catchment. Second, a large part of the flood deposits along the Lower Rhine originates from locally reworked floodplain sediment that has been eroded by lateral fluvial migration; especially bed load sediments are not transported through the entire system during a single flood event (Hoffmann et al, 2007). Moreover, the SDR varies per season, in the summer it is lower, due to the increases surface roughness by crops. In the winter there is low soil cover but the transport capacity also decreases (Walling, 1990; Asselman, 1997). The third main factor influencing flood characteristics is climate. Climate (change) controls the probability of the duration and frequency of floods (the flooding regime). Processes such as (de)forestation, changing agriculture, and other changes in land use influence the upstream sediment supply (Hoffmann et al. 2007).

Moreover, recent river basin management projects, rehabilitation of floodplains, construction of secondary channels, and restoration projects have changed the flooding regime of the Rhine River (Herget et al. 2005; Lammersen et al., 2002; Vorogushyn and Merz, 2012). In the Upper Rhine a large canalization project took place in between 1820 and 1860, when the Count of Tulla designed a plan to improve the navigability by straightening meanders (Beeger, 1990). Recent projects try to improve the water storage capacity of the river, by giving the river more space in times of high discharges, in order to prevent downstream floods (Lammersen et al., 2002; Herget et al., 2005).

Local factors

On a local scale, the amount of sediment that is deposited and the sedimentary pattern in the floodplains is controlled by two factors; floodplain topography and flood magnitude. Floodplain topography includes (natural) elevation differences and variations in the width of the floodplain. The topography of the floodplain is important as (averaged over multiple floods of varying magnitude) the amount of sand and coarse silt decreases with increasing distance to the river channel, while the content of clay and attached organic matter is relative constant with distance (Middelkoop, 1997). Therefore it is easier to identify an extreme flood event as a rare spike of coarser material at a distal floodplain than at proximal floodplain locations. The magnitude of the flood determines both the total sedimentation and the spatial pattern of deposition. The total deposition increases with flood magnitude. However, this increase is stronger for sand; minor floods are dominated by larger accumulation of fine sediment in lower areas and depressions while major floods are dominated by sand deposits, at least close to the channel (Middelkoop, 1997).

Dike-breach ponds and cut-off meanders within the embanked floodplains are natural traps for sediment during floods; meters of sediment can accumulate at such locations (Middelkoop, 1997; Toonen et al., 2012). Especially in lower lying regions (at slackwater conditions) detailed sequences of sediment record are deposited (Middelkoop, 2000; Thonon, 2006). Deposited sediments in local aquatic environments in the floodplains are generally laminated; deposition during successive floods builts up a sequence of layers with varying coarseness. Previous research concluded that the coarseness of suspended sediment that is transported, increases in the case of a higher discharge (Middelkoop, 1997; Toonen, 2013). Depending on flood magnitude (discharge), flood duration and the amount of sediment that is available, lamination and thickness of the deposits varies between several mm's to several cm's. The lamination is not regularly annual, but depends on the occurrence of floods roughly exceeding bank-full discharge (Middelkoop, 2011).

3.3. Sediment composition

Once deposited in the floodplains, sediment (especially in the clay fraction) acts as a transport agent for contaminants, nutrients and organic material. This role of fine-grained sediment is due to the binding ability of clay minerals, that allows contaminants to chemically attach to minerals. This way contaminants can be transported to lower river reaches to be deposited in the floodplains. The amount of heavy metals that is deposited depends on the amount of sediment that is deposited and therefore an important influence is the sediment yield. Furthermore the amount of heavy metals depends on the sources and inputs of heavy metals. Heavy metals can be spread in the dissolved phase, as aerosols or attached to soil particles (Vink et al., 1999; Vink & Behrendt, 2002). A distinction between natural and anthropogenic sources can be made when back ground concentrations can be distinguished. This is done using the information that urban area are the main contributors of heavy metals and that the attribution of these areas has declined over the past few decades.

Concentrations of elements and ratios of elements can be measured in order to retrieve a chemical fingerprint (Peart & Walling, 1986; Walling & Woodward, 1992; Støren et al, 2010). The chemical composition of the sediment depends on the source area of the suspended load. Each of the tributaries has a geologically and industrially distinct source area and therefore the sediment from the different sub-catchments has a varying chemical composition (Van Andel, 1950; Vink & Behrendt, 2002).

Disturbing factors, such as natural processes (Middelkoop, 2000; Thonon, 2006) and human activity (Herget et al, 2005) need to be taken into account. A range of chemical and physical processes controls the variation in metal pattern in floodplain deposits (Peart and Walling, 1986; Passmore and Macklin, 1994; Vink et al., 1999; Thonon 2006). Horizontal processes including (changes in) local floodplain topography, floodplain storage, and flow velocity can influence the chemical composition of surface samples. Besides of these horizontal processes, vertical processes can influence the chemical composition of the corings. The latter include hydraulic sorting (resuspension), metal enrichment and biological activities. An important aspect concerning the chemical composition of sediment from the youngest centuries to millennia is pollution. The basin of the Rhine is densely populated and in the last 300 years has become heavily industrialized with the Ruhr district and agglomerations as Frankfurt am Main, Stuttgart, Mannheim and Nuremberg. Change in the use of land and the environment have their impact on the emission of heavy metals, besides of that the transport of sediment is also affected by these industrialization factors (Thonon, 2006).

4. Fieldwork and core collection

4.1. Site selection

In this study, a core from the Bienener Althrein (along the Lower Rhine), from now on called the Bienen coring, was obtained to reconstruct a detailed record of the flood events along the Lower Rhine. This core is considered the sink of all upstream eroded material. To perform analysis on source areas, subsequently two types of data were needed from all the locations in the subcatchments. At first, for each of the subcatchments a (pre-industrial) record was needed of the local flood deposits; these were obtained by performing a coring (4.1.1). To obtain a post-industrial record for the tributaries, we also needed at least one surface sample from each of the subcatchments (4.1.2).

4.1.1. Cores

The cores on which this study is based were collected both from locations along the Lower Rhine, and from its upstream tributaries. As we want to perform a high resolution comparison, a location was needed that has a constant and rather stable deposition rate. To minimize the impact of grain size fluctuations caused by a varying distance to an active channel, we look for a site that is close a channel with an low migration rate. While selecting the locations of our coring sites, we need to keep in mind these needs to be able to obtain cores with a representative, high resolution, record of the local fluvial deposits. Slack-water environments seem to be the ideal locations for the coring locations along the lower Rhine and its main tributaries. Due to high sedimentation rates, cores collected in slack-water environments are assumed to have a high temporal resolution (Middelkoop, 1997). Another advantage of slack water environments is that they are currently being filled in. The latter is important to be able to make a comparison between recent fill-in the lower Rhine and the sub-catchments, as deposition rates can be calibrated (Middelkoop, 2000). An additional advantage of dike-breach ponds is that the formation date of a pond can often be obtained from historical data.

Suitable locations were selected using palaeogeographic maps (Toonen, 2013), geological maps, historical maps, Google Maps and detailed elevation models (AHN, Rijkswaterstaat, 2005). Residual channels are visible on maps as longitudinal depressions in the landscape, due to relative strong compaction of clay and peat in comparison with coarser clastic materials (Berendsen and Stouthamer, 2001). Historical maps were used to give insight in possible dike breach locations, channel diversions, canalization projects and natural displacements of river systems. The latter was used to check the lateral stability of the channel system; a channel with a low migration rate was needed to best represent the spectrum of grain size classes. In our search for coring locations we avoided areas where sedimentation was disturbed by human activities such as agricultural and industrial activities. Moreover, core samples were inspected visually for identification of bioturbation

and soil-forming processes as these could affect the chemical composition of the sediment (Middelkoop, 2000).

4.1.2. Surface samples

Locations of post-industrial sample sites were determined in the field. Prerequisites for these sites included that the material samples was deposited by recent fluvial floods, and that these deposits had not been affected by any external factor with a possible influence on its chemical composition. We thus took care of pollution from industrial activities (waste, cooling water), pollution from external (natural) sources (other attributing rivers, land run-off), agricultural land use, and digging activities (commercial, recreation).

4.2. Sampling sites

In this subchapter sampling sites (cores and surface samples) are presented. An overview of the catchment of the Rhine River including its tributaries sampling locations is found in Figure 4-1.



Figure 4-1 Overview of the Rhine River catchment

An overview of the Rhine River, its tributaries (blue) and some major adjacent cities (black) and regions (green). In red are the locations along the main tributaries from which the cores were taken. After Google maps 2011.

4.2.1. Lower Rhine

Close to the Dutch-German border, in between the German towns of Emmerich am Rhein and Xanten, the small town of Bienen is located. Northeast of the present-day path of the Rhine River, two cut-off meanders are located in the subsoil. The Bienener Altrhein, the oldest, has been active from the 14th century A.D. until the Rhine River shifted its course in Western direction (Toonen, 2013). This is when the other palaeochannel, the Grietherother Altrhein, became active (16th century A.D.). The latter remained active until it was artificially cut-off in the 18th century A.D. Due to its proximity to the main channel, the Bienener Altrhein palaeochannel was periodically flood with fluvial sediment from the Rhine River. In the last few centuries, a continuous record of fluvial deposits has been built up in the Bienener Altrhein palaeochannel. A coring was performed at the Bienener Altrhein site (Winkels, 2011; Toonen, 2013).



Figure 4-2 Location of coring site along the Lower Rhine: Bienener Altrhein (Bienen)

Exact location of site Bienener Altrhein (Bienen), Germany. Including present path and palaeochannels of the Rhine River. Source: Google Maps 2011. After Winkels, 2011; Aloserij, 201.

4.2.2. Tributaries

Upper Rhine

Pre-industrial

In the area around Speyer we noticed several cut-off meanders on the map (Figure 4-3). These are of different generations; first there is current Rhine channel, subsequently a first generation meander cut-offs caused by the canalization project, and then a second generation, that have been incised twice, by two new Rhine channel generations. These abandoned meander bends could be dated (relatively) using spatial cross-relations (Berendsen & Stouthamer, 2001). The second generation cut-offs originate from before the canalization project, these meander cut-offs were found at the villages

of Mechtersheim and Binshof, south and north of Speyer. We performed a coring nearby the town of Mechtersheim (Figure 4-3), this location will be referred to as Römerberg.

Post-industrial

Near the village of Römerberg, a recent cut-off meander is located. This has been filled up after the canalization project and therefore we took recent deposits from this location. Sampling sites along the Upper Rhine were located at 465 km, 515 km, 613 km and 655 km along the Rhine River. Exact locations of sampling sites are found in Table 3-2 and Appendix 3.



Figure 4-3 Location of coring site along the Upper Rhine: Römerberg.

Exact location (green arrow), Mechtersheim, Römerberg, Speyer, Germany. GPS position: N49 15 49.0 E8 23 12.2. After Google Maps 2011.

Neckar

Pre-industrial

Just to the south of the city of Heilbronn, close to the village of Lauffen am Neckar, a cut-off meander is visible on the map (Figure 4-4). This has been dated to be a Holocene cut-off, which has thus been filled in with floodplain sediment for approximately 6000 years (Hantke, 1993). At this location we performed a coring which can be used to establish a pre-industrial chemical composition signal.

Post-industrial

South of the location mentioned above, we found our coring location of recent deposits. Near the village of Kirchheim a river channel straightening project in the early 19th century took place. After the straightening the cut-off meanders have been filled up with material. From these post-industrial channel fills on the floodplains the post-industrial samples were collected. Sampling sites along the Neckar were located at 311 km, 410 km, and 418 km equivalent to the Rhine River. Exact locations of sampling sites are found in Table 4-2 and Appendix 3.



Figure 4-4 Location of coring site along Neckar: Lauffen.

Exact location (green arrow), Lauffen am Neckar, Heilbronn, Germany. GPS position: N49 03 45.0 E9 09 10.5. After Google Maps 2011.

Main

Pre-industrial

As the area around Frankfurt am Main is heavily industrialized, no pre-industrial floodplain deposits were found close to Frankfurt am Main. Therefore, a location had to be found upstream of the industrialized area. Around 50 km upstream of Frankfurt am Main, south of the city of Hanau, we found a palaeo meander (Figure 4-5). The meander shifted to the East, leaving behind remnants of the old meander, which are still visible in the form of a little stream near the village of Klein Krotzenburg. We also found a suitable location west of Frankfurt am Main, Sindlingen, close to Kelsterbach (Figure 4-5).

Post-industrial

On the other side of the Main, nearby the village of Kelsterbach (close to the Rhine-Main Airport) we have found suitable locations to collect post-industrial samples. These were taken from a location parallel to the river stream along an old river channel. Sampling sites along the Main were located at 433 km and 476 km equivalent to the Rhine River. Exact locations of sampling sites are found in Table 4-2 and Appendix 3.



Figure 4-5 Location of coring sites along Main: Sindlingen and Klein Krotzenburg.

Exact locations (blue arrows), (1, left) Sindlingen, West of Frankfurt am Main, Germany. GPS Position: N50 03 45.0 E8 31 11.6. (2, right) Klein Krotzenburg, East of Frankfurt am Main, Germany. GPS position: N50 04 32.1 E8 57 33.6. After Google Maps 2011.

Moselle

Pre-industrial

To be able to find a location to collect Holocene material we looked on geological maps of the Moselle area. As the chemical compositional signal should be specific for the sediment entering the Rhine River at Koblenz, a location close to Koblenz had to be found. However, the only Holocene floodplain deposits that are visible on the geological map, were found close to the city of Kenn (Figure 4-6).

Post-industrial

The floodplains along the lower part of the Moselle are confined in a bedrock valley and the river has been canalized during the last 50 years. We looked for a location close to the mouth of the main at Koblenz (in order to obtain the signal of the complete Moselle), but the possible influence of the backwater of the river Rhine was also taken into account. A location was found somewhat upstream of Kenn. Sampling sites along the Moselle were located at 412 km and 570 km equivalent to the Rhine River. Exact locations of sampling sites are found in Table 4-2 and Appendix 3.



Figure 4-6 Location of coring site along Moselle: Kenn.

Exact location (green arrow), Kenn, North-East of Trier, Germany. GPS position: N49 48 26.3 E6 43 55.8. After Google Maps 2011.

4.3. Sample collection

4.3.1. Corings

The cores were collected using a hand-operated corer which delivers 1 meter long segments of 4.5 cm diameter and they were collected in PVC tubes. Cores were logged in the field; sediment structure, organic matter content, colour, oxidation/reduction zone, carbonate content and plant remains were noted every ten centimetre interval. In the laboratory the core segments were divided into two halves (along the longer axis), logged in detail and photographed. The cores were sealed and packed again and stored in refrigerated storage cells to prevent oxidation of the cores. Both of the sections of each core segment were used; one for grain size analysis, and the other half was transported to the lab of the Aberystwyth University where a XRF scan was performed to retrieve chemical compositional data (chapter 5.1.2).

Lower Rhine site: Bienener Altrhein (Bienen)

In the context of his research about the infill of a cut-off meander of the Rhine River (i.e. Bienener Altrhein palaeochannel), Winkels performed a coring along the Bienener Altrhein (Table 3-1). The core segments were collected with a Bohncke modified piston corer. This coring resulted in a series

of 10 core segments, from now on called Bienen 1 to Bienen 10. In total, the depth covered over 8 meters corresponding to a maximum age of approximately 400 years (Winkels, 2011; Toonen, 2013).

Pre-industrial sites

During a fieldwork campaign (October 2011), cores have been taken at the sites presented in the previous section (Table 4-1). From each of the subcatchments, at least one core was collected with a soil corer. All of the corings resulted in a single core segment with a length of approximately one meter.

4.3.2. Surface samples

Post-industrial sites

Recent depositions are taken along the river channels of the different tributaries (Table 3-1). These samples were taken with an Edelman corer. From each catchment samples are taken from at least two different locations that are not too close to each other. At each location two samples are taken; one from a depth of 10 cm to 20 cm and one of a depth of 20 cm to 30 cm. Samples were collected in a plastic bag to transport them to the lab.

To allow further analysis, the samples were homogenised. First the bulk samples were dried at ambient room temperature and plant remnants were removed. Samples that were too moist were dried in an oven, overnight at 55 °C. Then, the bulk samples were manually grounded and pulverised in a porcelain mortar. By sieving the samples they were eventually homogenised.

Table 4-1 Overview of the sampling sites (corings)

Site	Location	Catchment	Date of collection	Coring depth
		Lower Rhine / Tributary	(month, year)	(cm)
Bienener Altrhein	Bienen	Lower Rhine	June, 2011	156 - 849
Römerberg	Speyer	Upper Rhine	October 2011	148 - 238
Lauffen	Heilbronn	Neckar	October 2011	100 - 190
Sindlingen	Frankfurt (west)	Main	October 2011	120 - 205
Klein Krotzenburg	Frankfurt (east)	Main	October 2011	125 - 215
Kenn	Trier	Moselle	October 2011	10 - 60

Table 4-2 Overview of the samping sites (surface samples)

Site	Setting Location		Catchment	Date of collection	Coring
(#)		(exact location (GPS)	(Tributary)	(month, year)	depth (cm)
		in Appendix 3)			
4	Levee	Kenn	Moselle	October 2011	0.10-0.30
5	Pointbar	Kenn	Moselle	October 2011	0.10-0.30
9	Levee	Klein Krotzenburg	Main	October 2011	0.10-0.30
11	Levee/floodplain (high)	Horkheim	Neckar	October 2011	0.10-0.30
12	Levee/floodplain (low)	Horkheim	Neckar	October 2011	0.10-0.30
13	Levee	Edingen/Neckarhausen	Neckar	October 2011	0.10-0.30
14	Floodplain (high)	Mannheim	Neckar	October 2011	0.10-0.30
16	Floodplain (high)	Römerberg	Upper Rhine	October 2011	0.10-0.30
17	Floodplain (low)	Römerberg	Upper Rhine	October 2011	0.10-0.30
18	Palaeochannel	Sindlingen	Main	October 2011	0.10-0.30
19	Floodplain	Rheindürkheim	Upper Rhine	October 2011	0.10-0.30
20	Levee	Rheindürkheim	Upper Rhine	October 2011	0.10-0.30
21	Levee	Ingelheim	Upper Rhine	October 2011	0.10-0.30
22	Levee	Ingelheim	Upper Rhine	October 2011	0.10-0.30
23	Floodplain	Alken	Moselle	October 2011	0.10-0.30
24	Floodplain	Alken	Moselle	October 2011	0.10-0.30
25	Floodplain	Alken	Moselle	October 2011	0.10-0.30
26	Floodplain	Andernach	Upper Rhine	October 2011	0.10-0.30
27	Floodplain (low)	Andernach	Upper Rhine	October 2011	0.10-0.30
28	Levee	Bonn	Upper Rhine	October 2011	0.10-0.30
29	Floodplain (high)	Bonn	Upper Rhine	October 2011	0.10-0.30

5. Laboratory methods and data analysis

5.1. Laboratory methods

5.1.1. Grain size analysis

The cores segments referred to as Bienen 1 to Bienen 10 were collected by Winkels in july 2011 at the Bienener Altrhein location (section 4.3.1). Winkels (2011) made notes of clearly visible transitions and sandy layers within the core segments. Moreover, photographs were taken, which also show the major depositional transitions and some sandy layers could be identified. The results of this visual analysis, including pictures and notes, are found in Appendix 8 and, more extensively, in Winkels (2011).

The Bienen cores were sampled continuously at a semi-regular sample thickness of 1-2 cm's to perform grain size analysis (Winkels, 2011). The upstream cores (Kenn, Klein Krotzenburg, Lauffen, Römerberg and Sindlingen) were sampled with a regular sample thickness of 1 cm per 5 cm. The relative low average sampling resolution can be interpreted in two ways. 1) A constant grain size within the sample results in corresponding mode and average values of the measurement. 2) If the grain size within a sample is not constant (in the case of a sandy layer) mode an average value differ and (minor) sandy layers might not be detected.

Sample intervals were slightly adjusted to correspond with visual flood layering i.e. sandy layers that had been identified during visual analysis were taken into account to be able to separate specific grain size classes in a sample. This was done to avoid the out averaging of grain size results within a sample and obtain an optimal representation of the grain size class for each of the samples. However, during the sampling of the Bienen core segments, Winkels sometimes deviated from the 2 cm sampling interval border instead of sticking to the continuous sampling, without notifying this. Therefore, the exact borders of the sample interval are not always known. The post-industrial samples have been sampled from homogenized material; each sample thus represents a depth of 10 cm.

Before grain size analysis was performed all samples were pre-treated, i.e. all non-siliclastic particles that could affect grain size measurements (e.g. plant or root remains), were removed from the sample (Konert and Vandenberghe, 1997). Organic matter was removed from the samples by adding 10 ml 30% H_2O_2 solution. All carbonates and other ions were removed from the sample by adding 5 ml of 10% HCl solution and boiling the mixture. Flocculates, caused by cohesiveness were separated by adding 300 mgs natriumpyrophosphate (Na₄P₂O₇·10H₂O).

Grain size was measured using laser diffraction analysis. This method is based on the correlation between (1) the angle of light scattered by particles under influence of a laser beam and

(2) the size distribution of these particles (Jonkers et al., 2009). Based on available time and budget, grain size analysis was performed on 2 cm resolution average.

Grain size analysis was carried out in the lab of the Vrije Universiteit in Amsterdam. Particle size distributions of suspended sediment samples in the range between 0.15 μ m and 2000 μ m were measured in 56 bins by the HELOS KR (Sympatec) Laser Particle Sizer (LPS) (Jonkers et al, 2009; Witt et al., 2010). Results of the analysis were grouped in a series of logarithmically spaced grain size distribution classes for each of the samples.

5.1.2. Chemical composition analysis

XRF core scanning

All cores were scanned at Aberystwyth University in Wales (UK) using an Itrax XRF scanner (Croudace et al, 2006). X-Ray Fluorescence (XRF) core scanning is a non-destructive characterization of sediment sequences that can be used for material from lacustrine environments (Jenkins & De Vries, 1970; Croudace et al, 2006; Richter et al, 2006). It provides high resolution information about changes in the chemical composition of a core by creating an elemental profile with a range from Aluminium (¹³AI) to Uranium (⁹²U). Although the quality of elemental data resulting from the scan mainly depends on the quality of the sample, the scanner provides a detailed relative log of the chemical composition of the core.

Under the influence of incoming X-ray radiation, an electron from an inner atom shell is ejected. This results in a vacancy which is filled by an electron falling back from an outer shell. The energy difference between the inner and the outer shell is emitted as electromagnetic radiation, the latter can be detected by the XRF core scanner. Each element has a characteristic wavelength of this emitted radiation, and the amplitudes of the peaks in the detected XRF-spectrum are proportional to the concentration of the elements in the range between Aluminium (¹³Al) to Uranium (⁹²U) (Croudace et al, 2006; Richter et al, 2006; Jones et al., 2009, 2010).

The XRF scanner performs a continuous XRF analysis on the surface of a split sediment core. Before inserting the core into the scanner, the surface of the core was cleaned and smoothened. Any visible cracks and holes were logged. Before the actual scan, the core was covered with micro-film to prevent desiccation (Lamb et al., 2005; Croudace et al, 2006). All cores were scanned using a molybdenum tube set, the preset voltage was 60 kV and the current varied between 40 mA and 50 mA. Based on available time and budget the scan resolution was either 500 µm or 1000 µm. For the all the Bienen cores, we used a XRF exposure time of 200 ms and a dwelling time of 30 s. Specific (optimal) XRF scan settings varied per core and are reported in Appendix 11. As starting and ending points of the measurements were put in manually, minor shifts in the depth output of the scanned core segments could occur.

Handheld XRF surface samples scanning

To identify the chemical composition of the surface samples, we used a handheld XRF scanning device. Although this device, provided by and operated at the Aberystwyth University, performs a scan on fewer elements, measures the concentration of several elements in the bulk samples. The handheld XRF scan detects the following elements; Sb, Sn, Cd, Ag, Sr, Rb, Pb, Se, As, Hg, Zn, Cu, Ni, Co, Fe, Mn and Cr. The output of the scan is an elemental count for each of these elements in parts per million (ppm). Cores were scanned by hand, applying a scanning time of at least 100 seconds to ensure all elements were detected and to minimize the error percentage of the scans. As these error percentages are relatively stable for each of the elements, a mean error percentage was calculated to determine the usability of the elements. Moreover, the duration of the scan is listed for each of the scans.

5.2. Data Analysis

In order to answer our research questions, a series of analytical steps was performed on the data obtained by grain size analysis and chemical composition analysis (Fig. 5-1). First, the grain size data were combined with historical data to identify flood events in the grain size data. Chemical composition data were normalized, to filter all scan-specific variations, and bulked, to equalize the resolution with that of the grain size data. The normalized and bulked data were combined with previous research to obtain element ratios that were usable to acquire information on grain size. This chemical proxy was consequently used for the first objective; i.e. to identify flood events in grain size data.

Moreover, the chemical proxy was used to correspond the grain size data set with the chemical composition data set. Subsequently, the correlation of aluminium (¹³Al) with the clay fraction was tested for its suitability as corrector for the clay content. Also, a series of correlation matrices were set up to acquire information for possible application of additional statistical methods.

Chemical composition data from the subcatchments (cores and surface samples) were used to setup characteristic fingerprints for each of the subcatchments. Also, the chemical proxy was used to obtain the chemical composition of the selected flood deposits from the chemical composition data set. Subsequently the results of the previous objectives were combined to trace the (mixed) origin of Lower Rhine flood events.



Figure 5-1. Schematic overview of analytical methods used in this study.

5.2.1. Grain size data

The distribution classes resulting from the analysis were bulked to five classes, representing the sand fraction (63 - 2000 μ m), the silt fraction (8 - 63 μ m), and the clay fraction (subdivided into three classes, < 2 μ m, < 4 μ m, and < 8 μ m). In addition, the 95th percentile (P95) value was calculated for each of the samples (Aloserij, 2013; Toonen, 2013). To enable analysis of the grain size data, grain size distributions of each of the samples were combined to assemble a continuous grain size depth profile. Due to human interference close to the sample location (the construction of a sluice and input of coarse-grained sands), the data retrieved from the upper part of the coring (Bienen 1 and Bienen 2) were not used in this analysis (Winkels, 2011; Aloserij, 2013). Furthermore, because separate core segments might have shrunk or expanded (due to compaction by drilling, transport or storage) causing discontinuities in the sample depth, sample depths were converted to real depth to form a continuous record of all the Bienen cores. In this conversion, it was assumed that the maximum depth of individual core segments resemble true depth, and that the core record was continuous. This way the length of (some) core segments was extended or reduced to fit the contiguous core segment, i.e. the real depth of the deepest point of the contiguous core segment.

From these data flood events were identified from peaks in the sandy grain size classes and higher P95 values. Subsequently, previous theses were used to verify these identified flood events in order to date the flood events. Toonen (2013) used historic sources to identify flood events. However, these data can be incomplete (due to varying source material) and the source of flood events is mostly not known. Aloserij (2013) verified whether these flood events had an upstream origin instead of being caused by local impacts (i.e. the collapse of ice dams or failure of river embankments). This was done by comparing two lower Rhine cores and identifying identical flood events are easier to recognize in distal floodplains, based on the fact that the coarse material and the amount of coarse material in these floods is relatively high.

5.2.2. Chemical composition data

Normalizing elemental data

The XRF core scanner provides counts for each of the elements. The amount of scattering is measured for each sampling point and each element in terms of coherent and incoherent scattering; to account for changes in water content and sediment density, this count-to-scatter ratio is calculated (personal communication with Rassner). To filter the scattering, measurement results had to be normalized by dividing elemental counts by the sum of the corresponding coherent and incoherent counts of molybdenum (a molybdenum tube set was used, see section 4.1.3).

Bulking XRF data

To compare grain size data with chemical composition data (see section 4.2.3), the data have to be uniform in resolution. This is not the case for the data resulting from the different analytical methods; the resolution of the grain size data is 1 cm to 5 cm while the resolution of the chemical composition data is 500 μ m or 1000 μ m. To set up a combined data set throughout the depth of the cores, the chemical composition data was bulked (continuously) by averaging a consecutive series of chemical composition data points to obtain a resolution that matches with the resolution of the grain size data.

5.2.3. Correlating grain size data and chemical composition data

Chemical proxy for grain size

Previous literature indicates that there are some elements that correlate with certain classes of the grain size of sediment. Previous research indicates that the Zr/Rb ratio can be exploited to acquire information on grain size (Dybvyk and Harris, 2001; Kylander et al., 2011). Zirconium (Zr) is an element that is associated with the relatively coarse grained fraction of sediments (Dypvyk and Harris, 2001). Consequently, the Zr counts can be used as an indicator of the abundance of relatively coarse grained sediment. Rubidium (Rb) on the other hand, shows a positive correlation with fine grained sediments (Dypvyk and Harris, 2001). Rb is normally associated with claystones and siltstones. Therefore Rb can be used as an indicator of the amount of fine grained sediment. Other ratios of elements that can be used to acquire grain size information are the Zr/Ti ratio (Oldfield et al., 2003) and some ratios based on Al, which is supposed to correlate with fine grained sediment and several elements that correlate well with coarse grained sediment (i.e. Si/Al, Ti/Al, and Zr/Al) (Calvert et al., 1996; Schneider et al., 1997; Calvert et al., 2001).

Correlating grain size and chemical composition

After normalizing, bulking and standardizing the chemical composition data were used to calculate the Zr/Rb ratio and other ratios (Zr/Ti, Si/Al, Ti/Al and Zr/Al). For each of the core segments, these ratios were compared with different cumulative grain size classes. For all of these classes the correlation coefficients were calculated. In some cases, results from the grain size analysis and ratios showed similar patterns, although the exact position of the peaks were slightly shifted. In these cases the correlation was improved by applying a minor shift to the depths of the chemical proxy ratio. Subsequently correlation coefficients were calculated for the corrected (i.e. shifted) matched depths.

5.2.4. Correction of the clay content

Correlation matrices

Set of elements that are associated with each other, can be used as an indicator for changes in grain size. To quantify the strength of association between sets of elements, correlation matrices were constructed using the data analysis tool of Microsoft Excel 2010. Sets of elements that are associated well, can be used in statistical methods (linear regression, principal component analysis) to unravel the contribution of a component . Although the XRF scans were standardized, XRF scan settings vary per core segment (due to varying settings). Therefore a separate correlation matrix was constructed for each of the core segments. We made a selection of ten elements of interest for this research, including Si, K, Ca, Ti, Mn, Fe, Rb, Sr, Zr and Pb.

Al-standardizing chemical composition data

To correct the chemical composition data for the variation in clay content, the correlation of ¹³Al with the clay fraction was tested. Correlation coefficients of ¹³Al were calculated with the clayey grain size classes (< 2 μ m, < 4 μ m, and < 8 μ m). Correcting the elemental counts for the clay content was done by dividing the elemental count of each sampling point by the corresponding ¹³Al count. We applied the same standardizing method on the subcatchment cores, to enable a comparison between the elemental counts of all core segments.

5.2.5. Characterizing subcatchments

The next part of the analysis involved the determination of the chemical composition of the subcatchments. The normalized and standardized elemental data of the upstream cores were used to find the chemical characteristics of each of the subcatchment source areas. The elements of the post-industrial samples that exceeded the average error percentage 15 %, were excluded. For each element a catchment-propagation graph was constructed to create a visual overview of the occurrence of these elements throughout the catchment.

Subsequently the data of the cores and the surface samples were used to set up a characteristic fingerprint for each of the subcatchments. To enable a combination of these two data sets, a set of elements was selected that was detected in both the cores and the surface samples. Elements that are sensitive to horizontal or vertical displacements and soil conditions were excluded from this selection. The remaining set of elements was used to identify the origin (source area) of certain downstream (flood event) depositions (i.e. fingerprinting). For each subcatchment a fingerprint was constructed by averaging the elemental occurrence in the pre-industrial core (i.e. throughout depth), and averaging the elemental occurrence of the surface samples.

To be able to use a set of fingerprints to provide information on the relative contribution of potential sediment sources to the sediment deposited of an downstream river, there are three main requirements (Walling et al, 1993);

- 1. Fingerprints should reflect environmental control and are capable of discriminating potential sediment sources.
- 2. The selection of fingerprints needs to be statistically tested to confirm that individual sediment sources can be distinguished by their fingerprint(s).
- A system needs to be developed that is capable of comparing the composition of downstream deposited sediment with the fingerprints of potential upstream sources. This system should also be able to provide an estimate of the relative contributions of those sources.

5.2.6. Tracing flood origin

By linking the peaks in grain size data with flood events, we identified the flood events in the grain size data (5.2.1). Taking into account the shifts that were needed to fit the grain size data with the chemical composition data, the chemical proxy was used to identify the flood events within the chemical composition data (5.2.3). These correlations were used to determine the chemical composition of the flood events. In this process we have only used the flood events that were dated to the same year at which we had identified peaks in our proxy abundance plots. As a consequence, we have only used those of the floods that were recognized with the chemical proxy data.

6. Results and discussion

6.1. Identification of flood events

Figure 5-1 provides plots of the cumulative silt and sand fraction and the P95 plotted against the converted (real) depth for each of the core segments. Appendix 1 provides the raw grain size data and raw XRF data for each of the Bienener Althrein core segments. Below, the processed grain size data are discussed for each of the core segments. Based on the percentage of the sandy fraction, or based on an excessive sum of the silt and sand fraction, layers were identified as a sandy layers. The relative low grain size sampling resolution (4.1.2) and in some cases the unnotified varying sampling interval borders (4.1.2), can cause some sandy layers (flood events) to remain unidentified.



Figure 6-1 Depth plots of Bienener Altrhein core segments 3-10.

Vertical axis represents depth (cm) throughout the core. Horizontal axis represents silt+sand fraction (%, upper axis, blue) and P95 (µm, lower axis, red).

Bienen 3

The original depth of Bienen 3 was 167 cm to 239 cm, we converted these to a real depth of 156 cm to 239 cm. Due to a partial collapse of the coring hole, the sandy upper part (3-4 cm) is not representative. Sandy layers were found at 165 cm, 177 cm, 184 cm, 195 cm, 198 cm, 216 cm, 221 cm and 239 cm.

Bienen 4

The original depth of 267 cm to 339 cm was converted to a real depth of 241 cm to 339 cm. Sandy layers were found at 246 cm, 266 cm, 276 cm, 282 cm, 320 cm. Moreover, two areas were identified as sandy, the first in between 298 cm and 304 cm and the other at the bottom of the core, from 331 cm to 339 cm.

Bienen 5

The original depth of 357 cm to 429 cm was converted to a real depth of 341 cm to 357 cm. Sandy layers were found at 370 cm, 383 cm and 429 cm.

Bienen 6

The original depth of 453 cm to 529 cm was converted to a real depth of 431 cm to 529 cm. We found a relative high average percentage of the sand fraction compared to the other cores. Sandy layers were distinguished at 444 cm to 446 cm, 465 cm, 475 cm, 490 cm and 526 cm.

Bienen 7

The original depth of 545 cm to 619 cm was converted to a real depth of 531 cm to 619 cm. Sandy layers could be distinguished and were found at 560 cm, 564 cm, 576 cm, 600 cm.

Bienen 8

The original depth of 631 cm to 719 cm was converted to a real depth of 621 cm to 719 cm. Sandy layers were found at 645 cm, 650 cm, 659 cm and between 679 cm and 683 cm.

Bienen 9

The original depth of 737 cm to 817 cm was converted to a real depth of 721 cm to 817 cm. We found a relative low average percentage of the sand fraction compared to the other cores. Sandy layers were distinguished at 745 cm, 771 cm, 791 cm and 810 cm.

Bienen 10

The Bienen 10 core was not converted as the original and real depth corresponded, i.e. they were both 819 cm to 849 cm. We found a relative high average percentage of the sand fraction compared to the other cores. No real sandy layers were distinguished, but grain size increased with depth. At the bottom of the core grain size increased rapidly due to coarser sands on which the coring ended.

6.1.1. Selected flood events

The results from Aloserij (2013) were used to link extreme flood events (known from historical flood data) with peaks in the grain size data. Ten major flood events were selected (based on grain size data) from the Bienener Altrhein core segments. Table 6-1 provides an overview of these flood events, their corresponding (cumulative) grain size classes (including sand and silt + sand) and the dates of these flood events.

Table 6-1 Correlation of extreme flood events.

Extreme flood events (based on historical flood data) were correlated with grain size data throughout depth (based on Aloserij, 2013).

Depth (real, cm)	Sand (%)	Silt + Sand (%)	Historical flood data (year A.D.)
156	15.13	62.92	1882/1883
239	15.75	57.95	1850
276	13.69	52.53	1845
446	12.63	67.90	1784
560	7.83	65.04	1729
564	8.48	70.58	1726
659	50.39	79.71	1682
683	16.32	63.03	1671
825	8.48	56.36	1608
835	9.21	55.17	1602

6.1.2. Upstream Rhine cores

Appendix 9 provides the results of the upstream Rhine cores. The sampling resolution of the upstream Rhine cores was 5 cm, which does not allow us to analyze these data in detail. Due to varying floodplain settings (e.g. distance to active river channel) and different core depths average sand fractions varied per subcatchment core. In the Upper Rhine core (Römerberg, 148-238 cm) the sand fraction varies between 40 to 60 percent. The sand fraction remains stable throughout the core, sandy areas were identified around 150 cm, 185 cm and 230 cm. In the Neckar core (Lauffen, 100-190 cm) the sand fraction varies between 70 to 90 percent. The sand fraction increases with depth, a sandy area was identified around 125 cm. In the first Main core (Sindlingen, 120-205 cm) the sand fraction varies between 60 to 80 percent. The sand fraction remains stable throughout the core, a sandy area was identified around 170 cm. In the other Main core (Klein Krotzenburg, 125-215 cm) the sand fraction varies between 50 to 80 percent. The sand fraction remains stable throughout the core, a sandy areas were identified around 135 cm, 150 cm and 160 cm. In the Moselle core (Kenn, 10-
60 cm) the sand fraction varies between 40 to 60 percent. The sand fraction decreases with depth, a sandy area was identified around 15 cm.

6.1.3. Discussion

A series of flood events was identified throughout the Bienen coring. However probably not all sandy layers were detected during visual and grain size analysis. Limiting factors as the relative low grain size sampling resolution and unnotified varying sampling interval borders might have caused some minor sandy layers to remain undetected. However, the major sandy layers were identified. The focus of this study is not on the construction of a detailed framework of flood events, in the next part of this research the major sandy layers are used to find a relation with chemical composition data.

6.2. Correlating grain size and chemical composition data

6.2.1. Normalized chemical composition data

Appendix 1 (raw data) and Appendix 2 (selected elements) provide the normalized elemental data for each of the Bienen core segments. These data include the normalized elemental counts at each depth, for the elemental range between Al and Pb. Zr counts vary between 0.040 and 0.060 for all the Bienen core segments and remain stable. Peaks in the Zr counts were identified at 179 cm, 184 cm and 232 cm (Bienen 3), 405 cm (Bienen 5), 441 and 446 cm (Bienen 6), 585 cm (Bienen 7), 663 cm, 674 cm and 681 cm (Bienen 8), 750 cm, 771 cm, and 810 cm (Bienen 9), and 829 cm and 845 cm (Bienen 10). Rb counts vary between 0.030 and 0.040 and remain stable. No peaks were identified in the Rb counts. The continuous record of the combined Bienen core segments does not show any trends. The records of the elemental counts of the combined Bienen core segments are not continuous, each of the separate core segments can be identified in the plots of most of the elemental counts.

6.2.2. Chemical proxy for grain size

Appendix 1 provides comparative data for each of the proposed chemical proxies. For each of the Bienen core segments an overview is given of the correlation coefficients (Zr/Rb, Si/Al, Ti/Al, Zr/Al, and Zr/Ti) with varying grain size classes (> 8 μ m, > 16 μ m, > 32 μ m, and > 64 μ m). In some cases a (partial) shift was needed to correlate the grain size data with the chemical composition data. Correlation coefficients were highest (overall > 0.7) with the Zr/Rb ratio in each of the core segments. In most cases there also was a mediocre correlation coefficients with grain size classes and are therefore not usable as a proxy. Due to its high correlation coefficient with particular grain size classes, the Zr/Rb ratio is the most suitable chemical proxy.

6.2.3. Bienen core segments

Appendix 8 provides the comparative data for the Bienen core segments, i.e. the combined plots of the Zr/Rb ratio and the grain size fractions.

Bienen 3

The basis plots of Bienen 3 core segment (Figure 6-2) of the Zr/Rb ratio and the > 8 μ m grain size class look similar; peak areas do correspond and the overall trend throughout depth is similar. However when we take a closer look, we find that although the peak show a similar pattern, they are not at the exact same position. The first grain size peak, at 165 cm, has no corresponding Zr/Rb ratio peak. The pattern of the grain size peaks at 177 cm, 184 cm and 195 cm have a corresponding pattern in the Zr/Rb ratio plot. However, these peaks are slightly shifted. The same goes for the grain size peaks at 216 cm and 221 cm, this pattern of peaks, although slightly shifted, is also found in the Zr/Rb ratio plot. The Zr/Rb ratio peak at 233 cm is not found in the grain size plot.



Although the distribution of peaks in both the grain size and the Zr/Rb ratio plots show a similar pattern, the exact position of the peaks are slightly shifted. Therefore all data points were shifted to a new depth, that of 1 cm less deep than the original depth.

	>8um	>16um	>32um	>64um
Original	0,461224	0,539429	0,578639	0,539442
Shifted	0,644679	0,723982	0,805674	0,834349

Table 6-2 Correlation matrix for Bienen 3. Original and shifted data.

Table 6-2 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio for the shifted data. Although the correlation of the Zr/Rb ratio goes best (r = 0.83) with the coarsest class (> 64 µm), there is a good correlation with all the selected fraction classes. The correlations increase with increasing particle size.

Bienen 4

The basic plots of the Bienen 4 core segment (Figure 6-3) show a similar pattern. Although the peak in the upper part of the core does not correspond, the same trend is visible in both plots. In the bottom of the core (310 cm – 339 cm) the two plots do correspond. The grain size peaks at 246 cm, 276 cm and 282 cm are not found in the Zr/Rb ratio plot. The Zr/Rb ratio peaks at 252 cm and 268 cm are not visible in the grain size plot. The bottom part shows a similar pattern in both of the plots. Overall there is a similar trend, the plots do not correspond well in the upper part whereas they do correspond in the bottom part of the core. Relative to each other, there is no shift that can be applied in order to improve the fit of the two plots.



Table 6-3 Correlation matrix for Bienen 4.

	>8um	>16um	>32um	>64um
Original	0,717176	0,700221	0,553047	0,110655

Table 6-3 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio. The correlation of the Zr/Rb ratio with the class > 8 μ m is good (r = 0.72). However, the correlation with the coarsest particle size class (> 64 μ m) is rather weak (r = 0.11).

Bienen 5

The basic plots of the Bienen 5 core segment (Figure 6-4) show a similar pattern, except for the extreme Zr/Rb ratio peak at 405 cm which is not visible in the grain size plot. The upper part of the Bienen 5 core shows a similar pattern for both of the plots. Peaks in the grain size data at 358 cm, 370 cm and 383 cm, have their equivalents in the Zr/Rb ratio plot. The extreme Zr/Rb ratio peak at 405 cm is not visible in the grain size plot. The orrelations decrease with increasing particle size.



Although the distribution of peaks in both the grain size and the Zr/Rb ratio plots show a similar pattern, the exact position of the peaks are slightly shifted in the upper part of the core segment. For this part (341 cm – 385 cm) a shift of the Zr/Rb ratio data would fit the peak areas of the plots. For this part we recalibrated the Zr/Rb ratio data; these data points are allocated to a new depth, that of 1 cm less deep than the original depth. However, the lower part still does not fit well. This is probably due to the Zr/Rb ratio peak at 405 cm which lacks in the grain size plot.

	>8um	>16um	>32um	>64um
Original	0,322911	0,323142	0,276425	0,197411
Shifted	0,319491	0,310755	0,323192	0,361464
Upper part				
(shifted)	0,731762	0,703849	0,692514	0,581068

Table 6-4 Correlation matrix for Bienen 5. Original, shifted and upper part data.

Table 6-4 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio for the shifted data. The correlation values are only based on the upper part of the core segment (341 cm – 385 cm). Although the correlation of the Zr/Rb ratio with the class > 8 μ m is good (r = 0.73), there also is a good correlation with the > 16 μ m and > 32 μ m classes. In the lower part of the core segment, the correlations are weak. The original correlations are weak (r < 0.33) and decrease with increasing particle size for the original. The correlations for the Upper part remain stable (variation < 0.05) with varying particle size.

Bienen 6

The basic plots of the Bienen 6 core segment (Figure 6-5) show a similar pattern. An equal trend is visible in both plots and the peak areas of the two plots do correspond well. The grain size peak area around 446 cm corresponds with the peak area in the Zr/Rb ratio plot. Moreover, the other peaks (around 465 cm, 475 cm, and 490 cm) are found at equal depths in both of the plots. The only area that corresponds less perfectly between the two plots, is the bottom 5 cms. No shift was needed to improve the fit of the two plots.



Table 6-5 Correlation matrix for Bienen 6.

	>8um		>32um	>64um
Original	0,786676	0,759489	0,73804	0,696085

Table 6-5 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio. The correlation of the Zr/Rb ratio goes best (r = 0.79) with the class > 8 μ m. The correlation with the > 16 μ m class and the > 32 μ m class are also quite good (r = 0.76 and r = 0.74). The correlations decrease with increasing particle size.

Bienen 7

The basic plots of the Bienen 7 core segment (Figure 6-6) of the Zr/Rb ratio and the > 8 μ m class look similar; peak areas are corresponding and the overall trend throughout depth is similar. All peaks are found in both the grain size and the Zr/Rb ratio plots, although sometimes minor shifts are visible. No shift was applied to improve the fit of the two plots.



Table 6-6 Correlation matrix for Bienen 7.

	>8um	>16um	>32um	>64um
Original	0,888924	0,918979	0,898392	0,847635

Table 6-6 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio. The correlation of the Zr/Rb ratio goes best (r = 0.92) with the class > 16 μ m. The correlation with the > 8 μ m class and the > 32 μ m class is also good (r = 0.89 and r = 0.90). The correlations slightly decrease with increasing particle size.

Bienen 8

The basis plots of the Bienen 8 core segment (Figure 6-7) of the Zr/Rb ratio and the > 8 μ m class show a similar overall trend and pattern of peak areas throughout depth. However, none of the peak areas are at the exact same depth, they are all shifted. The two major grain size peaks, at 659 cm and at 683 cm both correspond with a slightly shifted Zr/Rb ratio peak. The same shift can be applied to the general pattern of grain size peaks to fit the corresponding Zr/Rb ratio plot.



A shift was applied to fit the peak area of the plots. Therefore we recalibrated the Zr/Rb ratio data; all data points are allocated to a new depth, that of 1 cm less deep than the original depth.

Table 6-7 Correlation matrix for Bienen 8. Original and shifted data.

	>8um	>16um	>32um	>64um
Original	0,19721	0,242569	0,227442	0,154496
Shifted	0,667298	0,706786	0,676712	0,581338

Table 5-6 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio after we performed the recalibration. The correlation of the Zr/Rb ratio goes best (r = 0.71) with the class > 16 µm. The correlations decrease with increasing particle size.

Bienen 9

The basic plots of the Bienen 9 core segment (Figure 6-8) show a similar pattern, although some grain size peak areas (at 745 cm and 791 cm) are dislocated (shifted). The grain size peak at 771 cm and the majority of the minor peaks do correspond quite well with the Zr/Rb ratio plot. However, the Zr/Rb ratio peak at 783 cm does not have its equivalent in the grain size plot.



Table 6-8 Correlation matrix for Bienen 9.

	>8um	>16um	>32um	>64um
Original	0,601645	0,630126	0,599367	0,4238

Figure 6-8 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio after we performed the shift. Although there is no outstanding correlation, the Zr/Rb ratio correlates best (r = 0.63) with the class > 16 µm. The correlations decrease with increasing particle size.

Bienen 10

The basic plots of the Bienen 10 core segment (Figure 6-9) show a similar trend, but the plots of both grain size and the Zr/Rb ratio do not correspond. No equivalent peak areas are visible. One major peak (829 cm) in the Zr/Rb plot does not have an equivalent in the grain size plot. At 845 cm there is a peak in both of the plots. No shift could be used to improve the fit of the two plots.



Table 6-9 Correlation matrix for Bienen 10.

	>8um	>16um	>32um	>64um
Original	0,28399	0,274286	0,218542	0,13276

Table 6-9 shows the correlation matrix of the different grain size fractions with the Zr/Rb ratio. The correlations are weak (r < 0.28) and decrease with increasing particle size.

6.2.4. Upstream Rhine cores

Appendix 9 provides the combined grain size data and elemental data for the upstream cores. For none of the upstream cores, a good correlation between grain size and Zr/Rb ratio was found.

6.2.5. Discussion

The normalized data show that the elemental counts for each of the Bienen core segments are not continuous. Variations in scan results are caused by the different settings under which each of the core segments were scanned. To set up a relation between the grain size data and the chemical composition data, the separate core segments were consequently used to calculate correlation coefficients. Different chemical proxies were tested for their correlation with the sandy grain size classes (> 8 μ m, > 16 μ m, > 32 μ m, and > 64 μ m). The correlation coefficients for the Bienen core segments shows that the Zr/Rb ratio best correlates with the grain size fractions.

Subsequently, the Zr/Rb ratio were correlated with the different grain size fractions by means of plotting the graphs and calculating the correlation coefficients. For some core segments (Bienen 4, Bienen 6, Bienen 7, and Bienen 9), a relation was clearly detectable. For core segments

Bienen 3, Bienen 5, and Bienen 8 the correlation coefficients were increased by shifting the chemical composition data. The shifts were needed to correct for shrinking of the core segments, that might have occurred during transport and storage, or as a result of desiccation or scan settings. After the shifts were applied, good correlation coefficients were also obtained for the remaining core segments.

The resulting correlation coefficients show that in general the Zr/Rb ratio is a good indicator for the sandy grain size fraction. A quantified correlation was set up for each of the core segments. Highest correlations were found with the grain size classes > 8 μ m, > 16 μ m for most of the Bienen core segments (Bienen 4 - Bienen 10). Although the Zr/Rb ratio is correlated with the sandy class (> 63 μ m), a better relation is obtained when the silty grain size fraction is included in the correlation. Correlations coefficients vary per core segment, therefore a statistical relationship significant for the continuous Bienen coring could not be set up.

Anomalies occur between the plots of the silt and sand grain size fractions and the Zr/Rb plots; some peaks in the Zr/Rb plots are not visible in the grain size data. Possible explanations for these anomalies include the grain size sampling strategy (5.1.1) and the fact that small sandy layers could not be identified as these do not stand out in the grain size average (see 6.1.3). However, the corresponding peaks in both data sets represented some of the major sandy layers and could thus be used to match the data sets.

Making use of the Zr/Rb ratio as a chemical proxy for grain size, and taking into account the shifts that were performed, the flood events (detected in the grain size data) were also identified in the chemical composition data. For the upstream cores, no strong relations were found between grain size data and chemical composition data. This could be explained by the relative low sampling resolution on grain size (and, after bulking) chemical composition data; minor layers could not stand out in averages and were thus not reflected in the plots. As a result, no flood events were identified in the upstream cores.

6.3. Correction of clay content

6.3.1. Correlation matrices

Appendix 1 provides the correlation matrices representing the intercorrelation of elements for each of the core segments based on the non-bulked normalized data as well as the bulked normalized data. Although the first version (non-bulked) has a higher resolution, the correlation of elements is better shown in the bulked version. Therefore, we find the latter in the tables below (Figure 6-11), in which strong correlations are highlighted in orange. Elements Si, Ti and K are strongly correlated in most of the core segments. This group of elements also correlate quite well with elements Fe and Rb. Other correlations include Mn and Fe, and Ca and Sr. However these correlations were not strong in all core segments, i.e. they are not continuous throughout depth.

DICITETT	Si	K	Са	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Bienen 7	Si	K	Ca	Tī	Mn	Fe	Rb	Sr	Zr	Pb
Si	1,000										Si	1,000									
К	0,938	1,000									K	0,489	1,000								
Ca	0,758	0,814	1,000								Ca	0,356	0,071	1,000							
Ti	0,953	0,992	0,775	1,000							Ti	0,611	0,883	-0,007	1,000						
Mn	0,737	0,769	0,730	0,764	1,000						Mn	-0,258	0,134	0,328	-0,009	1,000					
Fe	0,890	0,980	0,771	0,974	0,826	1,000					Fe	-0,134	0,687	0,024	0,486	0,640	1,000				
Rb	0,876	0,959	0,686	0,956	0,653	0,945	1,000				Rb	0,108	0,718	-0,572	0,615	-0,084	0,544	1,000			
Sr	0.560	0.589	0.898	0.538	0.564	0.535	0.466	1.000			Sr	0.499	0.031	0.916	0.035	0.093	-0.148	-0.537	1.000		
Zr	-0,223	-0,495	-0,480	-0,428	-0,384	-0,574	-0,494	-0,348	1,000		Zr	0,468	-0,371	0,106	-0,012	-0,453	-0,754	-0,442	0,330	1,000	
Pb	0.246	0.146	0.070	0.201	0.205	0.111	0.107	0.043	0.483	1.000	Pb	-0.107	0.107	-0.285	0.078	-0.016	0.101	0.218	-0.300	-0.138	1.000
Bienen 4	Si	ĸ	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Bienen 8	Si	K	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb
Si	1,000										Si	1,000									
к	0.885	1.000									к	0.142	1.000								
Ca	0.070	0.009	1.000								Ca	0.102	-0.151	1.000							
Ti	0.889	0.976	-0.053	1.000							Ti	-0.119	0.935	-0.174	1.000						
Mn	0.450	0.427	0.048	0.466	1.000						Mn	-0.045	0.530	0.105	0.515	1.000					
Fe	0.660	0.876	0.071	0.832	0.606	1.000					Fe	-0.256	0.814	-0.138	0.886	0.708	1.000				
Rh	0 729	0.889	-0 137	0.860	0 168	0 729	1 000				Rh	-0 188	0.688	-0 335	0 735	0.259	0 716	1 000			
Sr	0,725	0.050	0.565	0.032	0,277	0,123	-0.239	1.000			Sr	0,100	0 132	0,555	-0.010	0,235	-0 107	-0.359	1.000		
7r	0.185	-0 114	-0 274	0.026	0.002	-0.413	-0.101	-0.105	1 000		7r	0,371	0,006	0 343	0.055	-0.286	-0 225	-0 334	0.435	1 000	
Ph	0,255	0 130	-0.535	0,020	0,002	-0.049	0,101	-0.326	0.611	1.000	Ph	0 104	0,000	-0 192	0,000	0.048	0.122	0,004	-0 222	-0.018	1 000
10	0,235	0,130	-0,555	0,277	0,200	-0,045	0,110	-0,520	0,011	1,000	10	0,104	0,201	-0,152	0,150	0,040	0,122	0,205	-0,222	-0,010	1,000
Bienen 5	Si	K	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Bienen 9	Si	K	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb
Bienen 5 Si	Si 1,000	К	Са	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Bienen 9 Si	Si 1,000	K	Са	Ti	Mn	Fe	Rb	Sr	Zr	Pb
Bienen 5 Si K	Si 1,000 0,723	K 1,000	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Bienen 9 Si K	Si 1,000 0,814	<u>к</u> 1,000	Са	Ti	Mn	Fe	Rb	Sr	Zr	Pb
Bienen 5 Si K Ca	Si 1,000 0,723 -0,066	K 1,000 -0,338	Ca 1,000	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Bienen 9 Si K Ca	Si 1,000 0,814 0,723	К 1,000 0,449	Ca 1,000	Ti	Mn	Fe	Rb	Sr	Zr	Pb
Bienen 5 Si K Ca Ti	Si 1,000 0,723 -0,066 0,721	K 1,000 -0,338 0,920	Ca 1,000 -0,476	Ti 1,000	Mn	Fe	Rb	Sr	Zr	Pb	Bienen 9 Si K Ca Ti	Si 1,000 0,814 0,723 0,790	K 1,000 0,449 0,957	Ca 1,000 0,333	<i>Ti</i> 1,000	Mn	Fe	Rb	Sr	Zr	Pb
Bienen 5 Si K Ca Ti Mn	Si 1,000 0,723 -0,066 0,721 0,138	K 1,000 -0,338 0,920 0,014	Ca 1,000 -0,476 0,418	Ti 1,000 -0,005	Mn 1,000	Fe	Rb	Sr	Zr	Pb	Bienen 9 Si K Ca Ti Mn	Si 1,000 0,814 0,723 0,790 0,479	K 1,000 0,449 0,957 0,579	Ca 1,000 0,333 0,257	Ti 1,000 0,643	<u>Mn</u> 1,000	Fe	Rb	Sr	Zr	Pb
Bienen 5 Si K Ca Ti Mn Fe	Si 1,000 0,723 -0,066 0,721 0,138 0,431	K 1,000 -0,338 0,920 0,014 0,645	Ca 1,000 -0,476 0,418 -0,229	Ti 1,000 -0,005 0,678	Mn 1,000 0,564	Fe	Rb	Sr	Zr	Pb	Bienen 9 Si K Ca Ti Mn Fe	Si 1,000 0,814 0,723 0,790 0,479 0,663	K 1,000 0,449 0,957 0,579 0,933	Ca 1,000 0,333 0,257 0,327	Ti 1,000 0,643 0,923	Mn 1,000 0,757	Fe 1,000	Rb	Sr	Zr	Pb
Bienen 5 Si K Ca Ti Mn Fe Rb	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444	К 1,000 -0,338 0,920 0,014 0,645 0,692	Ca 1,000 -0,476 0,418 -0,229 -0,610	Ti 1,000 -0,005 0,678 0,746	Mn 1,000 0,564 -0,212	Fe 1,000 0,435	Rb	Sr	Zr	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741	K 1,000 0,449 0,957 0,579 0,933 0,963	Ca 1,000 0,333 0,257 0,327 0,402	Ti 1,000 0,643 0,923 0,949	Mn 1,000 0,757 0,589	Fe 1,000 0,936	Rb	Sr	Zr	Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764	Ti 1,000 -0,005 0,678 0,746 -0.459	Mn 1,000 0,564 -0,212 0,367	Fe 1,000 0,435 -0,349	Rb 1,000 -0.588	Sr	Zr	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859	K 1,000 0,449 0,957 0,579 0,933 0,963 0,731	Ca 1,000 0,333 0,257 0,327 0,402 0,879	Ti 1,000 0,643 0,923 0,949 0,665	Mn 1,000 0,757 0,589 0,423	Fe 1,000 0,936 0.638	Rb 1,000 0,740	Sr	Zr	Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128	Ti 1,000 -0,005 0,678 0,746 -0,459 0,135	Mn 1,000 0,564 -0,212 0,367 -0,132	Fe 1,000 0,435 -0,349 -0,302	Rb 1,000 -0,588 -0,038	Sr 1,000 0,303	Zr 1,000	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Zr	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756	K 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460	Ti 1,000 0,643 0,923 0,949 0,665 0,632	Mn 1,000 0,757 0,589 0,423 0,334	Fe 1,000 0,936 0,638 0,396	Rb 1,000 0,740 0,573	Sr 1,000 0,635	Zr 1,000	Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100	K 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254	Ti 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130	Fe 1,000 0,435 -0,349 -0,302 0,369	Rb 1,000 -0,588 -0,038 0,367	Sr 1,000 0,303 -0,253	Zr 1,000 -0,235	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Sr Zr Pb	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756 0,388	K 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057	Ti 1,000 0,643 0,923 0,949 0,665 0,632 0,497	Mn 1,000 0,757 0,589 0,423 0,334 0,377	Fe 1,000 0,936 0,638 0,396 0,366	Rb 1,000 0,740 0,573 0,361	Sr 1,000 0,635 0,201	Zr 1,000 0,531	Pb 1,000
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254	Ti 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130	Fe 1,000 0,435 -0,349 -0,302 0,369	Rb 1,000 -0,588 -0,038 0,367	Sr 1,000 0,303 -0,253	2r 1,000 -0,235	Pb	Bienen 9 Si K Ca Ti Min Fe Rb Sr Zr Pb	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756 0,388	K 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057	Ti 1,000 0,643 0,923 0,949 0,665 0,632 0,497	Mn 1,000 0,757 0,589 0,423 0,334 0,377	Fe 1,000 0,936 0,638 0,396 0,366	Rb 1,000 0,740 0,573 0,361	Sr 1,000 0,635 0,201	Zr 1,000 0,531	Pb 1,000
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 6	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100 Si	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca	Тї 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324 Тї	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	Zr 1,000 -0,235 Zr	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 10	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756 0,388 Si	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382 К	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057 Ca	Ti 1,000 0,643 0,923 0,949 0,665 0,632 0,497 Ti	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn	Fe 1,000 0,936 0,638 0,396 0,366 Fe	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	Zr 1,000 0,531 Zr	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Zr Pb Bienen 6 Si	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,010 Si 1,000	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca	Ті 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324 Ті	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	2r 1,000 -0,235 2r	Pb 1,000	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Zr Zr Pb Bienen 10 Si	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756 0,388 Si 1,000	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,537 0,537 0,537	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057 Ca	Ti 1,000 0,643 0,923 0,949 0,665 0,632 0,632 0,497 Ti	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn	Fe 1,000 0,936 0,396 0,396 0,366 Fe	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	Zr 1,000 0,531 Zr	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 6 Si K	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100 Si 1,000 0,862	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,051 0,287 К 1,000	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca	1,000 -0,005 0,678 0,746 -0,459 0,135 0,324 77	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	2r 1,000 -0,235 2r	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 10 Si K	Si 1,000 0,814 0,723 0,790 0,663 0,741 0,859 0,756 0,388 Si 1,000 0,384	К 1,000 0,449 0,957 0,579 0,933 0,933 0,933 0,731 0,537 0,537 0,537 0,537 0,537 0,537 0,537 0,537	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057 Ca	Ti 1,000 0,643 0,923 0,665 0,632 0,632 0,497 Ti	Mn 1,000 0,757 0,589 0,423 0,334 0,337 Mn	Fe 1,000 0,936 0,638 0,396 0,396 0,366 Fe	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	2r 1,000 0,531 2r	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 6 Si K Ca	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100 Si 0,000 0,100	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К 1,000 -0,209	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca 1,000	π 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	2r 1,000 -0,235 2r	<u>Рb</u> 1,000 Рb	Bienen 9 Si K Ca Ti Min Fe Rb Sr Zr Zr Zr Bienen 10 Si K K Ca	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756 0,388 Si 1,000 0,384 0,111	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382 К К 1,000 0,069	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057 Ca 1,000	Ti 1,000 0,643 0,923 0,949 0,665 0,632 0,497 Ti	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn	Fe 1,000 0,936 0,638 0,396 0,366	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	2r 1,000 0,531 2r	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 6 Si K Ca Ti	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100 Si 1,000 0,862 0,800	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К 1,000 -0,209 0,974	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca 1,000 -0,321	Ti 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324 Ti 1,000	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	2r 1,000 -0,235 2r	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 10 Si K Ca Ti	Si 1,000 0,814 0,723 0,790 0,479 0,633 0,741 0,859 0,756 0,388 Si 1,000 0,384 0,111 0,108	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382 К К 1,000 0,069 0,817	Ca 1,000 0,333 0,257 0,327 0,402 0,402 0,407 0,405 Ca	Ti 1,000 0,643 0,923 0,645 0,632 0,632 0,632 0,497 Ti Ti	Mn 1,000 0,757 0,589 0,423 0,334 0,337 Mn	Fe 1,000 0,936 0,638 0,396 0,366 Fe	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	2r 1,000 0,531 2r	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb Sr Zr Pb Si K Ca Ti Mn	Si 1,000 0,723 -0,066 0,0721 0,138 0,444 -0,128 0,389 0,100 Si 1,000 0,862 0,806 0,806 0,806 0,806	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К 1,000 -0,209 0,974 0,398	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca 1,000 -0,321 -0,068	π 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324 π 1,000 0,342	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn 1,000	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	2r 1,000 -0,235 2r	Pb	Bienen 9 Si K Ca Ti Min Fe Rb Sr Zr Pb Bienen 10 Si K Ca Ti Ti Min	Si 1,000 0,814 0,723 0,790 0,663 0,741 0,859 0,756 0,388 Si 1,000 0,384 0,111 0,0307	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382 К К 1,000 0,069 0,817 0,268	Ca 1,000 0,333 0,257 0,402 0,879 0,460 0,057 Ca 1,000 -0,467 0,100	7i 1,000 0,643 0,923 0,665 0,632 0,497 7i 1,000 0,240	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn 1,000	Fe 1,000 0,936 0,638 0,396 0,366 Fe	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	Zr 1,000 0,531 Zr	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Zr Pb Bienen 6 Si K Ca Ti K Ca Ti Mn Fe	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100 Si 1,000 0,862 0,056 0,800 0,842	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К 1,000 -0,209 0,974 0,398 0,924	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca Ca 1,000 -0,321 -0,068	Ti 1,000 -0,005 0,678 0,746 -0,459 0,135 0,324 Ti 1,000 0,342 0,895	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn 1,000 0,622	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe 1,000	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	2r 1,000 -0,235 2r	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 10 Si Si K Ca Ti Mn Fe	Si 1,000 0,814 0,720 0,790 0,663 0,741 0,859 0,756 0,388 Si 1,000 0,384 0,111 0,108 -0,301	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382 К К 1,000 0,069 0,817 0,268 0,576	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057 Ca 1,000 -0,67 0,100	7i 1,000 0,643 0,923 0,665 0,632 0,497 7i 1,000 0,240 0,596	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn 1,000 0,867	Fe 1,000 0,936 0,638 0,396 0,396 0,366 Fe	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	2r 1,000 0,531 2r	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 6 Si K Ca Ti Mn Fe Rb	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,100 Si 1,000 0,862 0,0565 0,800 0,148 0,692 0,549	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К 1,000 -0,209 0,974 0,398 0,924 0,797	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 -0,254 -0,254 -0,321 -0,068 -0,166 -0,127	π 1,000 -0,005 0,678 0,746 -0,459 0,324 π 1,000 0,342 0,895 0,823	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn 1,000 0,622 0,224	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe 1,000 0,788	Rb 1,000 -0,588 -0,038 0,367 Rb	Sr 1,000 0,303 -0,253 Sr	2r 1,000 -0,235 2r	Pb	Bienen 9 Si K Ca Ca Ti Rb Sr Zr Pb Bienen 10 Si K Ca Ti Mn Fe Rb	Si 1,000 0,814 0,723 0,790 0,663 0,741 0,826 0,756 0,388 Si 1,000 0,384 0,111 0,108 -0,307 -0,340	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382 К К 1,000 0,069 0,817 0,268 0,576 0,645	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057 Ca 1,000 -0,467 0,100 -0,267	77 1,000 0,643 0,923 0,949 0,665 0,632 0,497 77 1,000 0,240 0,596 0,936	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn 1,000 0,867 0,028	Fe 1,000 0,936 0,638 0,396 0,366 Fe 1,000 0,425	Rb 1,000 0,740 0,573 0,361 Rb	Sr 1,000 0,635 0,201 Sr	2r 1,000 0,531 2r	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 6 Si K Ca Ti Mn Fe Rb Si Si Si Si Si Si Si Si	Si 1,000 0,723 -0,066 0,0721 0,138 0,434 0,444 -0,128 0,389 0,100 51 1,000 0,862 0,0566 0,800 0,148 0,652 0,549 0,368	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К К 1,000 -0,209 0,974 0,398 0,924 0,797 0,328	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca Ca 1,000 -0,321 -0,068 -0,166 -0,127 0,059	π 1,000 -0,005 0,678 0,746 0,135 0,324 π 1,000 0,342 0,895 0,298 0,298 0,298	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn 1,000 0,622 0,224 0,240	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe 1,000 0,768 0,272	Rb 1,000 -0,588 -0,038 0,367 Rb	5r 1,000 0,303 -0,253 5r 1,000	2r 1,000 -0,235 2r	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Bienen 10 Si K Ca Ti Mn Fe Rb Sr	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756 0,388 Si 1,000 0,384 0,111 0,108 -0,307 -0,311 -0,050	K 1,000 0,449 0,957 0,537 0,933 0,731 0,537 0,382 1,000 0,069 0,817 0,268 0,576 0,611	Ca 1,000 0,333 0,257 0,402 0,879 0,460 0,057 - - - 0,667 0,100 -0,467 0,100 -0,027 -0,026	77 1,000 0,643 0,943 0,665 0,632 0,655 0,632 0,497 77 77 1,000 0,240 0,596 0,936 0,936	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn 1,000 0,867 0,028 0,005	Fe 1,000 0,936 0,396 0,366 Fe 1,000 0,425 -0,034	Rb 1,000 0,740 0,573 0,361 Rb 1,000 -0,460	Sr 1,000 0,635 0,201 Sr	2r 1,000 0,531 2r	Pb 1,000 Pb
Bienen 5 Si K Ca Ti Mn Fe Rb Si K Ca Ti Bienen 6 Si K Ca Ti Rb Sr Zr	Si 1,000 0,723 -0,066 0,721 0,138 0,431 0,444 -0,128 0,389 0,389 0,100 5i 1,000 0,862 0,056 0,800 0,148 0,692 0,549 0,368 0,0754	К 1,000 -0,338 0,920 0,014 0,645 0,692 -0,443 -0,051 0,287 К 1,000 -0,209 0,974 0,398 0,924 0,797 0,328 -0,130	Ca 1,000 -0,476 0,418 -0,229 -0,610 0,764 0,128 -0,254 Ca Ca 1,000 -0,321 -0,066 -0,127 0,059 -0,121	77 1,000 -0,005 0,678 0,746 0,135 0,324 77 1,000 0,342 0,895 0,823 0,298 0,298	Mn 1,000 0,564 -0,212 0,367 -0,132 0,130 Mn 1,000 0,622 0,224 0,240 -0,578	Fe 1,000 0,435 -0,349 -0,302 0,369 Fe 1,000 0,768 0,272 -0,364	Rb 1,000 -0,588 -0,038 0,367 Rb 1,000 0,048 -0,070	5r 1,000 0,303 -0,253 5r 1,000 0,142	2r 1,000 -0,235 Zr 1,000	Pb	Bienen 9 Si K Ca Ti Mn Fe Rb Sr Zr Pb Bienen 10 Si K Ca Bienen 10 Si K Ca Ti Mn Fe Bienen 10 Si K Ca Zr Pb Sr Zr Zr Pb Si Zr Zr Pb Si Zr Zr Pb Si Zr Zr Pb Si Zr Zr Pb Si Zr Zr Pb Si Zr Zr Pb Si Zr Zr Pb Si Zr Zr Pb Si Zr Zr Zr Pb Si Zr Zr Zr Zr Zr Zr Zr Zr Zr Zr	Si 1,000 0,814 0,723 0,790 0,479 0,663 0,741 0,859 0,756 0,388 0,384 0,111 0,0301 0,301 -0,301 -0,040 -0,293	К 1,000 0,449 0,957 0,579 0,933 0,963 0,731 0,537 0,382 К К 1,000 0,069 0,817 0,268 0,576 0,645 0,011 0,176	Ca 1,000 0,333 0,257 0,327 0,402 0,879 0,460 0,057 Ca 1,000 -0,467 0,100 -0,027 -0,596 0,933 -0,637	7i 1,000 0,643 0,923 0,665 0,632 0,497 7i 1,000 0,240 0,596 0,936 -0,419 0,505	Mn 1,000 0,757 0,589 0,423 0,334 0,377 Mn 1,000 0,867 0,028 0,005	Fe 1,000 0,936 0,336 0,396 0,366 Fe 1,000 0,425 -0,034 -0,323	Rb 1,000 0,740 0,573 0,361 Rb 1,000 -0,460 0,636	5r 1,000 0,635 0,201 5r 1,000 -0,535	2r 1,000 0,531 2r 1,000	Pb 1,000 Pb

Figure 6-10 Correlation matrices for the Bienen cores

These correlation matrices show the intercorrelation of the selected elements of each of the Bienen cores (bulked). Elements that correlate well are highlighted (orange). Appendix 1 provides the raw data.

6.3.2. Al-standardized elemental data

Table 6-10 provides the correlation coefficients for ¹³Al with the clayey grain size classes (< 2 μ m, < 4 μ m, and < 8 μ m)(Appendix 6 provides raw data). Although ¹³Al does not correlate very well with any of the clayey grain size classes, the highest correlation coefficient is that with the class smaller than 8 μ m. Therefore ¹³Al is used as an indicator for the clay content and subsequently it was used to correct the chemical composition correct for the clay content.

Bienen	Grain size: clay classess						
Core segments	< 2 µm	< 4 µm	< 8 µm				
3	0.0120	-0.0189	-0.0300				
4	-0.1563	-0.2107	-0.2259				
5	0.0637	-0.1222	-0.2004				
6	-0.1568	-0.0942	-0.0289				
7	0.0383	0.1553	0.2345				
8	0.2598	0.2234	0.1714				
9	0.1496	0.0905	0.0080				
10	-0.0601	0.0041	0.0259				
Bienen total:	0.1705	0.21800	0.2137				

Figure 6-12 provides the plots of the Zr and Rb counts, corrected by the clay content (i.e. standardized by the Al content), merged to a continuous record of the coring. Appendix 2 provides the raw data of other elemental counts standardized by the Al content (Appendix 5 for the subcatchment cores). The plots are mainly characterized by the amount of Al counts, as we have learned the Zr and Rb counts remain relatively stable in each of the subcatchment cores.



Figure 6-11 Graphs of the Zr and Rb counts.

Plots of element occurrences of Zr and Rb. Left: normalized counts. Right: standardized by Al counts.

6.3.3. Discussion

In this section two methods were applied in order to correct the chemical composition data for clay content. First, correlation matrices for the selected elements for each Bienen core segment indicated that there were no groups of elements that were associated which each other, throughout the Bienen core. Therefore, it was not possible to use such a group of elements in additional statistical methods that can be applied to correct for the clay content (Kylander et al., 2011). Second, the chemical proxy (6.2.2) was used to find the correlation coefficient of Al with the clayey grain size classes. Although Al does not correlate well with the any of the clayey grain size classes, we did use Al to standardize the chemical composition data. No other indicator for the clay content was found, and to be able to trace the origin of flood, the chemical composition of flood events has to be corrected for the clay content.

6.4. Fingerprinting upstream catchments

6.4.1. Handheld XRF data

Appendix 4 provides the data resulting from the handheld XRF scans. Six elements remain usable for further research, these include Sr, Rb, Pb, Zn, Fe and Mn (i.e. these do not the exceed 15% error margin). Elemental occurrence at all locations were plotted on a Rhine kilometers axis and were sorted by subcatchment area.

Figure 6-12 shows the occurrence of the selected elements six elements, Sr, Rb, Pb, Zn, Fe and Mn. The occurrence of Pb shows an interesting trend. The amount of Pb present in the Moselle samples is relatively high compared to the other regions, although there are some variations per location. When the Moselle confluences with the Rhine the amount of Pb present in the Rhine (at 613 km) instantly increases. However, further downstream the amount of Pb decreases. The amount of Pb is influenced by pollution; especially in the catchment of the Moselle the impact of pollution is represented well by an increased occurrence of Pb. The same trend is found in the Zn plots; the amount of Zn in the Moselle. For Zn, we see the same effect (to a lesser extent) after the Main confluences with the Rhine. This might also be due to pollution. The Rb rates remain quite constant throughout the Rhine River course, but the amount of Zr in the Rhine decreases with Rhine while it is relatively low in all of the tributaries. The amount of Zr in the Rhine decreases with Rhine kilometers. The amount of Fe and Mn is too dependent on soil conditions to make any conclusions about changes in presence throughout the Rhine catchment.





Graphs representing the occurrence of the selected six elements (Sr, Rb, Pb, Zn, Fe and Mn) versus Rhine kilometers. In red is the Rhine River (Rhein), green the Moselle River, blue the Main River and yellow the Neckar River. On the vertical axis are the occurrences (in ppm) of the elements, on the horizontal axis are the Rhine kilometers. For the tributaries, this axis represents the relative Rhine kilometers.

6.4.2. Characterizing subcatchments

The tables in 5 provide the characteristic elemental composition for each of the subcatchments. The first part is the data obtained from the XRF scan of the pre-industrial cores (Appendix 5), the second part is the data obtained from the handheld XRF scan performed on the post-industrial samples (Appendix 4 and Appendix 5). Fn and Mn were excluded from the fingerprint (section 6.4.3). Table 6-11 provides the occurrences of the remaining set of elements, which includes Sr, Rb, Pb and Zn.

Table 6-11 Occurrences of trace elements in subcatchments

Occurrences of trace elements, grouped per subcatchment, sampling location and sampling method. Preindustrial cores are in normalized and Al-standardized elemental counts, post-industrial surface samples are in ppm. Raw data are provided in Appendix 5.

		Stan	dardized (Al) element co	ounts
Subcatchment	XRF data used	Sr	Rb	Pb	Zn
	Romerberg	413.8	119.3	10.6	33
Opper Knine	Surface samples	145,8	68,3	65,6	179,5
Nockar	Lauffen	212.3	84.7	5.8	18.2
Neckar	Surface samples	119,4	63,7	43,2	132,0
	Sindlingen	204.8	143.9	29	61.8
Main	Klein Krotzenburg	109.5	128.4	8.3	29.6
	Surface samples	97,7	69,0	46,4	157,4
Massila	Kenn	90.5	135.4	16.6	78.7
woselle	Surface samples	94,7	77,7	103,6	305,1

Based on the results shown in figure 6-11 the following remarks can be made:

- The most upstream subcatchments (Upper Rhine and Neckar) are characterized by a relative high amount of Sr, while the amounts of both Zn and Pb are low to average.
- The amount of Zn increases in downstream direction. Whereas Zn counts are low in the Upper Rhine and Neckar, they are high in the Main and Moselle catchments.
- When we compare the two cores from the Main; we see that the downstream core (Sindlingen) is characterized by much higher amounts of both Pb and Zn. Note that Sindlingen is located downstream of Frankfurt am Main while Klein Krotzenburg is located upstream of this industrialized area.
- The Moselle catchment is characterized by a low amount of Sr and average to high amount Rb. More important are the high amounts of Pb and Zn.

6.4.3. Discussion

To construct a fingerprint for each of the subcatchments, a series of requirements should be satisfied. In this study corings and surface samples were used to determine the chemical composition of floodplain depositions. The interpretation of changes in these chemical composition data solely as a result of changes of the chemical composition of sediment (as deposited in the floodplain) and/or as a results of varying grain size, would be an oversimplification. As stated in chapter 3, the complex patterns caused by both horizontal and vertical processes, might have influenced the results of the chemical composition analysis in the study. By carefully selecting suitable sampling sites, and by using multiple surface samples from each subcatchment, the influence of these processes was

minimized. This way the set of elements do reflect the environmental control. However, the resulting set of elements can barely be regarded a fingerprint as it consists of only 4 trace elements making it hard to be discriminating potential sources.

Although on a Rhine River catchment scale the different source area are only subcatchments, in fact the catchment of these area are enormous. Therefore, the composition of material transported by the tributaries may differ per flooding event. Within each subcatchment another layer of tributaries determines the composition of material that is transported to the point of confluence with the Rhine. This might explain the variation and inconsistency of the composition of a series of floods from a subcatchment. Subsequently it is impossible to set up a fingerprint that is characteristic for a subcatchment.

Lacking a set of fingerprints meeting the criteria (5.2.5), a set of elements was selected that is present in all core material and thus reflects a chemical signal of both the pre- and post-industrial composition. This set of elements, including Sr, Rb, Pb and Zn, represents the chemical composition of the source areas and subsequently, it can be used to correlate with the (characteristic) chemical composition of flood events.

6.5. Tracing flood origin

6.5.1. Characterizing flood events

Six of the floods that were identified in the grain size data (section 6.1) were also identified in the chemical composition data. Table 6-12 shows this subselection of cross-correlated flood events. Note that one of the flood events could not be identified in the chemical composition data. The data of the 1850 A.D. flood event (239 cm) were lost in the shifting process (section 6.2), as this layer was at the bottom of the Bienen 3 core segment. Table 6-11 provides the chemical composition data (selected elements) of the remaining five flood events (Appendix 7 provides raw data).

Table 6-12 Selection of flood events..

Depth (cm)	Core (#)	Flood event (year A.D.)	Sand (%)	Silt+Sand (%)	Zr/Rb
446	Bienen 6	1784	12,63	67,9	1,846883
560	Bienen 7	1729	7,83	65,04	1,42952
564	Bienen 7	1726	8,48	70,58	1,673995
659	Bienen 8	1682	50,39	79,71	1,555375
683	Bienen 8	1671	16,32	63,03	1,400364

Depth	(cm)	Standar	dized (Al)	element	counts.							
Floc	od event											
(ye	ear A.D.)	Si	К	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Zn
446	1784	12,9	142,7	553,5	152,5	95,1	5932,1	135,8	190,9	250,8	15,1	36,5
560	1729	12,6	117,7	314,5	100,7	128,3	4819,8	77,2	87,1	84,5	5,7	21,0
564	1726	19,1	174,0	318,5	159,9	157,9	6868,8	118,1	121,7	133,3	11,2	35,6
659	1682	28,0	296,9	1443,0	249,4	291,3	10020,9	197,2	343,8	306,7	21,0	51,3
683	1671	23,8	276,5	1130,4	243,6	318,9	11027,5	195,4	309,9	273,6	17,0	51,8

Table 6-13 Chemical composition of selected flood events. Appendix 7 provides raw data.

When we take a closer look at table 6-13, the following remarks can be made. The 1784 flood event has average occurrences of Sr, Rb and Zn. The flood events from the years 1729 and 1726 sow a similar pattern: both have relatively low Sr occurrence and relatively high Zn occurrence. Rb occurrences are average for these flood events. The last two flood events (1682 and 1671) both have a relatively high Sr occurrence, Rb and Zn occurrences are average.

Table 6-14 Occurrence of trace elements in flood events

Occurrence of trace elements in percentage for each of the historical flood events that we could correlate with the elemental data using the Zr/Rb ratio.

	Corresponding flood event	Elemental cou	nts (normalized	, Al-standard	lized)
Depth (cm)	(year A.D.)	Sr	Rb	Pb	Zn
446	1784	190,9	135,8	15,1	36,5
560	1729	87,1	77,2	5,7	21,0
564	1726	121,7	118,1	11,2	35,6
659	1682	343,8	197,2	21,0	51,3
683	1671	309,9	195,4	17,0	51,8

6.5.2. Allocating flood origins

When we compare the characteristic catchment compositions (table 5-12) with the characteristic flood composition (table 6-14) the following conclusions can be drawn concerning the allocation of flood origins:

- The combination of high values for Sr with low values for Pb and Zn, suggests that both the 1671 and the 1682 floods have an origin high upstream in the Rhine catchment; the sediment is likely to be deposited during floods originating from the Upper Rhine and Neckar.
- The combination of low Sr values and high Zn values suggest that both the 1726 and the 1729 floods are mainly composed by Moselle sediment; this sediment is likely to be deposited by a flood consisting of a high discharge from the Moselle catchment.

6.5.3. Discussion

Making use of a chemical proxy, the chemical compositions of the selected flood events (6.1 and 6.2) were obtained. These data were compared to the specific chemical composition of each of the subcatchments, which was reflected in the occurrences of a selected set of elements. Subsequently an attempt was made to allocate each of the flood events to one of the subcatchments. As no real fingerprints were set up, this comparison was based on the occurrences of a set of only four elements. These sets of elements were not sufficient to make any distinct remarks about the chemical composition of the flood events, only some minor variations were detected (6.4).

The selected trace elements could not characterize the flood events, as the variations of presence in the flood events were too low. Moreover, in some cases an inconsistent amount of these elements were present when the standardized with the normalized data are compared. The latter is due to the standardization method that was used (6.3).

It was thus not possible to quantitatively locate the flood origins. Consequently, it was not possible to unravel the mixed contribution of the subcatchment to each of the floods. However, some remarks were made about the (partial) contribution of tributaries to the flood events. Although a system was developed in which the composition of downstream deposited sediment was compared with "fingerprints" of upstream source areas, both the downstream flood signal, and the upsteam source area signals, could not be characterized distinctively. Therefore this system was not able to provide an estimate of the relative contributions of the source areas (subcatchments).

However, the chemical composition of sediment deposited during flood events along the Lower Rhine, is not only built up by its main tributaries. Although the Upper Rhine, Neckar, Main and Moselle largely determine the chemical composition of the sediment, there also a series of minor tributaries that confluence with the Rhine River on it way downstream. These tributaries dilute the Rhine discharge and can therefore cause additional variations in flood deposits along the Lower Rhine.

7. Conclusions and recommendations

Making use of historical sources and grain size analysis on the Bienener Altrhein palaeo-fill, a series of major flood events was identified. Together with knowledge obtained from previous research, the chemical composition of this core was used to set up a proxy for grain size. Analysis of the Bienener Althrein coring has shown that Zr/Rb is a suitable proxy for grain size in flood plain sediments. When looking at the separate Bienen core segments and taking into account minor shifts, most of the peaks in the grain size data had a corresponding peak area in the Zr/Rb ratio data. These correlations were recorded in correlation coefficients, resulting in a qualitative relationship per core segments. However, to set up a qualitative relation for the whole core, instead of for the separate Bienen segments, a standardization method needs to be found to correct for the varying settings for each of the core segments.

In this study it is proved that chemical composition data can be used to derive grain size peaks from (and flood events, Winkels, 2011; Aloserij, 2013). This relationship was quantified by means of the Zr/Rb ratio as proxy. Combined with previous research (Aloserij, 2011; Toonen, 2013) Zr/Rb profiles can be used to reconstruct a history of flood events at flood plain sites with high resolution deposits (slack water environments). However, a more detailed (higher resolution) grain size analysis needs to be performed to detect all (minor) sandy layers and create a continuous flood record in the data set. Moreover, better results can be obtained by improving the sampling method.

No adequate method was found to standardize the data for clay content. By correcting the chemical composition for clay content, all cores can be filtered by the clayey grain size fractions, enabling a comparison between downstream and upstream flood deposits. Two methods were applied in order to find a way to correct for the clay content. First, the construction of correlation matrices did not results in any group of elements that clustered throughout the Bienen core. The other method, involved the correlation of Al with the clayey grain size fractions and use this relation to correct for the clay content. Although, the relation of Al with clay, qualified with correlation coefficients, was not good, we have used this standardization method. A better standardization method, is of vital importance for the succeeding of the second part of this research. Therefore, additional research is needed to set up an adequate standardization method.

The next part of this research included the characterization of the subcatchments. Based on the corings and surface samples, we characterized each of the subcatchments. Although there were some minor differences in the chemical composition of the different subcatchment, it was not possible to set up characteristic fingerprints for the subcatchments. However, based on set of

elements that occurred in both the scores and the surface samples, some remarks were made regarding the characteristics of the subcatchments. The Upper Rhine and the Neckar are characterized by a high amount of Sr and low to average amounts of Zn and Pb. Moreover, sediment deposited by the Moselle is characterized by a low amount of Sr and high amounts of Pb and Zn.

Making use of the Zr/Rb ratio as a proxy, selected flood events were detected in the normalized and standardized (i.e. corrected for the clay content) chemical composition data. Although the variation of presence of these elements in the flood events was not high, a few remarks could be made regarding the characterization of these flood events. The flood events from the years 1729 and 1726 both have relatively low Sr occurrence, while the two flood events from the years 1682 and 1671 both have a relatively high Sr occurrence.

The combination of the characterizations of the subcatchments and the floods have led to the following suggestions: (1) the 1671 and 1682 floods are likely to have and origin in the Upper Rhine and Neckar catchments (due to high Sr values combined with low Pb and Zn values), and (2) the 1726 and 1729 floods are likely to originate from the Moselle catchment (due to the combination of low Sr values and high Zn values). Whereas we aimed for a quantitative calculation of the contribution to floods from each of the subcatchments, we can conclude that for now only a qualitative contribution can (partially) be obtained.

An additional conclusion can be made regarding pollution, which specifically had its effect on the sediment transported by the Mosell. Pb (and Zn) occurrences in the Moselle are higher than in the other tributaries. These results were found in the data from the cores and in the handheld XRF data. The coring performed at the Sindlingen location, downstream of Frankfurt am Main, has higher amounts of Pb and Zn compared to the coring upstream of Frankfurt am Main (Klein Krotzenburg); the pollution from the industrialized area around the city of Frankfurt is thus reflected in the chemical composition of floodplain deposits.

This study was performed in the floodplains of the Lower Rhine and its tributaries in the Netherlands and Germany. The research area is therefore focused on a moderate to long meandering river with a mixed load and its tributaries, while previous studies on a similar topic (based on the infill of cut-off meanders) were performed on a much smaller scale (Peart and Walling, 1986; Passmore and Macklin, 1994). The results of this study, i.e. the relation between the Zr/Rb ratio and grain size and the (quantitative) relation used to allocate flood origin, have yet to be applied in other study areas. Different results might be expected for sedimentary environments with another drainage basin, climate settings, river valley morphology and sediment transported. A last recommendation for further research includes the investigation of historic sources. Besides of the historic sources describing flood events in the Rhine River, flood propagation throughout the Rhine catchment should be mapped. Analysis of historic sources from each of the tributaries can be used to map flood events throughout the subcatchments. Combining flood propagation of each of the subcatchments in a model, will create an overview of flood propagation throughout the Rhine catchment.

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Appendices

Appendix 1 (A-H) Raw data from grain size and XRF scans (sorted by segment)Appendix 2 Normalized counts of selected elementsAppendix 3 Sampling locationsAppendix 4 Handheld XRF elemental countsAppendix 5 Normalized and standardized data for subcatchment coresAppendix 6 Al standardization Bienen CoresAppendix 7 Flood event dataAppendix 8 Correlation of grain size with Zr/Rb ratio (Bienen)Appendix 9 Correlation of grain size with Zr/Rb ratio (Subcatchments)Appendix 10 Standardized elemental data BienenAppendix 11 XRF settings

Appendix 1 - Bienen 10 B																											
Depth	Real dept	h %Clay	%Very Fine	%Fine Silt	%Coarse 5	%Very Fine?	%Fine San %	Middle C%	Coarse 5%	Very Coars	e Sand							Original					Shifted gra	ph			
		< 8 才m	8-16 † m	16-32 † m	32-63 fm (63-125 才m '	125-250 † n 25	50-500 オn 50	00-1000 110	00-2000 CI	ay S	ilt S	and	>8um	>16um	>32um	>64um	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
81	9 81	9 47.93	3 20.74	19.09	9.79	2.04	0.41	0	0	0	47.93	49.62	2.45	52.07	7 31.33	3 12.24	2.4	1.298183	32.2657	235.343	235.4541	1.000472	1.276342	15.42523	108.8621	110.7734	1.017556
82	1 82	47.3	7 20.22	19.16	9.63	2.75	0.87	0	0	0	47.37	49.01	3.62	52.63	3 32.41	13.25	3.62	1.276342	15.42523	108.8621	110.7734	1.017556	1.259673	16.88146	125.462	122.8967	0.97955
82	3 82	51.08	3 22.25	17.09	7.26	1.94	0.38	0	0	0	51.08	46.6	2.32	48.92	2 26.67	9.58	2.32	1.259673	16.88146	125.462	122.8967	0.979553	1.148672	18.2129	135.2645	126.7097	0.936755
82	5 82	43.64	4 18.79	17.91	11.18	4.43	2.49	1.55	0	0	43.64	47.88	8.48	56.35	5 37.56	5 19.65	8.48	1.148672	18.2129	135.2645	126.7097	0.936755	1.252195	17.71703	117.1923	114.8132	0.979699
82	7 82	7 46.44	4 18.85	18.09	11.49	4	1.1	0.03	0	0	46.44	48.43	5.13	53.56	5 34.71	16.62	5.13	1.252195	17.71703	117.1923	114.8132	0.979699	1.650056	25.01639	153.2295	250.0601	1.631932
82	9 82	9 52.6	6 19.89	16.63	7.91	2.55	0.43	0	0	0	52.6	44.42	2.98	47.41	1 27.52	10.89	2.98	1.650056	25.01639	153.2295	250.0601	1.631932	1.297267	23.209	161.6238	165.4244	1.023515
83	1 83	46.18	3 18.75	19.88	12.17	2.91	0.11	0	0	0	46.18	50.8	3.02	53.82	2 35.07	15.19	3.02	1.297267	23.209	161.6238	165.4244	1.023515	1.187727	18.72619	116.0446	112.9613	0.97343
83	3 83	3 47.1	1 19.77	18.79	10.85	3.32	0.18	0	0	0	47.1	49.4	3.5	52.91	1 33.14	14.35	3.5	1.187727	18.72619	116.0446	112.9613	0.97343	1.285529	25.292	154.92	162.424	1.048438
83	5 83	5 44.84	4 18.92	16.48	10.55	3.59	1.64	3.83	0.14	0	44.84	45.96	9.21	55.15	5 36.23	19.75	9.2	1.285529	25.292	154.92	162.424	1.048438	1.344235	21.34146	122.1433	134.8293	1.10386
83	7 83	7 45.29	9 20.49	16.95	9.65	3.02	1.33	3.08	0.19	0	45.29	47.09	7.62	54.71	1 34.22	17.27	7.62	1.344235	21.34146	122.1433	134.8293	1.103861	1.348158	24.54579	126.0916	144.2381	1.14391
83	9 83	9 49.62	2 21.93	18.29	8.64	1.52	0.01	0	0	0	49.62	48.86	1.53	50.39	9 28.46	5 10.17	1.53	1.348158	24.54579	126.0916	144.2381	1.143915	1.232656	15.46953	102.4492	102.7946	1.00337
84	1 84	1 45.8 ⁻	1 19.34	18.99	11.82	3.63	0.41	0	0	0	45.81	50.15	4.04	54.19	9 34.85	5 15.86	4.04	1.232656	15.46953	102.4492	102.7946	1.003371	1.449206	24.16054	145.796	168.2776	1.154199
84	3 84	3 42.4	5 19.86	20.51	13.1	3.77	0.32	0	0	0	42.45	53.46	4.09	57.56	5 37.7	7 17.19	4.09	1.449206	24.16054	145.796	168.2776	1.154199	1.682148	23.30435	150.3288	185.6168	1.234739
84	5 84	5 36.93	3 18.43	22.21	17.04	5.01	0.38	0	0	0	36.93	57.68	5.4	63.07	7 44.64	22.43	5.4	1.682148	23.30435	150.3288	185.6168	1.234739	1.289475	17.80046	104.5092	105.6009	1.010446
84	7 84	7 51.59	9 22.57	16.85	7.14	1.65	0.21	0	0	0	51.59	46.55	1.86	48.42	2 25.85	; 9	1.86	1.289475	17.80046	104.5092	105.6009	1.010446	1.438752	30.23396	110.7094	146.0415	1.319142
84	9 84	9 32.78	3 14.11	12.35	7.82	3.38	2.44	12.71	14.05	0.36	32.78	34.28	32.94	67.22	2 53.11	40.76	32.94	1.438752	30.23396	110.7094	146.0415	1.319142					

	Original					Shifted				
	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
>8um	0.28399	0.352758	-0.05605	-0.00959	0.133732	0.221663	-0.18845	-0.20324	-0.07548	0.009488
>16um	0.274286	0.3675	-0.05816	0.017674	0.182604	0.226339	-0.17165	-0.10618	-0.00532	0.028711
>32um	0.218542	0.399188	-0.13576	-0.01443	0.241181	0.236918	-0.07363	-0.05624	0.055359	0.087992
>64um	0.13276	0.411224	-0.20095	-0.04766	0.27932	0.132516	0.041891	-0.01523	0.061863	0.09155

 >8um
 >16um
 >32um
 >64um

 Original
 Original
 0.28399
 0.274286
 0.218542
 0.13276

 Shifted
 0.221663
 0.226339
 0.236918
 0.132516

Appendix 1	- Bienen 10	A (
Depth	Real depth	%Clay	%Very Fine	%Fine Silt	%Coarse S	%Very Fine	%Fine San	%Middle C	%Coarse S	%Very Coa	arse Sand											
		< 8 †m	8-16 † m	16-32 † m	32-63 オm	63-125 fm	125-250 fn:	250-500 オn	500-1000 オ	1000-2000	Clay	Silt	Sand	P95								
819	819	47.93	20.74	19.09	9.79	2.04	0.41	0	0	0	47.93	49.62	2.45	44.2								
821	821	47.37	20.22	19.16	9.63	2.75	0.87	0	0	0	47.37	49.01	3.62	52.6								
823	823	51.08	22.25	17.09	7.26	1.94	0.38	0	0	0	51.08	46.6	2.32	44.2								
825	825	43.64	18.79	17.91	11.18	4.43	2.49	1.55	0	0	43.64	47.88	8.48	88.4								
827	827	46.44	18.85	18.09	11.49	4	1.1	0.03	0	0	46.44	48.43	5.13	62.5								
829	829	52.6	19.89	16.63	7.91	2.55	0.43	0	0	0	52.6	44.42	2.98	44.2								
831	831	46.18	18.75	19.88	12.17	2.91	0.11	0	0	0	46.18	50.8	3.02	52.6								
833	833	47.1	19.77	18.79	10.85	3.32	0.18	0	0	0	47.1	49.4	3.5	52.6								
835	835	44.84	18.92	16.48	10.55	3.59	1.64	3.83	0.14	0	44.84	45.96	9.21	149								
837	837	45.29	20.49	16.95	9.65	3.02	1.33	3.08	0.19	0	45.29	47.09	7.62	88.4								
839	839	49.62	21.93	18.29	8.64	1.52	0.01	0	0	0	49.62	48.86	1.53	37.2								
841	841	45.81	19.34	18.99	11.82	3.63	0.41	0	0	0	45.81	50.15	4.04	52.6								
843	843	42.45	19.86	20.51	13.1	3.77	0.32	0	0	0	42.45	53.46	4.09	52.6								
845	845	36.93	18.43	22.21	17.04	5.01	0.38	0	0	0	36.93	57.68	5.4	62.5								
847	847	51.59	22.57	16.85	7.14	1.65	0.21	0	0	0	51.59	46.55	1.86	37.2								
849	849	32.78	14.11	12.35	7.82	3.38	2.44	12.71	14.05	0.36	32.78	34.28	32.94	595								
		Al	Si	Р	S	CI .	Ar	к	Ca	Sc	Ti	v	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	As	
819	819	0.000201	0.006477	6.5E-05	0.001075	1.45E-05	0.003889	0.05333	0.167933	2.04E-05	0.047245	0.001403	0.002853	0.056338	2.089301	0.020132	0.000522	9.02E-05	0.010516	0.00231	0.004685	
821	821	0.00041	0.006329	6.23E-05	0.00102	1.44E-05	0.002653	0.050412	0.188939	6.71E-06	0.044665	0.001415	0.002536	0.054269	1.958427	0.018576	0.000706	0	0.010374	0.001823	0.004276	
823	823	0.000353	0.005957	8.26E-05	0.000959	3.11E-05	0.001602	0.051351	0.235237	4.29E-05	0.044269	0.001698	0.002439	0.052458	2.013875	0.019069	0.000355	0	0.010294	0.001801	0.005082	
825	825	0.000317	0.005766	4.9E-05	0.00118	2.55E-05	0.002017	0.052016	0.363842	5.21E-05	0.04282	0.001776	0.002491	0.061671	2.193707	0.022047	0.000571	4.08E-06	0.010362	0.001952	0.006203	
827	827	0.000373	0.006617	9.23E-06	0.001114	9.23E-06	0.001878	0.053789	0.404387	5.23E-05	0.043771	0.001317	0.002663	0.04898	2.00262	0.019811	0.000684	0	0.009895	0.001759	0.005379	
829	829	0.000217	0.005436	0.000113	0.000879	5.46E-05	0.002957	0.03904	0.231835	4.63E-05	0.033295	0.001132	0.001914	0.020437	1,255493	0.01437	0.000951	0.000131	0.008175	0.001972	0.003573	
831	831	0.000295	0.006841	2 27E-05	0.000995	0	0.002598	0.057558	0 300915	8 25E-05	0.047642	0.001781	0.002752	0.039609	1 836755	0.018829	0.001166	6 73E-05	0.010421	0.002987	0.004409	
833	833	0.000233	0.006439	4 2E-05	0.000923	1 74E-05	0.002000	0.054316	0.506875	7.06E-05	0.039901	0.001666	0.002356	0.049257	1 869213	0.01884	0.001111	3.48E-05	0.009551	0.002005	0.003242	
935	925	0.000256	0.006479	2 465-05	0.000020	2.46E-05	0.003257	0.052017	0.503006	8 2E-06	0.030697	0.001502	0.002350	0.051514	1 959592	0.018246	0.001044	0.402 05	0.0000000	0.001703	0.003242	
035	035	0.000230	0.000475	2.40L-05	0.0000071	2.401-05	0.003237	0.032517	0.365556	2 45 05	0.035007	0.001333	0.002402	0.051514	1.030302	0.010240	0.001274	2 915 05	0.000069	0.001703	0.004455	
000	037	0.000310	0.000732	1 095 05	0.001045	1 255 05	0.003200	0.040074	0.417593	6 77E OF	0.03007	0.001716	0.002013	0.034213	1 700007	0.015005	0.001374	6 2EE 06	0.0000000	0.002014	0.004663	
035	035	0.000284	0.000570	1.560-05	0.00105	1.550-05	0.002804	0.045074	0.417362	0.77E=03	0.055650	0.001/10	0.00205	0.049605	1.005035	0.010902	0.000700	0.232*00	0.008037	0.002209	0.004302	
841	841	0.000428	0.006616	4.15E-05	0.000957	0	0.001932	0.055805	0.379399	5.0E-U5	0.043815	0.001437	0.002495	0.040696	1.895825	0.019029	0.001082	0	0.010218	0.002539	0.003476	
843	843	0.000301	0.007283	4.34E-05	0.001161	5.04E-06	0.00233	0.054146	0.371387	4.23E-05	0.043952	0.001595	0.002575	0.040812	1.775632	0.018479	0.001081	0	0.010457	0.002098	0.004325	
845	845	0.000357	0.00833	6.6E-05	0.000935	0	0.001609	0.059978	0.184125	0	0.053732	0.00186	0.00275	0.03644	1.749882	0.017472	0.000848	3.98E-05	0.010374	0.002551	0.005377	
847	847	0.00042	0.007475	5.78E-06	0.001016	2.7E-05	0.002301	0.056643	0.399551	0	0.043886	0.001645	0.00229	0.038514	1.832444	0.01795	0.001138	0	0.010414	0.002039	0.004661	
849	849	0.000284	0.008581	6.53E-05	0.006251	1.71E-05	0.003295	0.046844	0.405883	1.61E-05	0.031423	0.001085	0.001926	0.033836	1.375648	0.013627	0.001202	0	0.007559	0.002126	0.005023	
		~			~	_		~ .	~	~			-									. (0)
		se	Br	KD	Sr	Zr i	Ag		Sn	50	LS -	ва	1a	w	Ir	AU	Hg	PD	D1	MO INC	Mocon	Zr/RD
819	819	0.004245	0.000841	0.036411	0.045868	0.047268	0.000327	0.000414	0.000928	0.000683	0	0.00095	0.004815	0.008363	0.001684	0.004511	0.003908	0.003505	0.003712	0.751156	0.248844	1.298183
821	821	0.004968	0.001397	0.035609	0.047473	0.045449	0.000688	0.000284	0.001219	0.00113	0	0.000659	0.005401	0.008445	0.001961	0.004435	0.00394	0.003978	0.003565	0.753818	0.246182	1.276342
823	823	0.004608	0.000494	0.034424	0.054448	0.043364	0.000/16	0.000177	0.001454	0.001755	0	0.000464	0.004978	0.00811	0.001602	0.004379	0.003695	0.003328	0.003761	0.74692	0.25308	1.259673
825	825	0.004859	0.001436	0.03492	0.06/05/	0.040112	0.000433	0.00035	0.002145	0.003328	0	0.000536	0.005298	0.008381	0.001732	0.005159	0.004323	0.003232	0.004586	0.743527	0.256473	1.148672
827	827	0.004985	0.001114	0.034246	0.069705	0.042882	0.000608	0.000317	0.002231	0.003579	0	0.000428	0.005176	0.009108	0.001799	0.005089	0.003926	0.002983	0.004186	0.741706	0.258294	1.252195
829	829	0.00393	0.001041	0.032929	0.062205	0.054335	0.000651	0.000221	0.001143	0.002294	8.31E-06	0.000706	0.004213	0.007366	0.001607	0.004627	0.003827	0.003366	0.002273	0.742686	0.257314	1.650056
831	831	0.004113	0.000682	0.037588	0.061345	0.048762	0.000613	0.000201	0.001652	0.002199	0	0.000907	0.005122	0.010124	0.001136	0.00433	0.004207	0.004083	0.003559	0.746383	0.253617	1.297267
833	833	0.004222	0.001308	0.032702	0.078397	0.038841	0.000581	0.000273	0.002638	0.004301	0	0.00048	0.004593	0.009169	0.001383	0.004349	0.003629	0.003809	0.003349	0.741524	0.258476	1.187727
835	835	0.004931	0.001217	0.032367	0.080483	0.041609	0.000283	0.000423	0.002718	0.004416	0	0.000482	0.004909	0.009114	0.001703	0.005028	0.004191	0.002984	0.003868	0.741073	0.258927	1.285529
837	837	0.004452	0.000508	0.03192	0.062826	0.042908	0.000332	0.000375	0.001802	0.00321	0	0.00091	0.005431	0.00992	0.001261	0.004612	0.0039	0.003684	0.003087	0.744902	0.255098	1.344235
839	839	0.004431	0.000936	0.030407	0.067656	0.040993	0.000204	0.000386	0.00199	0.003397	0	0.000507	0.004978	0.008862	0.000949	0.004848	0.004263	0.003112	0.003629	0.744138	0.255862	1.348158
841	841	0.004362	0.001205	0.035665	0.069352	0.043963	0.000359	0.000348	0.002005	0.003045	0	0.000639	0.004684	0.008804	0.001045	0.004501	0.003932	0.004185	0.002983	0.746315	0.253685	1.232656
843	843	0.004083	0.000773	0.035005	0.066351	0.050729	0.000257	0.000313	0.001823	0.003022	0	0.001032	0.004649	0.009528	0.001051	0.004667	0.003895	0.003151	0.003743	0.743715	0.256285	1.449206
845	845	0.003649	0.000648	0.03944	0.047814	0.066344	0.000498	0.000262	0.000894	0.00084	0	0.001212	0.005011	0.009857	0.001397	0.004381	0.003818	0.003597	0.003465	0.7521	0.2479	1.682148
847	847	0.004662	0.001068	0.034389	0.068279	0.044344	0.000353	0.000308	0.001658	0.003346	0	0.000626	0.004949	0.008863	0.001638	0.004811	0.004527	0.003648	0.004638	0.744958	0.255042	1.289475
849	849	0.004219	0.000523	0.028811	0.060055	0.041451	0.000419	0.00034	0.00193	0.003542	0	0.000687	0.004013	0.008853	0.001335	0.004892	0.004401	0.002782	0.002549	0.743086	0.256914	1.438752

Appendix	1 - Bienen 9 I	В																				
Depth	Real depth	%Clay	%Very Fine	%Fine Silt	%Coarse S%	6√ery Fine%	%Fine San %	Middle C%Co	oarse S%	Very Coars	e Sand							Original (-la	ast)			
		< 8 才m	8-16 才m	16-32 † m	32-63 tm 6	i3-125 才m 1	125-250 才n 25	0-500 才n 500-	-1000 \$ 10	000-2000 C	ay Silt	t S	and	>8um	>16um	>32um	>64um	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
737	7 721	49.88	21.38	17.07	8.25	2.84	0.57	0	0	0	49.88	46.7	3.42	50.11	28.73	11.66	3.42	1.271767	20.48503	156.479	185.2515	1.183874
739	723	49.55	20.81	17.12	8.91	3.06	0.55	0	0	0	49.55	46.84	3.61	50.45	29.64	12.52	3.61	1.090349	13.82236	88.51896	75.27545	0.850388
743	726	50.19	23.57	16.41	7.22	2.27	0.35	0	0	0	50.19	47.19	2.62	49.82	26.25	9.84	2.62	1.080732	31.71176	217.3941	187.9647	0.864626
743	3 728	50.22	22.64	16.18	7.62	2.76	0.57	0	0	0	50.22	46.44	3.34	49.77	27.13	10.95	3.34	1.055215	15.91922	117.5376	101.1448	0.860532
745	5 731	53.66	23.62	16.08	5.1	1.2	0.34	0	0	0	53.66	44.79	1.55	46.34	22.72	6.64	1.55	1.056821	18.60526	122.8589	97.311	0.792055
747	7 733	52.12	24.9	17.05	5.14	0.68	0.1	0	0	0	52.12	47.1	0.78	47.87	22.97	5.92	0.78	1.058496	14.712	108.188	86.568	0.800163
749	735	51.36	25.49	16.06	5.47	1.33	0.29	0	0	0	51.36	47.02	1.62	48.64	23.15	7.09	1.62	0.942748	17.20988	139.758	95.46667	0.683085
753	738	56.27	20.73	14.84	6.26	1.55	0.35	0	0	0	56.27	41.83	1.9	43.73	23	8.16	1.9	0.961294	14.2354	103.8248	73.55657	0.708468
753	3 740	52.74	23.18	16.04	6.04	1.61	0.4	0	0	0	52.74	45.25	2.01	47.27	24.09	8.05	2.01	0.969979	14.5823	104.3539	79.04527	0.757473
755	5 743	52.98	23.57	16.73	5.49	1	0.22	0	0	0	52.98	45.79	1.22	47.01	23.44	6.71	1.22	0.964051	18.59211	141.9316	104.0237	0.732914
757	7 745	47.97	24.33	19.14	6.89	1.36	0.3	0	0	0	47.97	50.36	1.67	52.02	27.69	8.55	1.67	0.956844	16.8186	129.1651	90.85349	0.70339
759	9 747	55.16	20.74	15.42	6.87	1.6	0.22	0	0	0	55.16	43.03	1.81	44.85	24.11	8.69	1.81	1.022077	14.36257	114.2144	83.02729	0.726942
763	750	66.83	19.77	10.58	2.78	0.04	0	0	0	0	66.83	33.13	0.04	33.17	13.4	2.82	0.04	1.046001	17.95735	139.9882	104.7488	0.748269
763	3 752	67.1	18.94	10.17	2.79	0.68	0.32	0	0	0	67.1	31.9	1	32.9	13.96	3.79	1	0.739905	15.52902	120.308	72.76339	0.604809
765	5 755	58.79	21.54	13.1	4.75	1.37	0.45	0	0	0	58.79	39.39	1.82	41.21	19.67	6.57	1.82	0.848911	17.72953	126.4417	89.20099	0.705471
767	7 757	56.38	22.6	13.81	5.46	1.42	0.32	0	0	0	56.38	41.88	1.74	43.61	21.01	7.2	1.74	0.918139	15.54279	115.3178	88.30073	0.765716
769	9 759	59.9	21.95	13.04	3.8	0.78	0.53	0	0	0	59.9	38.79	1.31	40.1	18.15	5.11	1.31	0.861406	21.39519	166.6907	120.3333	0.721896
77:	762	55.28	23.95	14.51	5.02	1.01	0.23	0	0	0	55.28	43.49	1.23	44.72	20.77	6.26	1.23	0.908895	14.75506	114.9124	82.36629	0.716775
773	3 764	52.44	22.57	16.19	6.86	1.58	0.35	0	0	0	52.44	45.62	1.94	47.55	24.98	8.79	1.94	0.901318	13.26531	101.4143	73.98163	0.729499
775	5 767	55.48	22.61	14.73	5.67	1.23	0.27	0	0	0	55.48	43.02	1.5	44.51	21.9	7.17	1.5	0.97168	18.70326	141.4095	110.2611	0.779729
77	7 769	55.11	21.35	15.89	5.9	1.22	0.54	0	0	0	55.11	43.13	1.77	44.9	23.55	7.66	1.77	0.896982	19.9746	138.8984	106.5302	0.766965
779	9 771	41.21	19.87	21.69	12.51	3.93	0.79	0	0	0	41.21	54.07	4.72	58.79	38.92	17.23	4.72	1.157215	17.29537	87.41313	81.82046	0.93602
78:	. 774	60.98	21.73	12.01	3.79	1.06	0.43	0	0	0	60.98	37.53	1.49	39.02	17.29	5.28	1.49	0.863146	15.20899	104.3191	77.64045	0.744259
783	3 776	55.93	21.27	14.59	6.08	1.79	0.35	0	0	0	55.93	41.94	2.14	44.08	22.81	8.22	2.14	0.961182	15.20042	98.13987	79.50522	0.810121
785	5 779	52.67	20.83	16.22	7.87	2.09	0.32	0	0	0	52.67	44.92	2.42	47.33	26.5	10.28	2.42	0.922463	16.25159	103.7844	77.49471	0.74669
78.	781	57.26	22.23	14.74	4.88	0.89	0.01	0	0	0	57.26	41.85	0.89	42.75	20.52	5.78	0.89	0.856417	15.1299	102.9134	72.27629	0.702302
789	9 783	59.66	22.31	13.97	4.01	0.05	0	0	0	0	59.66	40.29	0.05	40.34	18.03	4.06	0.05	1.070348	15.91105	102.5094	94.61186	0.922958
793	786	54.76	21.16	15.38	6.38	1.9	0.42	0	0	0	54.76	42.91	2.33	45.24	24.08	8.7	2.33	0.940608	17.13333	113.8833	85.06905	0.746984
793	8 788	56.53	21.57	14.68	5.69	1.36	0.16	0	0	0	56.53	41.94	1.53	43.46	21.89	7.21	1.53	0.923965	16.94272	118.463	86.94749	0.733963
795	5 791	48.64	25.14	18.44	6.45	1.15	0.19	0	0	0	48.64	50.03	1.33	51.37	26.23	7.79	1.33	0.911503	23.01338	158.5318	118.7057	0.748782
/9.	/ /93	54.75	21.24	15.63	6.62	1.49	0.26	0	0	0	54.75	43.49	1.76	45.24	24	8.37	1.76	1.070542	18.745	122.47	101.3	0.82/141
/99	9 /95	55.75	21.1	14.91	6.31	1.67	0.25	0	0	0	55.75	42.32	1.93	44.24	23.14	8.23	1.93	0.9/39/3	16.77488	119.6493	93.109	0.778183
802	/98	51.55	20.69	17.26	8.61	1.85	0.04	0	0	0	51.55	46.56	1.89	48.45	27.76	10.5	1.89	0.93043	14.27766	97.58664	/3.51566	0.753337
803	8 800	52.37	21.51	17.37	6.78	1.4	0.57	0	0	0	52.37	45.65	1.97	47.63	26.12	8.75	1.97	0.873183	14.54776	102.115	70.12865	0.686761
805	803	60.5	21.19	13.39	4.38	0.53	0.01	0	0	0	60.5	38.95	0.55	39.5	18.31	4.92	0.55	0.996296	17.63679	123.1415	91.99292	0.74705
807	805	56.59	23.39	14.89	4.51	0.57	0.05	0	0	0	56.59	42.79	0.62	43.41	20.02	5.13	0.62	1.065793	18.1945	112.1818	88.56448	0.789473
809	807	49.77	22.75	18.26	7.38	1.58	0.27	0	0	0	49.77	48.39	1.85	50.24	27.49	9.23	1.85	1.112171	20.70055	127.3599	108.8736	0.85485
811	810	43.95	21.15	21.1	11.32	2.42	0.07	0	0	0	43.95	53.57	2.48	56.06	34.91	13.81	2.48	1.314516	20.06667	101.1379	104.1701	1.029981
813	8 812	45.8	21.21	20.39	10.44	2.11	0.05	0	0	0	45.8	52.05	2.16	54.2	32.99	12.6	2.16	1.141407	16.41221	94.24618	80.48664	0.854004
815	5 815	44.01	20.11	20.33	12.5	3.01	0.04	0	0	0	44.01	52.94	3.05	55.99	35.88	15.55	3.05	1.15502	21.38033	114.5213	99.00984	0.864554
817	/ 817	42.47	19.52	20.74	13.82	3.39	0.06	0	0	0	42.47	54.08	3.45	57.53	38.01	17.27	3.45	28.24242	0.642857	0.380952	55.47619	145.625

	Original				
	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
>8um	0.601645	0.218664	-0.10606	0.165965	0.516456
>16um	0.630126	0.169016	-0.20474	0.10843	0.556532
>32um	0.599367	0.136923	-0.22572	0.103775	0.567165
>64um	0.4238	0.111696	-0.12262	0.166649	0.498668

	>8um	>16um	>32um	>64um
Original	0.326337	0.39212	0.433385	0.277504
Original - last	0.601645	0.630126	0.599367	0.4238
Shifted	0.173047	0.109683	0.069308	0.07333

Appendix 1 - Bienen 9 A Depth Real depth %Clay %Very Fine %Fine Silt %Coarse \$%Very Fine%Fine San %Middle C%Coarse \$%Very Coarse Sand

Appendix 1 - Depth R	Bienen 9 / eal depth	A %Clay	%Very Fine	%Fine Silt	%Coarse S	%Very Fine	%Fine San	%Middle C	%Coarse S	%Very Coa	rse Sand											
737	721	< 8 7m 49.88	8-16 fm 21.38	16-32 fm 17.07	32-63 fm 8.25	63-125 fm 2.84	125-250 fn 0.57	250-500 Jn 0	500-1000 ł 0	1000-2000 0	49.88	Silt 46.7	Sand 3.42	44.2								
739 741	723 726	49.55 50.19	20.81 23.57	17.12 16.41	8.91 7.22	3.06 2.27	0.55	0	0	0	49.55 50.19	46.84 47.19	3.61 2.62	52.6 44.2								
743	728	50.22 53.66	22.64	16.18 16.08	7.62	2.76	0.57	0	0	0	50.22 53.66	46.44	3.34	44.2								
747	733	52.12	24.9	17.05	5.14	0.68	0.1	0	0	0	52.12	47.1	0.78	31.3								
749	735	51.36 56.27	25.49 20.73	16.06 14.84	5.47 6.26	1.33	0.29	0	0	0	51.36 56.27	47.02 41.83	1.62	37.2								
753 755	740 743	52.74 52.98	23.18 23.57	16.04 16.73	6.04 5.49	1.61 1	0.4	0	0	0	52.74 52.98	45.25 45.79	2.01 1.22	37.2 31.3								
757	745	47.97	24.33	19.14	6.89	1.36	0.3	0	0	0	47.97	50.36	1.67	37.2								
759	747	55.16 66.83	20.74	15.42	2.78	0.04	0.22	0	0	0	66.83	43.03	0.04	22.1								
763 765	752 755	67.1 58.79	18.94 21.54	10.17 13.1	2.79 4.75	0.68 1.37	0.32	0	0	0	67.1 58.79	31.9 39.39	1 1.82	26.3 37.2								
767	757	56.38	22.6	13.81	5.46	1.42	0.32	0	0	0	56.38	41.88	1.74	37.2								
769	762	59.9 55.28	21.95	13.04	3.8 5.02	1.01	0.53	0	0	0	55.28	38.79 43.49	1.31	31.3								
773 775	764 767	52.44 55.48	22.57 22.61	16.19 14.73	6.86 5.67	1.58 1.23	0.35	0	0	0	52.44 55.48	45.62 43.02	1.94 1.5	37.2 37.2								
777	769	55.11	21.35	15.89	5.9	1.22	0.54	0	0	0	55.11	43.13	1.77	37.2								
779	774	41.21 60.98	19.87 21.73	21.69 12.01	12.51 3.79	3.93	0.79	0	0	0	41.21 60.98	54.07 37.53	4.72	52.6 31.3								
783 785	776 779	55.93 52.67	21.27 20.83	14.59 16.22	6.08 7.87	1.79 2.09	0.35	0	0	0	55.93 52.67	41.94 44.92	2.14 2.42	37.2 44.2								
787	781	57.26	22.23	14.74	4.88	0.89	0.01	0	0	0	57.26	41.85	0.89	31.3								
789 791	783 786	59.66 54.76	22.31 21.16	13.97 15.38	4.01 6.38	0.05	0.42	0	0	0	59.66 54.76	40.29 42.91	2.33	26.3 37.2								
793 795	788 791	56.53 48.64	21.57 25.14	14.68 18.44	5.69 6.45	1.36 1.15	0.16	0	0	0	56.53 48.64	41.94 50.03	1.53	37.2								
797	793	54.75	21.24	15.63	6.62	1.49	0.26	0	0	0	54.75	43.49	1.76	37.2								
799 801	795 798	55.75 51.55	21.1 20.69	14.91 17.26	6.31 8.61	1.67	0.25	0	0	0	55.75 51.55	42.32 46.56	1.93 1.89	37.2								
803 805	800 803	52.37 60.5	21.51 21.19	17.37 13.39	6.78 4.38	1.4	0.57	0	0	0	52.37 60.5	45.65 38.95	1.97	37.2 31.3								
807	805	56.59	23.39	14.89	4.51	0.57	0.05	0	0	0	56.59	42.79	0.62	31.3								
809 811	807 810	49.77 43.95	22.75 21.15	18.26 21.1	7.38 11.32	1.58 2.42	0.27	0	0	0	49.77 43.95	48.39 53.57	1.85 2.48	37.2 44.2								
813 815	812 815	45.8 44.01	21.21	20.39	10.44	2.11	0.05	0	0	0	45.8 44.01	52.05 52.94	2.16	44.2								
817	817	42.47	19.52	20.74	13.82	3.39	0.06	0	0	0	42.47	54.08	3.45	52.6								
	2	AI	Si	Р	s	CI	Ar	к	Ca	Sc	Ti	v	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	As	
737	721	0.000245	0.005012	0.000129 6 78E-05	0.002381	3.96E-05 8.05E-06	0.007762	0.043146	0.173652	1.32E-05	0.038288	0.001305	0.002407	0.035092	1.593198	0.016715	0.001043	0.000224	0.008666	0.001512	0.003212	
741	726	0.000219	0.006935	4.76E-05	0.006216	1.16E-05	0.002402	0.05779	0.270814	8.36E-05	0.047542	0.001851	0.002833	0.052401	2.129286	0.020657	0.000894	1.42E-05	0.010989	0.002464	0.003823	
743 745	728 731	0.000408	0.006494 0.008247	4.2E-05 0.000115	0.005328	5.68E-06 5.3E-06	0.002226	0.056823 0.065316	0.240685	0	0.04795	0.001957	0.00289	0.05606	2.057781 2.305637	0.021376	0.001175	7.73E-05 7.11E-05	0.012458	0.002028	0.003592	
747	733	0.000508	0.007473	7.11E-05	0.001486	0	0.002297	0.063293	0.152625	0	0.054953	0.00225	0.00329	0.060172	2.308946	0.023109	0.001475	0.000116	0.013848	0.002366	0.004733	
749	735	0.000419	0.007213	9.52E-05 8.33E-05	0.001296	7.24E-06 0	0.002125	0.064817	0.141809	1.14E-US 0	0.058573	0.002053	0.003556	0.076733	2.300706	0.024842	0.000659	7.35E-05 8.94E-05	0.012893	0.002259	0.005391	
753	740	0.000521	0.007603	6.01E-05	0.00099	1.61E-05	0.002038	0.063008	0.192495	0	0.054406	0.00203	0.003529	0.050351	2.318309	0.021847	0.001242	4.51E-05	0.012414	0.002034	0.005261	
757	745	0.000432	0.007266	4.32E-05	0.001130	5.02E-06	0.002563	0.062399	0.178299	0	0.055799	0.00205	0.003465	0.072811	2.482486	0.023372	0.00097	8.64E-05	0.012609	0.002328	0.006322	
759 761	747 750	0.000523	0.007517 0.007807	5.51E-05 4.95E-05	0.001053 0.001067	0 4.12E-06	0.002464 0.001849	0.06428	0.156964 0.160451	0 3.71E-05	0.059777 0.06086	0.002209 0.00243	0.003562 0.003571	0.066203 0.048718	2.337966 2.391024	0.022276 0.023536	0.001572 0.001775	8.26E-05 0.000104	0.013525 0.012856	0.002288	0.005933 0.004554	
763	752	0.000461	0.007159	0.000111	0.000976	1.54E-05	0.002792	0.072968	0.19176	5.15E-06	0.055465	0.002075	0.003418	0.067807	2.799709	0.026723	0.0008	4.53E-05	0.012093	0.001688	0.004854	
763	757	0.000431	0.006919	9.03E-05	0.001013	5.55E-08 0	0.002855	0.072482	0.152852	3.37E-05	0.054555	0.002172	0.003393	0.048744	2.20958	0.023209	0.001022	0.000179	0.012003	0.002239	0.005282	
769 771	759 762	0.000299	0.006401	1.64E-05 0.000114	0.002246	0 1.33E-05	0.002413	0.062738	0.215201 0.183645	0	0.049868	0.002187	0.003101 0.002987	0.073723	2.520933 2.360954	0.024322 0.023119	0.000765	8.22E-06 0	0.011701 0.012098	0.001817	0.005267	
773	764	0.000499	0.006615	9.97E-05	0.002712	0	0.001811	0.059128	0.19639	0	0.050574	0.002138	0.003094	0.063568	2.480954	0.022572	0.000508	4.07E-06	0.011292	0.001412	0.006286	
775	769	0.000348	0.006506	7.84E-05 3.43E-05	0.005189	4.29E-06	0.001791	0.057744	0.238337	1.55E-US 0	0.04919	0.002019	0.003163	0.07023	2.451482	0.024022	0.000539	2.68E-05	0.01095	0.002271	0.005863	
779 781	771 774	0.000536	0.009277 0.006737	2.8E-05 1.79E-05	0.002022	0 1.29E-05	0.00188	0.058026	0.315792 0.241374	0 1.99E-05	0.046886	0.00166	0.002833 0.002911	0.050964	1.915111 2.339004	0.019531 0.022389	0.001214	6.32E-05 4.78E-05	0.010695	0.002222 0.001376	0.004922 0.00663	
783	776	0.000488	0.007425	6.12E-05	0.001049	0	0.001307	0.058773	0.239678	0	0.047938	0.001817	0.003049	0.047819	2.181142	0.021756	0.000731	0	0.011473	0.001585	0.00492	
785 787	7/9	0.000483	0.007853	4.19E-05 5.2E-06	0.001172	1.43E-05 0	0.001854	0.063145	0.262598	0	0.050149	0.002108	0.002933 0.003158	0.049547 0.039473	2.323497 2.314393	0.022058	0.000708	3.78E-05 0.000175	0.011997 0.012314	0.002022	0.004849	
789	783 786	0.000434	0.006899	5.73E-05	0.000975	1.75E-05 0	0.004399	0.054863	0.204421	0	0.044448	0.001189	0.002732	0.037447	1.953089	0.019577	0.000906	5.38E-05	0.010766	0.002543	0.004788	
793	788	0.000435	0.007371	6.65E-05	0.001246	0	0.002913	0.061298	0.241094	0	0.05154	0.002046	0.003016	0.081119	2.500685	0.02388	0.000795	4.15E-05	0.012905	0.002176	0.005338	
795 797	791 793	0.000314	0.007224 0.007793	1.68E-05 1.46E-05	0.001194 0.000976	8.4E-06 0	0.002985 0.00322	0.06257 0.062378	0.279595 0.247084	0	0.04976 0.050915	0.001968 0.001714	0.002971 0.003014	0.057491 0.046839	2.312811 2.179023	0.022086 0.021892	0.001092 0.001505	8.5E-05 7.38E-05	0.01215	0.001847 0.002143	0.005129	
799 801	795 798	0.000428	0.007176	0.000105 3.84F-05	0.000938	3.75E-05	0.002096	0.062565	0.237392	0 8 785-06	0.051183	0.001928	0.003226	0.041347	2.255607	0.02192	0.000962	5.27E-05	0.012423	0.002211	0.005689	
803	800	0.000539	0.007834	4.83E-05	0.001098	0	0.001815	0.070428	0.251871	0	0.054992	0.002096	0.003272	0.03909	2.358852	0.022857	0.001146	6.4E-05	0.011733	0.001785	0.00492	
805 807	803 805	0.000443 0.000479	0.007819 0.008718	7.95E-05 2.03E-05	0.001096 0.001236	0 5.07E-06	0.002279 0.002109	0.063283 0.06368	0.211631 0.267946	0	0.05459 0.053753	0.002172 0.001701	0.003202 0.003272	0.056757 0.06591	2.423121 2.402204	0.022969 0.023028	0.000638 0.001147	0 6.79E-05	0.012598 0.011989	0.002172 0.002822	0.004851 0.00504	
809	807	0.000401	0.008308	0.000108	0.001119	0	0.001977	0.059987	0.248118	4.41E-06	0.051117	0.002031	0.003009	0.049805	2.14541	0.020608	0.000707	9.92E-06	0.01131	0.002115	0.005041	
813	812	0.000553	0.009101	3.69E-05	0.001118	0	0.003018	0.06214	0.292956	2.22E-05	0.052109	0.001350	0.002803	0.056404	2.129328	0.019402	0.001137	1.58E-05	0.011038	0.002422	0.004525	
815 817	815 817	0.000423 0.000347	0.009047 0.000223	3.75E-05 0.000198	0.001285	5.55E-05 0.000451	0.006755 0.032593	0.06148	0.330276	1.11E-05 2.89E-05	0.048457 0.000132	0.001515 4.55E-05	0.00298	0.050528 0.00038	2.061585 0.002592	0.019314 0.001666	0.001473	0.000173 0	0.015149 0.030005	0.002515 0.00019	0.004441 0.002336	
		50	Pr	Ph	Cr	7r	A.a.	Cd.	Cn.	ch	~	Pa	та	\A/	lr.	A.,	Ha	Ph	D1	Moline	Mo coh	7r/Ph
737	721	0.00464	0.001795	0.035642	0.046696	0.045328	0.000261	0.000592	0.000469	0.000733	0	0.001131	0.004643	0.007711	0.001713	0.004371	0.003234	0.004067	0.002533	0.744575	0.255425	1.271767
739	723	0.004996	0.001321 0.001876	0.039776	0.050001	0.043369	0.000255	0.000425	0.000646	0.001354 0.001623	0	0.001273	0.005212	0.008853	0.001764	0.004567	0.003951 0.003581	0.003643	0.005341 0.003834	0.74831	0.25169	1.090349
743 745	728	0.004644	0.001427	0.039103	0.048961	0.041262	0.000543	0.000306	0.000568	0.001475	0	0.001647	0.004889	0.008367	0.001983	0.004947	0.003974	0.005045	0.004135	0.748473	0.251527	1.055215
743	733	0.004777	0.001611	0.041542	0.046833	0.043972	0.000438	0.000329	0.00027	0.000445	0	0.002704	0.005313	0.009297	0.001296	0.004389	0.00353	0.005693	0.004422	0.751352	0.248648	1.058496
749 751	735 738	0.005668 0.005386	0.001763 0.001461	0.04244 0.042598	0.046899 0.049513	0.040011 0.04095	0.00043 0.000467	0.000256 0.000357	0.000202 0.000291	0.000322 0.000934	0 0	0.003765 0.003118	0.005647 0.005611	0.008771 0.009222	0.001612 0.001602	0.004517 0.004594	0.003655 0.003494	0.005109 0.004339	0.005943 0.00594	0.749274 0.751964	0.250726 0.248036	U.942748 0.961294
753	740	0.004862	0.001568	0.042486	0.050216	0.041211	0.000511	0.000241	0.000519	0.000697	0	0.001306	0.005659	0.008712	0.001934	0.004905	0.003654	0.004225	0.005221	0.751359	0.248641	0.969979
757	745	0.005136	0.001644	0.041038	0.047582	0.039248	0.000237	0.000335	0.000351	0.000585	0	0.00164	0.005201	0.008899	0.001779	0.004021	0.003925	0.00423	0.00542	0.753988	0.246012	0.956844
759 761	747 750	0.004776	0.001734 0.001025	0.042516 0.043537	0.045942 0.046806	0.043454 0.045539	0.000463	0.000446 0.000179	0.000418	0.000697	0	0.001537 0.001979	0.005519 0.005793	0.008982	0.001592	0.004264 0.00421	0.003733 0.004101	0.004217 0.004764	0.005149 0.005099	0.753179 0.751114	0.246821 0.248886	1.022077
763	752	0.005439	0.000925	0.045338	0.04764	0.033546	0.00025	0.000392	0.000432	0.000765	0	0.001586	0.005467	0.008285	0.002651	0.004577	0.004273	0.004099	0.006587	0.750445	0.249555	0.739905
767	757	0.005332	0.001044	0.045557	0.045455	0.03931	0.000548	0.000332	0.000409	0.000421	0	0.001300	0.005021	0.008102	0.001964	0.004554	0.003834	0.003405	0.00525	0.751335	0.248665	0.918139
769 771	759 762	0.004833 0.004743	0.001363 0.002226	0.041792 0.041258	0.052171 0.050647	0.036 0.037499	0.000392 0.000589	0.000493 0.000168	0.000611 0.000534	0.001132 0.000887	0	0.001436 0.001532	0.005534 0.004865	0.008699 0.008519	0.001613 0.001813	0.004558 0.004476	0.003897 0.003104	0.003755 0.004273	0.005394 0.005142	0.751032 0.75158	0.248968 0.24842	0.861406 0.908895
773	764	0.00493	0.001627	0.040933	0.051677	0.036893	0.000241	0.000422	0.000496	0.000739	0	0.001302	0.005519	0.008158	0.001889	0.004679	0.00339	0.003904	0.005869	0.74952	0.25048	0.901318
775 777	/67 769	0.005322	0.001448	0.039473	0.05197 0.056661	0.038355 0.035971	0.000252	0.000247	0.000986	0.00145 0.001807	0	0.002316 0.001378	0.005002	0.008543	0.001712	0.004584	0.003669	0.003156 0.003168	0.004982 0.005385	0.748223 0.749613	0.251777 0.250387	0.97168 0.896982
779 781	771 774	0.004686	0.000544	0.037924	0.061148	0.043886	0.000529	0.000266	0.001302	0.002148	0	0.001083	0.005097	0.009427	0.001536	0.004546	0.003901 0.002874	0.003938	0.004133 0.005578	0.744757	0.255243	1.157215 0.863146
783	776	0.005343	0.001435	0.040404	0.055485	0.038836	0.000545	0.000275	0.000741	0.001416	0	0.000959	0.004562	0.008058	0.001712	0.004623	0.003696	0.003789	0.00483	0.747255	0.252745	0.961182
785 787	779 781	0.005401 0.005538	0.00087 0.001441	0.040593 0.042556	0.056103 0.055848	0.037446 0.036445	0.000424 0.00054	0.000298 0.000139	0.001058 0.000645	0.001798 0.001651	0	0.000945 0.001321	0.004845 0.004821	0.008304 0.00867	0.001684 0.002181	0.004777 0.004374	0.004173 0.003728	0.004027 0.003586	0.005548 0.005127	0.746959 0.748289	0.253041 0.251711	0.922463 0.856417
789	783 796	0.004362	0.001255	0.038327	0.052237	0.041023	0.000276	0.000299	0.000596	0.000787	0	0.001215	0.004877	0.007675	0.001408	0.004036	0.003347	0.003664	0.003539	0.748307	0.251693	1.070348
791	788	0.005249	0.00157	0.039416	0.053573	0.037829	0.000334	0.000152	0.000724	0.001609	0	0.002592	0.004944	0.008096	0.001594	0.004659	0.003085	0.004/73	0.00502	0.747173	0.252827	0.923965
795 797	791 793	0.00555 0.005148	0.001349 0.001199	0.040877 0.039339	0.058209 0.055744	0.03726	0.000504 0.00045	0.000344	0.001088 0.000857	0.00214 0.00148	0	0.001718 0.001368	0.005179 0.005495	0.008352 0.008793	0.002109 0.001725	0.004832 0.004946	0.004211 0.003965	0.003835 0.004379	0.005097 0.004808	0.746625 0.747545	0.253375 0.252455	0.911503 1.070542
799	795	0.004857	0.001547	0.040894	0.054525	0.03983	0.000465	0.000305	0.00105	0.001117	0	0.001493	0.005297	0.008811	0.001573	0.004651	0.003537	0.003898	0.005194	0.748801	0.251199	0.973973
801 803	798 800	0.004781	0.001297	0.041523	0.05687	0.038634	0.000391	0.000344	0.000939	0.001494	0	0.001023	0.004684	0.008393	0.001115	0.004113	0.003633	0.00385	0.00458	0.746655	0.253345	0.93043
805 807	803 805	0.005261 0.004497	0.001267	0.040933 0.039817	0.05128	0.040781 0.042437	0.00043	0.000189	0.000736	0.001059 0.001541	0 N	0.00219	0.00528	0.008901 0.00882	0.001649 0.00146	0.004593	0.003956 0.004387	0.004656 0.004298	0.005152 0.005592	0.748239 0.746045	0.251761 0.253955	0.996296 1.065793
809	807	0.00508	0.002215	0.03929	0.055686	0.043697	0.000753	0.000228	0.001159	0.001668	0	0.002017	0.00489	0.009352	0.001032	0.004747	0.003671	0.003964	0.00438	0.746276	0.253724	1.112171
811 813	810 812	0.004889	0.001238	0.036257	0.063625	0.04/66	0.00078	0.000255	0.001489	0.002372	0	0.001211	0.00488	0.009031	0.000963	0.004941	0.003635	0.004088	0.003/97	0.743198	0.25507	1.514516 1.141407
815 817	815 817	0.005499 0.00671	0.001323 0.004543	0.036271 0.000682	0.058886 0.000947	0.041894 0.019265	0.000598 0.001484	0.000307 0.000298	0.001225 0.000124	0.002131 2.48E-05	0 1.65E-05	0.002482 2.07E-05	0.004715 0.001505	0.008203 0.001753	0.001258 0.001869	0.005043 0.008248	0.003987 0.003282	0.004577 0.002638	0.00522 0.002373	0.742821 0.730886	0.257179 0.269114	1.15502 28.24242
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Appendix 1 - E	lienen 8 B								5 0/1/		<u> </u>			I													
Depth Re	al depth %	6Clay %	6Very Fin∈ %	6-32 tm	%Coarse 5%	Very Fine%	Fine San %	Viddle C%Cc	arse 5%Ve	ry Coarse	e Sand	211+	Sand	- 8um	16um >	-32um	~64um	Original Zr/Rb	Si/AI	Ti/AI	Zr/AI	Zr/Ti	Shifted grap)h Si/Al	Ti/AI	7 r/A1	Zr/Ti
631	621	46.06	20.6	18.32	10.66	3.78	0.57	0-300 11300-	0	0	46.06	49.59	4.35	53.93	33.33	15.01	4.35	1.432824	9.512097	79.37903	117.6129	1.481662	1.222747	12.45552	99.91103	115.0819	1.151843
633	623	50.25	21.02	16.91	8.09	2.96	0.77	0	0	0	50.25	46.02	3.73	49.75	28.73	11.82	3.73	1.222747	12.45552	99.91103	115.0819	1.151843	1.14217	15.69841	126.496	132.0159	1.043636
635	625	54.39	21.62	15.06	6.59	2.01	0.33	0	0	0	54.39	43.27	2.34	45.61	23.99	8.93	2.34	1.14217	15.69841	126.496	132.0159	1.043636	1.275461	16.96241	142.609	260.5489	1.827015
637	628	54.41	21.59	15.1	6.74	1.92	0.25	0	0	0	54.41	43.43	2.17	45.6	24.01	8.91	2.17	1.275461	16.96241	142.609	260.5489	1.827015	1.185575	14.5614	114.7149	158.3991	1.380807
639	630	54.07	21.67	15.98	6.57	1.41	0.31	0	0	0	54.07	44.21	1.72	45.94	24.27	8.29	1.72	1.185575	14.5614	114.7149	158.3991	1.380807	1.107221	23.67708	194.6927	200.1302	1.027929
641	632	53.82	21.14	15.98	7.49	1.56	0.01	0	0	0	53.82	44.61	1.57	46.18	25.04	9.06	1.57	1.107221	23.67708	194.6927	200.1302	1.027929	1.058321	16.14618	145.1761	124.3123	0.856286
643	634	51.32	21.73	17.3	7.87	1.68	0.09	0	0	0	51.32	46.91	1.77	48.67	26.94	9.64	1.77	1.058321	16.14618	145.1761	124.3123	0.856286	1.049053	11.41304	191.1565	170.0652	0.889665
645	637	50.88	20.7	16.63	8.83	2.59	0.37	0	0	0	50.88	46.16	2.96	49.12	28.42	11.79	2.96	1.049053	11.41304	191.1565	170.0652	0.889665	1.07133	23.03252	376.1789	323.4634	0.859866
647	639	49.59	23.98	15.77	7.72	2.55	0.39	0	0	0	49.59	47.47	2.94	50.41	26.43	10.66	2.94	1.07133	23.03252	376.1789	323.4634	0.859866	1.18683	31.38947	473.3368	434.8421	0.918674
649	641	45.84	20.42	18.93	11.21	3.11	0.5	0	0	0	45.84	50.56	3.6	54.17	33.75	14.82	3.6	1.18683	31.38947	4/3.3368	434.8421	0.918674	1.2111112	14.59447	210.9631	201.106	0.953276
651	643	48.64	21.53	18.05	9.62	2.11	0.05	0	0	0	48.64	49.2	2.16	51.30	29.83	11.78	2.10	1.211112	26 22622	210.9631	201.106	0.953276	1.22814	30.32032	256 5061	463.3579	0.926501
655	649	42.4	10.72	19.00	10.16	4.03	0.55	0	0	0	42.4	46.65	4.37	50.77	21.05	1/.05	4.57	1 210/29	17 28650	256 5061	405.5579	0.920301	1 2/7/99	17.20039	172 2122	235.001	1 217202
657	650	43.23	20.16	17 37	12.85	5.82	0.30	0	0	0	43.23	50.37	6.54	56.92	36.76	19.20	6.54	1 347489	12 25888	172 2132	2253.001	1 317898	1 218109	29 25217	396 713	220.3334	0.937705
659	652	49.03	21.57	17.08	8.79	3.04	0.5	0	0	0	49.03	47.44	3.54	50.98	29.41	12.33	3.54	1.218109	29.25217	396.713	372	0.937705	1.276869	21.20732	277.6768	255,5061	0.920156
661	654	45.39	21.63	19.74	10.18	2.75	0.31	0	0	0	45.39	51.55	3.06	54.61	32.98	13.24	3.06	1.276869	21.20732	277.6768	255.5061	0.920156	1.151337	12.24908	176.3736	143.8791	0.815763
663	657	33.47	15.15	15.12	11.48	12.81	11.3	0.66	0	0	33.47	41.75	24.78	66.52	51.37	36.25	24.78	1.151337	12.24908	176.3736	143.8791	0.815763	1.246405	32.18421	394.0439	381.7281	0.968745
665	659	20.3	9.18	9.57	10.57	23.75	24.96	1.67	0	0	20.3	29.32	50.39	79.7	70.52	60.95	50.39	1.246405	32.18421	394.0439	381.7281	0.968745	1.555375	27.98693	249.3791	306.6732	1.229747
667	661	56.91	21.54	14.17	5.23	1.7	0.45	0	0	0	56.91	40.94	2.15	43.09	21.55	7.38	2.15	1.555375	27.98693	249.3791	306.6732	1.229747	1.452224	15.14559	159.9464	188.0268	1.175562
669	663	55.48	24.25	15.21	4.57	0.49	0.01	0	0	0	55.48	44.03	0.5	44.53	20.28	5.07	0.5	1.452224	15.14559	159.9464	188.0268	1.175562	1.082503	16.34146	225.6293	189.1951	0.838522
671	666	53.95	24.48	15.89	5	0.59	0.09	0	0	0	53.95	45.38	0.67	46.05	21.57	5.68	0.67	1.082503	16.34146	225.6293	189.1951	0.838522	1.018846	24.58519	365.0222	283.5259	0.776736
673	668	49.75	22.41	17.8	7.72	1.98	0.34	0	0	0	49.75	47.93	2.32	50.25	27.84	10.04	2.32	1.018846	24.58519	365.0222	283.5259	0.776736	1.085905	18.04734	260.0237	213.0237	0.819247
675	670	46.18	23.71	19.92	8.39	1.71	0.09	0	0	0	46.18	52.02	1.8	53.82	30.11	10.19	1.8	1.085905	18.04734	260.0237	213.0237	0.819247	1.207121	19.75595	291.5	251.0595	0.861268
677	672	44.72	20.55	19.04	11.22	3.92	0.54	0	0	0	44.72	50.81	4.47	55.27	34.72	15.68	4.47	1.207121	19.75595	291.5	251.0595	0.861268	1.279903	18.185	232.315	226.53	0.975098
679	674	45.51	20.61	18.8	10.77	3.74	0.58	0	0	0	45.51	50.18	4.31	54.5	33.89	15.09	4.31	1.279903	18.185	232.315	226.53	0.975098	1.247161	14.95434	207.9224	195.5708	0.940595
681	677	40	21	19	10.32	3.16	0.53	0	0	0	40	50.32	3.68	54.01	33.01	14.01	3.68	1.24/161	14.95434	207.9224	195.5708	0.940595	1.26191	20.24571	284.1029	266.7029	0.938/55
083	679	40.17	19.45	19.59	14.97	2.09	0.42	0	0	0	20.69	52.24	7.59	59.83	40.38	20.79	/.55	1.20191	20.24571	284.1029	200.7029	0.938/55	1.30/108	33.00001	490.7778	210 2057	1.052040
687	683	39.00	14.96	15 58	14.07	12 02	3.4	0.01	0	0	35.00	33.97 46.71	4.55	62.04	41.55	22 5	4.53	1 201672	21 20052	202 2517	219 2957	1 052040	1.391072	22.00932	242 6012	272 5051	1 1 2 2 1 2 7
689	686	56.49	21.81	14 21	5.42	1 73	0.33	0.01	0	0	56.49	40.71	2.06	43.5	21 69	7 48	2.06	1 400364	23 79141	243 6012	273 5951	1 123127	1.002652	13 15929	206 6991	172 3097	0.833626
691	688	50.17	23.41	16.38	7.14	2.48	0.41	0	õ	0	50.17	46.94	2.89	49.82	26.41	10.03	2.89	1.002652	13,15929	206.6991	172.3097	0.833626	1.165337	16.28729	260.3481	229.2044	0.880377
693	690	47.48	26.46	18.33	6.06	1.45	0.22	0	0	0	47.48	50.85	1.67	52.52	26.06	7.73	1.67	1.165337	16.28729	260.3481	229.2044	0.880377	1.054073	18.34177	282.8165	241.8165	0.85503
695	692	47.17	23.31	17.63	8.85	2.5	0.54	0	0	0	47.17	49.8	3.04	52.83	29.52	11.89	3.04	1.054073	18.34177	282.8165	241.8165	0.85503	1.082821	13.82791	219.814	190.214	0.865341
697	695	52.63	23.73	15.68	6.03	1.55	0.38	0	0	0	52.63	45.44	1.94	47.37	23.64	7.96	1.94	1.082821	13.82791	219.814	190.214	0.865341	1.091862	22.62791	362.5969	305.0698	0.841347
699	697	52.49	24.11	17.02	5.16	0.8	0.41	0	0	0	52.49	46.3	1.22	47.5	23.39	6.37	1.22	1.091862	22.62791	362.5969	305.0698	0.841347	1.168335	28.10476	444.781	405.6571	0.912038
701	699	53.49	23.17	15.38	6.06	1.6	0.29	0	0	0	53.49	44.62	1.89	46.5	23.33	7.95	1.89	1.168335	28.10476	444.781	405.6571	0.912038	1.063624	13.84689	221.3349	193.3301	0.873473
703	701	52.15	22.35	16.08	7.07	1.92	0.43	0	0	0	52.15	45.5	2.35	47.85	25.5	9.42	2.35	1.063624	13.84689	221.3349	193.3301	0.873473	1.093411	17.23429	264.04	234.7086	0.888913
705	703	51.13	22.41	16.4	7.55	2.19	0.33	0	0	0	51.13	46.36	2.52	48.88	26.47	10.07	2.52	1.093411	17.23429	264.04	234.7086	0.888913	1.199306	21.52713	339.8992	332.124	0.977125
707	706	54.85	23.82	14.11	5.3	1.49	0.43	0	0	0	54.85	43.23	1.92	45.15	21.33	7.22	1.92	1.199306	21.52713	339.8992	332.124	0.977125	1.050253	17.78873	334.4014	286.8521	0.857808
709	708	54.63	22.96	14.78	5.4	1.89	0.33	0	0	0	54.63	43.14	2.22	45.36	22.4	7.62	2.22	1.050253	17.78873	334.4014	286.8521	0.857808	0.974071	32.80769	622.8205	492.7051	0.791087
711	710	50.30	23.03	16.20	4.53	1.42	0.35	0	0	0	50.30	41.87	1.78	43.04	19.81	0.3	1./8	0.974071	32.80/09	160 2205	492.7051	0.791087	0.908535	20.90470	408.2280	338.3333	0.705723
715	712	51.46	21.04	16.30	8.04	2.43	0.58	0	0	0	51.46	44.00	2.33	47.45	23.39	9.21	2.55	1 140937	20.90470	406.2260	379 5934	0.703723	1.140957	10 92105	98 46053	115 2/01	1 17042
715	717	53.93	22.11	14.96	6.8	1 78	0.04	0	0	0	53.93	43.50	1.87	46.07	27.42	8 67	1.87	1 156166	10 92105	98 46053	115 2401	1 17042	1 173033	14 1769	92 42506	90 61179	0.980381
719	719	49.69	21.37	17.35	8.54	2.6	0.45	0	0	0	49.69	47.26	3.04	50.31	28.94	11.59	3.04	1.173033	14.1769	92.42506	90.61179	0.980381	111/5055	1.1.1.05	52.12500	50.01175	0.500501
																-											
									0.1.1	a a l		0 10724	0.2425.00	0 227442	0.154400			Uriginal	C: /AI	T: /AI	7-/01	7. /T:	Shifted	C:/AI	T:/AI	7-/01	7-/T:
									Urigi	ingi oq		0.19/21	0.242569	0.22/442	0.154496		- 9	2F/KD	5I/AI	11/AI	2f/Al	2ľ/11	2F/KD	51/AI	11/AI	21/AI	2F/11
									SUIL	eu		0.007298	0.700786	0.070712	0.581338		>00111	0.19/21	0.122457	0.14909	0.173048	-0.12093	0.007298	0.282700	0.003/52	0.212358	0.148052
																	>32um	0 227442	0 189675	0.113673	0 166691	-0.03390	0.676712	0 287195	0.013166	0 179927	0.22393
																	>64um	0.154496	0.180605	0.100069	0.138287	-0.03404	0.581338	0.298414	0.028059	0.173531	0.238928

Appendix 1- Depth R	Bienen 8 A eal depth	%Clay	%Very Fine	%Fine Silt	%Coarse S	%Very Fine	%Fine San	%Middle C	%Coarse S	%Very Coa	se Sand	Cil.	Cand	Dor								
631	621 623	< 8 m 46.06 50.25	20.6 21.02	16-32 fm 18.32 16.91	10.66 8.09	3.78 2.96	0.57	250-500 im 0	0	0 0	46.06 50.25	49.59 46.02	4.35 3.73	52.6 44.2								
635 637	625 628	54.39 54.41	21.62 21.59	15.06 15.1	6.59 6.74	2.01 1.92	0.33	0	0	0	54.39 54.41	43.27 43.43	2.34 2.17	37.2 37.2								
639 641	630 632	54.07 53.82	21.67 21.14	15.98 15.98	6.57 7.49	1.41 1.56	0.31 0.01	0	0	0	54.07 53.82	44.21 44.61	1.72 1.57	37.2 37.2								
643 645	634 637	51.32 50.88	21.73 20.7	17.3 16.63	7.87 8.83	1.68 2.59	0.09 0.37	0	0	0	51.32 50.88	46.91 46.16	1.77 2.96	37.2 44.2								
647 649	639 641	49.59 45.84	23.98 20.42	15.77 18.93	7.72	2.55	0.39	0	0	0	49.59 45.84	47.47	2.94 3.6	44.2 52.6								
653	643 645	48.64	21.53 19.91	18.05	9.62 13.27	2.11 4.03	0.05	0	0	0	48.64	49.2 53.02	4.57	44.2 52.6								
657	650 652	43.09 49.03	20.16	17.37	12.85	5.82 3.04	0.50	0	0	0	43.09 49.03	50.37 47.44	4.12 6.54 3.54	62.5 52.6								
661 663	654 657	45.39 33.47	21.63 15.15	19.74 15.12	10.18 11.48	2.75 12.81	0.31 11.3	0	0	0	45.39 33.47	51.55 41.75	3.06 24.78	44.2 149								
665 667	659 661	20.3 56.91	9.18 21.54	9.57 14.17	10.57 5.23	23.75 1.7	24.96 0.45	1.67 0	0	0	20.3 56.91	29.32 40.94	50.39 2.15	177 37.2								
669 671	663 666	55.48 53.95	24.25 24.48	15.21 15.89	4.57	0.49	0.01	0	0	0	55.48 53.95	44.03 45.38	0.5	31.3 31.3								
673 675	668 670	49.75	22.41 23.71	17.8 19.92	7.72	1.98	0.34	0	0	0	49.75	47.93	2.32	44.2 37.2								
679	674	44.72 45.51 46	20.55 20.61	18.8	10.77	3.74	0.54	0	0	0	44.72 45.51 46	50.81	4.47	52.6 52.6								
683 685	679 681	40.17	19.45 18.77	19.59 22.33	13.2 14.87	5.89 3.93	1.7	0	0	0	40.17 39.68	52.24 55.97	7.59 4.35	74.3 52.6								
687 689	683 686	36.96 56.49	14.96 21.81	15.58 14.21	16.17 5.42	12.92 1.73	3.4 0.33	0.01 0	0	0	36.96 56.49	46.71 41.45	16.32 2.06	105 37.2								
691 693	688 690	50.17 47.48	23.41 26.46	16.38 18.33	7.14 6.06	2.48 1.45	0.41 0.22	0	0	0	50.17 47.48	46.94 50.85	2.89 1.67	44.2 37.2								
695 697	692 695	47.17 52.63	23.31 23.73	17.63	8.85 6.03	2.5 1.55	0.54	0	0	0	47.17	49.8 45.44	3.04	44.2 37.2								
701	697 699 701	52.49 53.49	24.11 23.17	17.02	5.16 6.06 7.07	1.6	0.41	0	0	0	52.49 53.49	46.3	1.22	31.3 37.2								
705	703	51.13 54.85	22.33	16.4	7.55	2.19	0.43	0	0	0	51.13 54.85	46.36	2.53	44.2 37.2								
709 711	708 710	54.63 56.36	22.96 23.83	14.78 13.51	5.4 4.53	1.89 1.42	0.33	0	0	0	54.63 56.36	43.14 41.87	2.22 1.78	37.2 31.3								
713 715	712 715	52.57 51.46	21.84 21.11	16.38 16.41	6.66 8.04	1.97 2.43	0.58 0.54	0	0	0	52.57 51.46	44.88 45.56	2.55 2.97	37.2 44.2								
717 719	717 719	53.93 49.69	22.44 21.37	14.96 17.35	6.8 8.54	1.78 2.6	0.09 0.45	0	0	0	53.93 49.69	44.2 47.26	1.87 3.04	37.2 44.2								
631	621	AI	Si 0.003808	P 6 465-05	S 0.001024	CI	Ar	K	Ca	Sc	n 0.031781	V 0.001048	Cr	Mn	Fe	Co	Ni	Cu	Zn 0.008745	Ga	As	
633	623	0.000386	0.003808	0.000144 6.93E-05	0.001843	5.22E-05 1.67E-05	0.002481	0.046222	0.165715	4.81E-05	0.038584	0.001048	0.002189	0.036195	1.777628	0.017809	0.000629	0.000144 3.47E-05	0.011103	0.001833	0.005213	
637	628 630	0.00017	0.002881	8.56E-05 7.76E-05	0.003237	2.04E-05	0.000664	0.028331	0.135418	1.92E-05 0.000107	0.024226	0.000851	0.001585	0.027881	1.214218	0.014244	0.00028	1.15E-05 3.64E-05	0.008671	0.001293	0.004027	
641 643	632 634	0.000221	0.005232	5.06E-05 0.000135	0.001498	4.6E-06	0.000514	0.050795	0.171319	3.45E-05 0	0.04302	0.001454	0.002584	0.04373	1.946311 2.323169	0.019614	0.000999	0.000133 6.85E-06	0.01354	0.00216	0.005022	
645 647	637 639	0.000254	0.0029	7.18E-05 0.000111	0.002562	0 2.78E-05	0.001328	0.051707	0.158898	2.76E-05 2.22E-05	0.048575	0.002463 0.002326	0.002996	0.051142	2.342085	0.022846	0.001071 0.000968	0 3.89E-05	0.011699	0.001767	0.006334	
649 651	641 643	0.000107 0.000239	0.003357 0.00349	8.78E-05 7.27E-05	0.001783 0.003264	0	0.001361 0.001239	0.053581 0.052391	0.151681 0.145426	3.04E-05 1.1E-05	0.050618 0.050447	0.002203 0.002392	0.003057	0.071355 0.034217	2.521093 2.249187	0.023968 0.021686	0.00041 0.000576	4.5E-06 0.000107	0.011465 0.010626	0.002133 0.002071	0.005936 0.005686	
653 655	645 648	0.000107 0.000182	0.003872 0.003154	8.3E-05 4.23E-05	0.001579 0.008856	0 4.12E-05	0.001392 0.00116	0.05476	0.164809 0.252405	0	0.053306 0.046795	0.002386 0.002023	0.003089	0.03791 0.043578	2.245284 2.16016	0.021485 0.022539	0.001024 0.00066	0	0.011246 0.010944	0.002687 0.002443	0.005366 0.006274	
657 659	650 652	0.000222 0.000129	0.002725 0.003761	7.67E-05 4.92E-05	0.025743 0.003567	7.9E-06 0	0.001615 0.001734	0.039102 0.053598	0.445842 0.194713	0	0.038285 0.051009	0.001847 0.002267	0.002171 0.003133	0.046898 0.057542	1.962517 2.424905	0.02078 0.023007	0.000613 0.000631	0	0.009573 0.011191	0.00192 0.00291	0.005114 0.007204	
661 663	654 657	0.00019	0.004028	0.000122 3.35E-05	0.001234	0 5.78E-06	0.002009	0.055045	0.197091	0	0.052735	0.00213	0.003362	0.074633	2.72927	0.023946	0.000843	0 7.17E-05	0.010803	0.002002	0.005355	
667	659 661 663	0.000126	0.00405	3.75E-05 3.2E-05 2.24E-05	0.000909	5.52E-06	0.0022	0.054491 0.050135 0.053687	0.207278	4.41E-06	0.049592	0.001857	0.002823	0.048187	2.064542 1.691992 2.038911	0.019501 0.016752	0.001223	8.83E-05 7.73E-06 9.4E-05	0.010677 0.008654	0.002694	0.004958	
671	666 668	0.000232	0.003696	7.17E-05 4.2E-05	0.001115 0.001103	1.01E-05 0 1.21E-05	0.002373 0.002626	0.056507	0.20006	0	0.05103	0.002476	0.003058 0.00362	0.086866	2.42766	0.02344	0.001349	0.000179 5.41E-05	0.011852 0.01239	0.001962	0.005073	
675 677	670 672	0.000206 0.000194	0.003723 0.003824	0.000104 8.64E-05	0.001199 0.00107	0	0.002991 0.002682	0.055428	0.175939 0.163457	0 1.96E-05	0.053639 0.056425	0.001933 0.00221	0.003138	0.083332	2.551264 2.469328	0.022815 0.023029	0.001276 0.001326	8.67E-05 0.000184	0.011984 0.012029	0.002085	0.006363 0.005133	
679 681	674 677	0.000228 0.000258	0.004143 0.003861	8.2E-05 7.31E-05	0.000873 0.000881	0	0.003692 0.004384	0.056018 0.05577	0.163978 0.163106	3.99E-05 0	0.052928 0.05368	0.002217 0.002088	0.003014 0.003066	0.040073 0.043517	2.175683 2.269444	0.020178 0.020837	0.001299 0.0013	2.28E-05 0.000118	0.011295 0.011367	0.002906 0.003234	0.004708 0.00491	
683 685	679 681	0.000193 0.00011	0.003917	5.86E-05 4.54E-05	0.001074 0.000884	0 3.87E-05	0.003057	0.05711	0.146549 0.128429	1.77E-05 7.75E-06	0.054967 0.05442	0.002258	0.003083	0.034555 0.033779	2.220438 2.096292	0.021884 0.020746	0.000959 0.001498	0.000147	0.011997 0.011718	0.002569	0.004909 0.005595	
687 689 601	683 686	0.000162	0.003537 0.004305	0.000105 6.77E-05	0.00095	1.21E-05 0.000131	0.002574	0.048887 0.050033	0.182236 0.204551	6.4E-05 7.77E-06	0.049017 0.04408	0.002108 0.001818 0.002204	0.003031 0.002895	0.057001	2.102316 1.995458	0.02092	0.001126	6.18E-05 0	0.0011133 0.009377 0.011071	0.002777	0.004835	
693 695	690 692	0.000199	0.003239	8.68E-05 8.48E-05	0.001207	4.20E-00 0 1E-05	0.002575	0.051875	0.102536	0	0.051767	0.002264	0.003157	0.066996	2.668062	0.023918	0.000517	3.3E-05 6.14E-05	0.011215	0.001742	0.005787	
697 699	695 697	0.000233	0.003221	0.000107 7.18E-05	0.001076	1.73E-05 2.54E-05	0.002675	0.0514	0.11727	8.67E-06 7.73E-06	0.051203	0.002197	0.003148	0.05252	2.367479	0.021936	0.000834	5.53E-05 4.53E-05	0.01136	0.002148	0.005645	
701 703	699 701	0.000116 0.000228	0.003272 0.003163	8.98E-05 8.2E-05	0.000939 0.000974	0 5.47E-06	0.003766 0.00321	0.050912 0.052908	0.113498 0.124512	0	0.05179 0.050566	0.001995 0.002333	0.002893 0.003285	0.037646 0.046421	2.160622 2.33791	0.02144 0.02229	0.000885 0.001	0.000121 0.000115	0.01114 0.011426	0.002626 0.002364	0.005333 0.005925	
705 707	703 706	0.000192 0.000144	0.003312 0.00311	8.56E-05 6.5E-05	0.001032 0.000888	0 7.84E-06	0.00344 0.003415	0.053389 0.050737	0.155658 0.164178	7.69E-06 0	0.050738 0.049106	0.002228 0.001769	0.00318	0.051648 0.046775	2.335173 2.190373	0.023334 0.022594	0.000804 0.001496	5.38E-05 7.62E-05	0.011766 0.011187	0.002439 0.00279	0.005106 0.00488	
709 711	708	0.000153 8.3E-05	0.002722	6.9E-05 6.81E-05	0.000905	0	0.001972	0.053537	0.128734 0.127649	0 4.26E-06	0.051163	0.002031	0.00325	0.051436	2.418057	0.023662	0.000432	6.79E-05 2.13E-05	0.011568	0.002904	0.005637	
713 715 717	712 715 717	0.000118	0.003178 0.003783	0.000146 0.000135	0.001081	0 000115	0.00244 0.005042 0.003731	0.059932	0.163791 0.17879 0.119969	2.59E-05 0 1.59E-05	0.055307	0.00216	0.003541	0.077994	2.501068	0.025111 0.023944 0.019075	0.001081	0.000186	0.012926	0.002501	0.00607	
719	719	0.000528	0.007484	0.000193	0.001254	2.33E-05	0.004252	0.057145	0.174531	2.21E-05	0.048794	0.001935	0.002848	0.051087	2.075091	0.019151	0.000966	0.000135	0.011775	0.001825	0.005288	
631	621	Se 0.003862	Br 0.001274	Rb 0.032865	Sr 0.041408	Zr 0.047089	Ag 0.000324	Cd 0.00062	Sn 0.000304	Sb 0.000557	Cs 0	Ba 0.001104	Ta 0.004172	W 0.007016	lr 0.002322	Au 0.003855	Hg 0.003069	Pb 0.003734	D1 0.001939	Mo inc 0.747178	Mo coh 0.252822	Zr/Rb 1.432824
633 635	623 625	0.004381	0.000994	0.036347	0.047138	0.044443	0.000371 0.000354	0.000219	0.000741	0.000691	0	0.000991 0.000367	0.00419	0.007175	0.002178	0.004009	0.003616	0.003881 0.0041	0.002242	0.747511	0.252489	1.222747
637 639	628 630	0.004049	0.001058	0.034702	0.044957	0.044261	0.000247	0.000181	0.000315	0.001005	0	0.000232	0.003111	0.005193	0.001473	0.004859	0.003344	0.004124	0.001801	0.74749	0.25251 0.25078	1.275461 1.185575 1.107221
643 645	634 637	0.004397 0.004749	0.001668	0.040391 0.041195	0.047119 0.047299	0.042747 0.043215	0.000367 0.000166	0.000414 0.000386	0.000426	0.00124 0.000647	0	0.000693 0.001138	0.004991 0.005542	0.00859	0.001518 0.001712	0.004149 0.00506	0.003844 0.00428	0.004117 0.003485	0.004508	0.754956 0.75612	0.245044 0.24388	1.058321
647 649	639 641	0.005982 0.005141	0.001462 0.001333	0.04129 0.039181	0.046836 0.045031	0.044236 0.046501	0.000513 0.000247	0.00017	0.000486 0.000334	0.000356 0.000476	0	0.001098 0.000698	0.005472 0.005407	0.009037	0.001714 0.001801	0.004748 0.004812	0.003894 0.003882	0.003556 0.003569	0.004682	0.757489 0.755149	0.242511 0.244851	1.07133 1.18683
651 653	643 645	0.005287 0.004969	0.000814 0.001215	0.039707 0.040214	0.044595 0.048077	0.04809 0.049388	0.000585 0.000343	0.000279 0.000237	0.000354 0.000558	0.000607 0.000711	0	0.000927 0.000688	0.005383 0.005996	0.009143 0.010245	0.001284 0.001383	0.004385 0.004682	0.003949 0.003676	0.003553 0.003769	0.004185 0.004461	0.757947 0.756251	0.242053 0.243749	1.211112 1.22814
655 657	648 650	0.004643	0.000859	0.037859	0.048178	0.046167	0.00038	0.000218	0.000851	0.001761	0	0.000596	0.005156	0.008721	0.001352	0.005011	0.004166	0.003164	0.004264	0.75566	0.24434	1.219428
661	654	0.004778	0.0001234	0.039267	0.050473	0.047831	0.000628	0.000243	0.000512	0.000855	0	0.001551	0.005608	0.010423	0.001438	0.004719	0.004061	0.003014	0.005029	0.753132	0.243972	1.218109
665 667	659 661	0.005096	0.000739 0.00135	0.038544 0.033292	0.053086 0.058041	0.048042 0.051781	0.000486	0.000247 0.000409	0.000702 0.000874	0.000936	0	0.002632 0.001919	0.005759	0.01062	0.001624 0.001055	0.004124 0.004529	0.00418	0.002972 0.003551	0.004724 0.002778	0.754538	0.245462 0.245996	1.246405
669 671	663 666	0.004532 0.005158	0.001145 0.001017	0.037835 0.039529	0.05539	0.054945 0.04279	0.000414 0.000385	0.000241 0.000145	0.000839	0.001398 0.001019	0	0.001777 0.00174	0.005733	0.010305	0.001142 0.001953	0.004607	0.00369	0.003362 0.003886	0.004303 0.005319	0.752015	0.247985 0.247443	1.452224 1.082503
673 675	668 670	0.005377 0.005354	0.000888 0.001042	0.041496 0.040467	0.047332 0.049102	0.042278 0.043944	0.000477 0.000624	0.000324 0.000259	0.000501 0.00068	0.000406 0.000614	0 0	0.001888 0.002733	0.005841 0.006695	0.009318 0.009888	0.002188 0.002245	0.004715 0.004269	0.004112 0.004073	0.004046 0.003207	0.005005 0.006267	0.75525 0.754545	0.24475 0.245455	1.018846 1.085905
677 679	672 674	0.005377	0.001012	0.040259	0.047854	0.048597	0.000801	0.000221	0.00055	0.00068	0	0.001517	0.006332	0.009648	0.002087	0.005391	0.003907	0.004301	0.005043	0.751728	0.248272	1.207121
681 683	677	0.005252	0.00129	0.040485	0.047298	0.050491	0.000355	0.000385	0.000352	0.000483	0	0.001754	0.006014	0.010154	0.001607	0.004203	0.003679	0.004265	0.004826	0.753968	0.245784	1.247161
687 687	683 692	0.004185	0.000805	0.03709	0.052038	0.053032	0.000474	0.000163	0.000412	0.00035	0	0.001377	0.005999	0.009799	0.001706	0.004868	0.003706	0.003929	0.004237	0.751614	0.245163	1.30/168
691 693	688 690	0.004696	0.000965	0.041365 0.039108	0.043063	0.041474 0.045574	0.000315	0.000301 0.000282	0.000257	0.000224	0	0.001537	0.00544	0.008739	0.002172	0.00483	0.003485	0.003825	0.005247	0.757283	0.242717	1.002652
695 697	692 695	0.005501 0.004976	0.001199 0.001186	0.040436 0.040919	0.045471 0.045585	0.042622 0.044308	0.000463 0.00043	0.000272	0.000436	0.000512 0.000239	0	0.001623 0.001472	0.005673	0.008624	0.002127	0.004862 0.00456	0.003541 0.003395	0.004008	0.005038 0.005012	0.757406	0.242594 0.24302	1.054073 1.082821
699 701	697 699	0.004943 0.004427	0.001381 0.000811	0.03982 0.040429	0.046028 0.042834	0.043478 0.047234	0.000394 0.000267	0.000204 0.000352	0.000404 0.000226	0.000589 0.000346	0 0	0.001058 0.001082	0.006229 0.005837	0.009137 0.009649	0.00233 0.00252	0.005031 0.004544	0.003567 0.003867	0.00375 0.004024	0.005007 0.004681	0.757293 0.757267	0.242707 0.242733	1.091862 1.168335
703	701 703	0.00503	0.00109	0.041526	0.045006	0.044168	0.000307	0.000318	0.000397	0.000379	0	0.001069	0.005849	0.008845	0.001797	0.005138	0.003693	0.003747	0.004919	0.7562	0.2438	1.063624
707	706	0.004591	0.000829	0.040008	0.049443	0.047982	0.000558	0.000164	0.000399	0.000342	0	0.001208	0.005837	0.008679	0.0017	0.004284	0.003715	0.003649	0.004218	0.752605	0.247395	1.199306
713 715	710 712 715	0.005384	0.001573	0.043726	0.046023	0.04235	0.000322	0.000214	0.000435	0.000663	0	0.001367	0.006247	0.009455	0.002591 0.002493 0.00253	0.005075	0.004053	0.004305	0.005684	0.756854	0.243146	0.968535
717 719	717 719	0.00484 0.004901	0.000938 0.000943	0.040046 0.04078	0.046543 0.050126	0.046299 0.047837	0.000345	0.000481 6.1E-05	0.000291 0.00073	0.00051 0.000739	5.29E-06 0	0.002288 0.003401	0.004484 0.004878	0.00743	0.002033 0.002273	0.00417	0.003872 0.003971	0.003036 0.00371	0.003437 0.003981	0.748533 0.747251	0.251467 0.252749	1.156166 1.173033

Appendix 1	- Bienen 7 I	В											-					reversed				
Depth	Real depth	%Clay	%Very Fine	%Fine Silt	%Coarse S%	öVery Fin∈%	%Fine San %	Middle C%Coa	arse S %	Very Coarse	Sand							Original				
		< 8 才m	8-16 † m	16-32 † m	32-63 fm 63	3-125 fm 1	25-250 才n 25	50-500 tn 500-1	000 1 10	00-2000 Cla	ay S	Silt S	Sand	>8um :	>16um	>32um	>64um	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
545	531	43.03	19.14	19.57	13.31	4.44	0.51	0	0	0	43.03	52.03	4.95	56.97	37.83	18.26	4.95	1.476632	22.01515	146.3232	208.0859	1.422097
547	533	48.06	20.2	17.19	10.2	3.9	0.44	0	0	0	48.06	47.59	4.35	51.93	31.73	14.54	4.35	1.188998	24	169.9226	150.6465	0.88656
549	536	51.14	20.12	15.98	9.07	3.3	0.4	0	0	0	51.14	45.17	3.69	48.87	28.75	12.77	3.69	1.153813	15.53314	118.268	115.7205	0.97846
551	538	49.46	20.22	16.71	9.84	3.41	0.36	0	0	0	49.46	46.77	3.77	50.54	30.32	13.61	3.77	1.195206	18.71071	143.6071	138.55	0.964785
553	541	54.84	23.51	14.56	5.54	1.36	0.19	0	0	0	54.84	43.61	1.55	45.16	21.65	7.09	1.55	1.159216	11.69583	86.49375	79.46667	0.918756
555	543	52.79	22.81	16.62	6.29	1.21	0.27	0	0	0	52.79	45.72	1.48	47.2	24.39	7.77	1.48	1.036847	14.82308	114.4077	90.69487	0.792734
557	545	51.51	21.46	17.27	7.57	1.79	0.4	0	0	0	51.51	46.3	2.18	48.49	27.03	9.76	2.18	1.110693	18.95156	146.7024	126.6574	0.863363
559	548	52.81	21.58	16.7	7	1.57	0.34	0	0	0	52.81	45.28	1.91	47.19	25.61	8.91	1.91	1.103164	23.68644	177.6356	152.0169	0.85578
561	550	51.85	25.29	15.39	5.67	1.47	0.33	0	0	0	51.85	46.35	1.8	48.15	22.86	7.47	1.8	1.108722	14.5288	109.4476	95.14398	0.86931
563	552	50.88	22.09	17.71	7.44	1.53	0.34	0	0	0	50.88	47.24	1.87	49.11	27.02	9.31	1.87	1.12649	16.27005	122.393	102.607	0.83834
565	555	52.96	21.92	15.86	7.04	1.84	0.38	0	0	0	52.96	44.82	2.22	47.04	25.12	9.26	2.22	1.121668	18.58571	157.5071	133.6107	0.848284
567	557	46.65	21.43	19.65	9.57	2.27	0.43	0	0	0	46.65	50.65	2.71	53.35	31.92	12.27	2.71	1.146752	14.13095	109.5095	93.02619	0.84948
569	560	34.95	16.47	21.86	18.88	6.97	0.86	0	0	0	34.95	57.21	7.83	65.04	48.57	26.71	7.83	1.42952	21.85401	157.8212	161.1496	1.02109
571	562	37.85	17.65	21.82	16.68	5.41	0.58	0	0	0	37.85	56.16	5.99	62.14	44.49	22.67	5.99	1.318132	19.1761	136.2358	128.3396	0.94204
573	564	29.43	15.56	24.19	22.35	7.84	0.64	0	0	0	29.43	62.1	8.48	70.58	55.02	30.83	8.48	1.673995	19.49072	111.5358	125.8249	1.128112
575	567	42.6	20.5	21.9	12.29	2.25	0.45	0	0	0	42.6	54.7	2.71	57.39	36.89	14.99	2.71	1.460346	17.0989	131.3929	130.2115	0.991009
577	569	45.23	23.41	18.07	9.17	3.23	0.89	0	0	0	45.23	50.66	4.11	54.77	31.36	13.29	4.11	1.236536	15.32827	121.5532	109.845	0.903678
579	571	48.21	26.09	17.19	6.33	1.95	0.22	0	0	0	48.21	49.62	2.17	51.78	25.69	8.5	2.17	1.10522	16.70755	136.4528	117.327	0.859836
581	574	49.83	26.87	16.11	5.09	1.45	0.64	0	0	0	49.83	48.07	2.09	50.16	23.29	7.18	2.09	1.033475	23.06608	187.978	148.3789	0.789342
583	576	47.69	26.04	16.53	7.13	2.35	0.26	0	0	0	47.69	49.7	2.62	52.31	26.27	9.74	2.62	1.123313	17.7623	123.6585	103.4645	0.836695
585	579	51.61	21.09	16.64	8.33	2.1	0.22	0	0	0	51.61	46.07	2.32	48.38	27.29	10.65	2.32	1.121932	18.73375	141.2724	119.5882	0.846508
587	581	55.57	21.14	15	6.32	1.54	0.44	0	0	0	55.57	42.46	1.97	44.44	23.3	8.3	1.97	1.081368	14.12366	119.4812	99.10215	0.829437
589	583	50.07	27.69	15.52	5.44	1.22	0.06	0	0	0	50.07	48.65	1.28	49.93	22.24	6.72	1.28	1.073478	17.78931	143.8585	116.2327	0.807966
591	586	50.63	22.74	16.21	8.2	2.14	0.08	0	0	0	50.63	47.15	2.22	49.37	26.63	10.42	2.22	1.128898	19.12541	159.8911	133.3366	0.833922
593	588	53.17	22.26	15.79	7.07	1.66	0.06	0	0	0	53.17	45.12	1.72	46.84	24.58	8.79	1.72	1.103875	15.44	117.86	97.5025	0.827274
595	590	51.48	24.61	14.75	6.82	2.02	0.31	0	0	0	51.48	46.19	2.33	48.51	23.9	9.15	2.33	1.095042	12.58391	100.6552	84.49195	0.83942
597	593	51.33	21	15.96	8.62	2.66	0.42	0	0	0	51.33	45.58	3.09	48.66	27.66	11.7	3.09	1.16029	15.64266	118.9972	107.7784	0.905722
599	595	54.7	20.2	14.72	8.13	2.21	0.03	0	0	0	54.7	43.05	2.24	45.29	25.09	10.37	2.24	1.132616	16.33125	126.6188	113.5625	0.896885
601	598	54.48	19.83	14.59	8.08	2.68	0.34	0	0	0	54.48	42.5	3.02	45.52	25.69	11.1	3.02	1.062157	14.79634	110.5849	93.56136	0.846059
603	600	49.11	19.48	16.82	11.28	3.25	0.06	0	0	0	49.11	47.58	3.31	50.89	31.41	14.59	3.31	1.170151	17.36607	127.6101	114.7619	0.899317
605	602	54.03	20.97	15.23	7.94	1.8	0.02	0	0	0	54.03	44.14	1.82	45.96	24.99	9.76	1.82	1.100756	17.14245	128.6154	107.7863	0.838052
607	605	51.18	21.56	16.11	8.9	2.23	0.03	0	0	0	51.18	46.57	2.25	48.83	27.27	11.16	2.25	1.100713	15.81313	116.404	96.67929	0.830549
609	607	51.85	20.69	15.35	9.4	2.67	0.05	0	0	0	51.85	45.43	2.72	48.16	27.47	12.12	2.72	1.153869	23.63504	166.4781	141.1131	0.847638
611	609	54.86	25.06	13.87	5.17	1.03	0.01	0	0	0	54.86	44.1	1.04	45.14	20.08	6.21	1.04	1.003601	14.41667	104.3148	82.57639	0.791607
613	612	55.41	21.89	14.66	6.54	1.45	0.05	0	0	0	55.41	43.09	1.51	44.59	22.7	8.04	1.51	1.039903	14.52798	108.4599	86.67883	0.799179
615	614	52.78	23.79	14.94	6.76	1.69	0.03	0	0	0	52.78	45.49	1.73	47.21	23.42	8.48	1.73	1.113963	15.88298	117.4681	99.1516	0.844073
617	617	54.5	21.58	15.25	6.39	1.85	0.43	0	0	0	54.5	43.22	2.28	45.5	23.92	8.67	2.28	1.070454	16.4322	125.435	102.6215	0.818124
619	619	54.75	21.53	15.01	6.72	1.83	0.15	0	0	0	54.75	43.26	1.99	45.24	23.71	8.7	1.99	1.083377	13.90431	106.2368	89.40191	0.841534

		>8um	>16um	>32um	>64um		
Original	Original	0.888924	0.918979	0.898392	0.847635		

	Original				
	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
>8um	0.888924	0.404022	0.179432	0.490025	0.623926
>16um	0.918979	0.409592	0.15759	0.507835	0.676282
>32um	0.898392	0.404882	0.137977	0.496107	0.680155
>64um	0.847635	0.419218	0.168177	0.514968	0.673439

Appendix 1 - B Depth Rei	lienen 7 / al depth '	A %Clay	%Very Fine	%Fine Silt	%Coarse S	%Very Fine	%Fine San	%Middle C	%Coarse S	%Very Coa	rse Sand		1									
EAE	521	< 8 fm	8-16 fm	16-32 łm	32-63 łm	63-125 tm	125-250 7	250-500 tn	500-1000 1	1000-2000	Clay	Silt	Sand	P95								
545	531	43.03	20.2	19.57	10.2	4.44	0.51	0	0	0	43.03	47.59	4.95	52.6								
549 551	536 538	51.14 49.46	20.12	15.98 16.71	9.07	3.3 3.41	0.4	0	0	0	51.14 49.46	45.17	3.69	52.6 52.6								
553	541	54.84	23.51	14.56	5.54	1.36	0.19	0	0	0	54.84	43.61	1.55	37.2								
555 557	543 545	52.79 51.51	22.81 21.46	16.62 17.27	6.29 7.57	1.21	0.27	0	0	0	52.79 51.51	45.72 46.3	1.48 2.18	37.2 37.2								
559	548	52.81	21.58	16.7	7	1.57	0.34	0	0	0	52.81	45.28	1.91	37.2								
561	550	51.85	25.29	15.39	5.67	1.47	0.33	0	0	0	51.85	46.35	1.8	37.2								
565	555	52.96	22.09	15.86	7.04	1.84	0.34	0	0	0	52.96	44.82	2.22	37.2								
567	557	46.65	21.43	19.65	9.57	2.27	0.43	0	0	0	46.65	50.65	2.71	44.2								
509	560	34.95	16.47	21.80	16.68	5.41	0.58	0	0	0	34.95	56.16	5.99	62.5								
573	564	29.43	15.56	24.19	22.35	7.84	0.64	0	0	0	29.43	62.1	8.48	74.3								
575 577	567 569	42.6 45.23	20.5 23.41	21.9 18.07	12.29 9.17	2.25	0.45	0	0	0	42.6 45.23	54.7 50.66	2.71 4.11	44.2 52.6								
579	571	48.21	26.09	17.19	6.33	1.95	0.22	0	0	0	48.21	49.62	2.17	37.2								
581 583	574 576	49.83	26.87 26.04	16.11 16.53	5.09 7.13	1.45 2.35	0.64	0	0	0	49.83	48.07	2.09	37.2								
585	579	51.61	21.09	16.64	8.33	2.1	0.22	0	0	0	51.61	46.07	2.32	44.2								
587 589	581 583	55.57 50.07	21.14	15 15.52	6.32 5.44	1.54	0.44	0	0	0	55.57 50.07	42.46	1.97	37.2								
591	586	50.63	22.74	16.21	8.2	2.14	0.08	0	0	0	50.63	47.15	2.22	44.2								
593	588 590	53.17 51.48	22.26 24.61	15.79 14.75	7.07	1.66	0.06	0	0	0	53.17	45.12	1.72	37.2								
597	593	51.33	21	15.96	8.62	2.66	0.42	0	0	0	51.33	45.58	3.09	44.2								
599 601	595 598	54.7 54.48	20.2	14.72 14.59	8.13	2.21	0.03	0	0	0	54.7 54.48	43.05	2.24	44.2								
603	600	49.11	19.48	16.82	11.28	3.25	0.06	0	0	0	49.11	47.58	3.31	52.6								
605	602	54.03	20.97	15.23	7.94	1.8	0.02	0	0	0	54.03	44.14	1.82	44.2								
609	607	51.18	20.69	15.35	9.4	2.23	0.03	0	0	0	51.85	45.43	2.23	44.2								
611	609	54.86	25.06	13.87	5.17	1.03	0.01	0	0	0	54.86	44.1	1.04	31.3								
615	612	52.78	23.79	14.00	6.76	1.45	0.05	0	0	0	52.78	43.09	1.51	37.2								
617	617	54.5	21.58	15.25	6.39	1.85	0.43	0	0	0	54.5	43.22	2.28	37.2								
619	619	54.75	21.53	15.01	0.72	1.63	0.15	U	U	U	54.75	43.20	1.99	37.2								
	t	Al	Si	Р	s	CI A	Ar	к	Ca	Sc	Ti	v	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	As	
545 547	531	0.000489	0.006805	8.2E-05 2.85E-05	0.001611	1.05E-05 0	0.00315	0.061939	0.181406	1.41E-05 0	0.051995	0.002212	0.003321	0.059057	2.362008	0.023534	0.000729	7.96E-05 7.61E-05	0.011779	0.002664	0.006288	
549	536	0.000452	0.007172	7.21E-05	0.000969	0	0.002317	0.061772	0.207834	0	0.053043	0.001902	0.003	0.083337	2.400696	0.022236	0.000745	5.76E-05	0.011898	0.002026	0.00623	
551	538	0.000486	0.007056	5.79E-05	0.001249	0	0.002184	0.064014	0.201682	0	0.052679	0.001909	0.003244	0.061562	2.381687	0.022578	0.000613	4.85E-05	0.011355	0.001833	0.005107	
555	541	0.000331	0.007357	9.33E-05 7.84E-05	0.001236	1.09E-05	0.001761	0.065584	0.200544	0	0.053236	0.001921	0.002959	0.057968	2.359729	0.022581	0.00059	0.85E-05 0	0.012098	0.002819	0.007461	
557	545	0.000471	0.007453	4.4E-05	0.001082	0	0.002741	0.06514	0.201481	0	0.054867	0.002192	0.00304	0.042392	2.266525	0.02066	0.000668	5.95E-05	0.011677	0.003501	0.005266	
559 561	548 550	0.000416	0.007133	0.000108 3.92F-05	0.001209	0	0.001894	0.062617	0.190636	1.42E-05	0.053516	0.001781	0.002977	0.050232	2.332177	0.021663	0.000717	2.13E-05	0.012209	0.002171	0.006272	
563	552	0.000439	0.006492	7.79E-05	0.001282	2.98E-05	0.001718	0.060558	0.237261	0	0.048521	0.001883	0.00314	0.08475	2.557139	0.024067	0.000442	2.41E-05	0.010482	0.002137	0.00595	
565	555	0.000386	0.006308	0	0.001301	9.66E-06	0.001593	0.059309	0.234784	0	0.048904	0.001897	0.002788	0.080826	2.517826	0.022254	0.00039	0	0.010688	0.002039	0.00753	
567 569	557 560	0.000428	0.006699	5.34E-05 0.000111	0.00109	3.44E-05 0	0.00165	0.061059 0.06168	0.187239 0.164817	0	0.050958	0.00199	0.003246	0.044957 0.067251	2.248352 2.525628	0.021804 0.022936	0.000642	5.93E-05 3.37E-05	0.011451 0.011025	0.002676 0.00163	0.006141	
571	562	0.000469	0.007236	7.03E-05	0.001244	0	0.001627	0.06262	0.167575	0	0.055232	0.002074	0.003409	0.046209	2.359676	0.021834	0.001097	0.000127	0.012676	0.002565	0.00627	
573 575	564 567	0.000351	0.006703	7.63E-05 9.65E-05	0.00108	0 9.06E-05	0.001436	0.060991	0.111638	0	0.056042	0.002032	0.003454	0.055358	2.407531 2.43761	0.022994	0.001105	0 5.06E-05	0.012488	0.00247	0.006245	
577	569	0.000439	0.006193	6.13E-05	0.001064	0	0.001371	0.060771	0.182191	0	0.052395	0.00186	0.003666	0.061579	2.447283	0.023638	0.000552	3.54E-05	0.011716	0.002478	0.006433	
579 581	571 574	0.000379	0.007096	0.000138 4.35E-05	0.001309	2.11E-05	0.001361	0.062354	0.165549	0	0.053508	0.002275	0.003183	0.053368	2.402153	0.021943	0.000714	0 8.23E-06	0.011226	0.001861	0.006637	
583	576	0.000275	0.006351	6.07E-05	0.001144	1.09E-05	0.001553	0.062574	0.200284	4.12E-05	0.051761	0.001875	0.002946	0.105718	2.639957	0.023979	0.000486	0	0.011297	0.002	0.005878	
585	579	0.000373	0.006224	8.2E-05	0.001065	4.92E-05	0.001291	0.059596	0.182018	0	0.050831	0.002023	0.00306	0.099746	2.422016	0.021714	0.000929	0	0.012072	0.002092	0.007528	
589	583	0.000432	0.007384	6.64E-05	0.001035	9.49E-05	0.001055	0.061064	0.193259	0	0.056743	0.002023	0.003164	0.054636	2.104424	0.0220281	0.000985	3.68E-05	0.011557	0.002476	0.006564	
591	586	0.000461	0.008979	0.000111	0.001118	0	0.001409	0.0569	0.298224	0	0.051381	0.00135	0.002661	0.047759	1.82751	0.017624	0.001205	0	0.010124	0.002423	0.006642	
595	590	0.000328	0.007208	0.000117	0.00103	0	0.001837	0.059347	0.230334	9.34E-00 0	0.051038	0.001904	0.003033	0.042128	2.016871	0.020401	0.000981	0	0.010734	0.002110	0.006338	
597	593	0.000488	0.006903	6.63E-05	0.00113	4.19E-05	0.002369	0.061741	0.182971	0	0.053493	0.001675	0.003383	0.046095	2.291696	0.022056	0.000891	1.28E-05	0.011856	0.002245	0.006304	
601	595	0.000326	0.006059	9.08E-05 3.89E-05	0.001241	1.22E-05	0.001292	0.059861	0.190996	0	0.051345	0.001933	0.002859	0.056378	2.375968	0.02148	0.000511	5.34E-05	0.011439	0.001881	0.005528	
603	600	0.000445	0.006469	2.45E-05	0.001136	9.32E-06	0.001586	0.058981	0.206235	0	0.048729	0.001901	0.003242	0.047941	2.220108	0.021231	0.000692	0	0.011356	0.002141	0.005824	
605	602	0.000274	0.006491	9.13E-05	0.001053	2.2E-05	0.001296	0.058364	0.212446	0	0.048677	0.001797	0.003027	0.055583	2.220242	0.021146	0.000505	2.09E-05 0	0.011069	0.001765	0.005921	
609	607	0.000456	0.006766	8.19E-05	0.001104	1.99E-05	0.001387	0.061512	0.191038	0	0.052218	0.002242	0.002957	0.075028	2.443062	0.023343	0.000314	5.85E-06	0.011853	0.0022	0.006547	
611 613	609 612	0.000572	0.00669	8.7E-05 0.000114	0.00108	0 3.28E-05	0.00135	0.058317	0.171676	0 2.11E-05	0.049477	0.001767	0.003037	0.063691	2.234296	0.021636	0.000644	0 8.55E-05	0.011518	0.001829	0.006214	
615	614	0.000389	0.006038	3.02E-05	0.001433	0	0.00104	0.05601	0.180769	0	0.045976	0.001853	0.003138	0.063342	2.180507	0.019492	0.000457	2.8E-05	0.011273	0.001796	0.006864	
617 619	617 619	0.000318	0.007632	4.18E-05 0.000144	0.001118	0 1.67E-05	0.00135	0.064257	0.174596	0 3.47E-05	0.054039	0.002042	0.003387	0.052594	2.233237	0.021043	0.000949	8.24E-05 0.000366	0.013599	0.002014	0.005858	
545	531	Se 0.005178	Br 0.001445	Rb 0.040388	Sr 0.047901	Zr	Ag 0.000336	Cd 0.0003	Sn 0.000254	Sb 0.000241	Cs 0	Ba	Ta 0.005925	W 0.00886	Ir 0.002077	Au 0.004729	Hg 0.003935	Pb 0.002872	D1 0.005377	Mo inc 0.75282	Mo coh 2 0.24718	Zr/Rb 1.083377
547	533	0.004664	0.000709	0.040367	0.048508	0.043211	0.000523	0.000194	0.000507	0.000511	0	0.001793	0.005128	0.009219	0.001904	0.00474	0.004129	0.003492	0.004778	0.75392	0.24608	1.070454
549 551	536 538	0.004615	0.000913	0.040192	0.049244 0.04921	0.044772	0.000372	0.000238	0.000549	0.000422	0	0.001082	0.005617	0.009003	0.001743	0.004792	0.004172	0.003285	0.00414	0.753115	0.246885	1.113963
553	541	0.005362	0.001025	0.04199	0.048774	0.042142	0.000604	0.000185	0.000371	0.00071	0	0.001435	0.005431	0.008835	0.001761	0.00484	0.004223	0.002745	0.005538	0.755369	0.244631	1.003601
555 557	543 545	0.005637	0.000937	0.040429	0.050353	0.04665	0.000408	0.00028	0.00067	0.000586	0	0.001005	0.005626	0.009342	0.001548	0.004784	0.004076	0.004014	0.005414	0.751722	0.248278	1.153869
559	548	0.004485	0.000927	0.040744	0.04775	0.044849	0.000525	0.00026	0.000343	0.00053	0	0.00154	0.005493	0.008937	0.00158	0.005055	0.004757	0.003595	0.004485	0.753108	0.246892	1.100756
561	550	0.004597	0.001341	0.039141	0.049238	0.045801	0.000492	0.000243	0.000436	0.000514	0	0.001045	0.005375	0.008847	0.001412	0.004451	0.003694	0.003307	0.004655	0.753269	0.246731	1.170151
565	555	0.004664	0.001028	0.038725	0.052554	0.043861	0.000483	6.28E-05	0.000568	0.001015	0	0.000883	0.005462	0.00831	0.001561	0.005208	0.004405	0.002998	0.0053	0.751304	0.248696	1.132616
567	557	0.005237	0.000662	0.039778	0.047626	0.046154	0.000214	0.000255	0.000287	0.000599	0	0.001138	0.005478	0.009127	0.001752	0.004721	0.003907	0.003331	0.004133	0.754574	0.245426	1.16029
571	562	0.005424	0.001347	0.040432	0.04505	0.044273	0.000332	0.000281	0.000131	0.000199	0	0.000939	0.005551	0.008725	0.002327	0.005048	0.004135	0.002555	0.003285	0.754142	0.247342	1.103875
573	564	0.005577	0.000622	0.041398	0.042662	0.046735	0.000488	9.95E-05	6.36E-05	0.000155	0	0.001416	0.006085	0.009525	0.001786	0.004637	0.004226	0.003928	0.005348	0.756122	0.243878	1.128898
575	567	0.005025	0.00095	0.040528	0.045418	0.043506	0.000372	0.000175	0.000299	0.000167	0	0.001071	0.005624	0.009073	0.002165	0.005007	0.003835	0.003047	0.005839	0.752148	0.243852	1.073478
579	571	0.004878	0.000741	0.040373	0.046046	0.045295	0.000473	0.000273	0.000226	0.000307	0	0.001395	0.005829	0.009075	0.002111	0.005183	0.004383	0.003173	0.004796	0.753239	0.246761	1.121932
581 583	574 576	0.005101	0.000762	0.039629	0.048922	0.044516	0.000366	0.00049	0.000252	0.000511	0	0.001097	0.005493	0.009042	0.001678	0.004586	0.004224	0.004036	0.004656	0.753108	0.246892	1.123313
585	579	0.005122	0.001122	0.039546	0.045916	0.043707	0.000613	0.000179	0.000414	0.000436	8.2E-06	0.001366	0.005474	0.008769	0.001634	0.00499	0.003786	0.003347	0.005712	0.754992	0.245008	1.10522
587	581	0.004701	0.001687	0.035037	0.051453	0.043324	0.000438	0.000243	0.000573	0.001111	0	0.001122	0.005489	0.008449	0.001948	0.004762	0.004078	0.003192	0.004894	0.749446	0.250554	1.236536
591	586	0.004029	0.000833	0.034626	0.061358	0.057963	0.000754	0.000222	0.00085	0.001672	0	0.00114	0.005042	0.010009	0.00130	0.004576	0.004205	0.001994	0.003439	0.744268	0.255732	1.673995
593	588	0.004557	0.001442	0.036905	0.055929	0.048645	0.000396	0.000156	0.000855	0.001155	0	0.00095	0.005649	0.01004	0.001802	0.004796	0.004395	0.003894	0.004245	0.750815	0.249185	1.318132
595 597	590 593	0.004694	0.000/14	0.030929	0.055031	0.052/91	0.000262	0.00022	0.000598	0.000913	0	0.001254	0.005278	0.009899	0.001267	0.004922	0.003937	0.003311	0.003/98	0.755054	0.249932	1.146752
599	595	0.00486	0.001056	0.038831	0.048405	0.043556	0.000692	0.000156	0.000375	0.00031	0	0.000756	0.005594	0.008486	0.001808	0.00503	0.00418	0.003767	0.004275	0.755054	0.244946	1.121668
601 603	598 600	0.004542 0.004539	0.001133 0.001584	0.037883 0.038207	0.049201 0.049171	0.042675 0.042361	0.000353 0.000533	0.000189	0.000515 0.000364	0.000648	0	0.001035 0.000901	0.005378 0.005139	0.008917 0.008156	0.00162 0.001902	0.004528	0.004143 0.003817	0.003922	0.004765 0.003682	0.753263 0.753032	0.246737 0.246968	1.12649 1.108722
605	602	0.005008	0.000748	0.037761	0.048104	0.041657	0.000399	0.000275	0.000478	0.000546	0	0.000997	0.005332	0.008443	0.002017	0.004636	0.003832	0.003142	0.004612	0.754724	0.245276	1.103164
607 609	605 607	0.005152	0.001554	0.038096	0.048499	0.042313 0.041395	0.000474	0.00023	0.000639	0.000675	0	0.000795	0.005551	0.00854	0.001641	0.005365	0.004035	0.003014	0.004416	0.755093	0.244907	1.110693
611	609	0.004874	0.0012	0.039214	0.047068	0.045457	0.000275	0.000224	0.000375	0.000427	0	0.000994	0.005024	0.008557	0.001753	0.00449	0.004145	0.003486	0.004464	0.750995	0.249005	1.159216
613		0.004053	0.001006	0.038002	0.048936	0.04542	0.000421	0.000286	0.000337	0.000533	0	0.001084	0.00489	0.00817	0.002153	0.004931	0.004131	0.003393	0.003964	0.75296	0 24704	1.195206
615	612	0.004357	0.001100	0.038090	0.047441	0.044996	0.000/19	0.000204	0.000/172	0.000663	0	0.000883	0.004652	0.007722	0.001621	0.004639	0.004101	0.003091	0.004941	0.754460	0.245521	1.153912
615 617	612 614 617	0.004357 0.004722 0.005391	0.0011000 0.001101 0.001123	0.038989 0.040293	0.047441 0.046927	0.044986 0.047909	0.000418 0.000636	0.000294 0.000262	0.000472 0.000274	0.000663 0.00048	0 0	0.000882 0.001583	0.004653 0.005811	0.007733 0.009316	0.001621 0.001563	0.004638 0.004406	0.004101 0.00421	0.003081 0.004049	0.004841 0.00482	0.754469 0.757696	0.245531 0.242304	1.153813 1.188998

Appendix 1	- Bienen 6 E	3																				
Depth	Real depth	%Clay	%Very Fine	Sine Silt	%Coarse S	%Very Fine%	%Fine San %	Middle C%	Coarse S%V	ery Coars	e Sand							Original				
		- < 8 才m	8-16 才m	16-32 † m	32-63 才m (- 63-125 才m 1	25-250 才n 2	50-500 才n 50	00-1000 7 100	00-2000 CI	lay S	Silt S	Sand	>8um	>16um	>32um	>64um	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
453	431	45.58	20.26	18.49	11.01	4.06	0.6	0	0	0	45.58	49.76	4.67	54.42	34.16	15.67	4.67	1.673786	3.573529	61.34559	187.8456	3.062088
455	434	48.14	20.92	18.31	9.4	2.9	0.33	0	0	0	48.14	48.63	3.23	51.86	30.94	12.63	3.23	1.396001	13.12	116.45	251.35	2.158437
457	436	50.56	23.25	15.94	7.63	2.21	0.41	0	0	0	50.56	46.82	2.62	49.44	26.19	10.25	2.62	1.356318	12.28906	156.7344	216.5234	1.381467
459	439	42.64	19.8	19.3	13.28	4.58	0.4	0	0	0	42.64	52.38	4.98	57.36	37.56	18.26	4.98	1.345212	10.13636	127.9148	168.8011	1.319638
461	441	38.54	18.68	21.54	15.71	5.12	0.42	0	0	0	38.54	55.92	5.53	61.47	42.79	21.25	5.53	1.82733	24.2987	304.5195	507.2857	1.665856
463	444	32.97	17.76	23.39	19.45	6.02	0.41	0	0	0	32.97	60.6	6.43	67.03	49.27	25.88	6.43	1.692488	9.074286	126.0457	198.0114	1.570949
465	446	32.1	16.35	22.03	16.89	9.22	3.4	0.01	0	0	32.1	55.27	12.63	67.9	51.55	29.52	12.63	1.846883	12.93836	152.4795	250.8219	1.644956
467	449	50.31	22.59	17.24	7.72	1.73	0.41	0	0	0	50.31	47.55	2.14	49.69	27.1	9.86	2.14	1.606679	13.01316	140.7105	223.7829	1.590378
469	452	53.25	22.85	15.53	6.2	1.77	0.39	0	0	0	53.25	44.59	2.16	46.74	23.89	8.36	2.16	1.284672	13.57143	174.1518	221.5714	1.272289
471	454	51.66	21.41	16.67	7.55	2.14	0.58	0	0	0	51.66	45.63	2.71	48.35	26.94	10.27	2.71	1.34495	10.21233	142.5068	186.8836	1.311401
473	457	50.51	26.04	15.64	5.92	1.55	0.35	0	0	0	50.51	47.6	1.89	49.5	23.46	7.82	1.89	1.292456	6.038647	93.77778	126.6232	1.350247
475	459	50.34	22.69	16.74	7.65	2.12	0.45	0	0	0	50.34	47.09	2.57	49.65	26.96	10.22	2.57	1.290331	10.8	182.7238	247.9524	1.356979
477	462	52.18	21.28	16.36	7.83	2.08	0.28	0	0	0	52.18	45.47	2.35	47.83	26.55	10.19	2.35	1.236731	10.11765	186.5	251.7353	1.349787
479	465	47.09	21.73	19.16	9.24	2.27	0.5	0	0	0	47.09	50.14	2.77	52.9	31.17	12.01	2.77	1.34839	9.105769	175.8077	270.1058	1.536371
481	467	51.02	24.45	16.27	6.47	1.47	0.33	0	0	0	51.02	47.18	1.8	48.99	24.54	8.27	1.8	1.376345	7.05303	133.4318	221.0076	1.656333
483	470	49.51	20.72	17.77	9.38	2.43	0.19	0	0	0	49.51	47.88	2.61	50.49	29.77	12	2.61	1.275792	12.32673	209.604	274.9901	1.311951
485	472	47.87	19.95	17.66	11.04	3.36	0.12	0	0	0	47.87	48.65	3.48	52.13	32.18	14.52	3.48	1.338066	8.902299	123.431	161.4138	1.307725
487	475	41.55	18.62	19.14	14.75	5.62	0.32	0	0	0	41.55	52.51	5.94	58.45	39.83	20.69	5.94	1.420341	11.4964	151.9496	219.9281	1.44/3/5
489	4//	51.73	22.39	16.43	7.3	1.84	0.31	0	0	0	51.73	46.12	2.16	48.27	25.88	9.45	2.16	1.338621	12.06667	153.0519	213.1481	1.392653
491	480	50.29	21.83	17.42	8.25	2.08	0.14	0	0	0	50.29	47.49	2.22	49.72	27.89	10.47	2.22	1.26/15	19.5/4/1	2/3.9425	329.7356	1.203667
493	483	49.7	22.82	17.53	7.74	1.87	0.33	0	0	0	49.7	48.1	2.2	50.29	27.47	9.94	2.2	1.339688	15.55814	185.2403	223.8837	1.208612
495	485	49.88	24.22	16.61	7.03	1.93	0.33	0	0	0	49.88	47.86	2.26	50.12	25.9	9.29	2.26	1.2/4814	7.85	96.26538	105.5154	1.096089
497	488	48.8	21.07	17.44	9.39	2.96	0.34	0	0	0	48.8	47.9	3.3	51.2	30.13	12.69	3.3	1.314975	16.64925	196.3209	220.5821	1.123579
499	490	45.64	20.32	17.77	10.75	4.91	0.62	0	0	0	45.64	48.83	5.53	54.37	34.05	16.28	5.53	1.346338	9.430962	109.3305	128.5105	1.175431
501	493	49.47	22.79	16.18	8.39	2.91	0.27	0	0	0	49.47	47.35	3.18	50.54	27.75	11.57	3.18	1.2/1152	26.82796	295./52/	320.1935	1.08264
503	495	49.76	21.25	16.98	8.84	2.77	0.4	0	0	0	49.76	47.07	3.1/	50.24	28.99	12.01	3.1/	1.251/62	12 17.20119	205.8209	205.4104	0.998006
505	498	53.05	22.14	10.09	0.00	1.07	0.37	0	0	0	53.05	44.71	2.24	40.95	24.81	9.12	2.24	1.108105	11 72200	148.8030	141.1001	0.947888
507	501	53.3	21.91	10.33	0.02	1.56	0.35	0	0	0	55.5	44.77	1.95	40.09	24.70	0.45	1.95	1.130204	11./5290	220 5770	149.4007	0.9745
509	505	51.24	21.20	16.05	7.71	2.41	0.39	0	0	0	51.24	45.90	2.0	40.70	27.31	10.01	2.0	1.144004	17 /2025	220.5776	217.1401	1 0/9806
512	500	47 47	21.50	17.91	10.26	2.34	0.47	0	0	0	17.40	40.73	2.02	52 54	20.57	12 21	2.02	1 2/0717	0 910045	120 / 926	1/10 2607	1 06200
515	511	41.41	21.32	17.01	0.20	2.07	0.00	0	0	0	47.47	49.30	2.35	50.77	20.90	12.21	2.33	1 250224	0 67/022	142 5746	162 559	1 12222
517	514	49.22	20.00	17.27	10.05	2.04	0.50	0	0	0	49.22	47.37	J.4 4.6	52 52	23.05	15.02	J.4 4.6	1 222150	16 25052	272 9762	212 0175	1 1/2551
510	516	40.47	20.19	17.16	0.35	3.57	0.04	0	0	0	40.47	40.55	3.64	51.29	30.24	13.50	3.64	1 29638/	10.35052	273.8703	25/ 322	1.142551
521	510	40.71	21.00	17.10	9.40	3.72	0.52	0	0	0	40.71	47.05	3.88	51.25	30.23	13.07	3.88	1 297377	18 371/13	273 181	312 8286	1 1/15133
523	521	40.1	20.68	17.32	5.05 11 1	3.27	0.01	0	0	0	40.1	40.01	1 24	54.01	30.85	15.31	1 24	1 338202	9 /1358	162 ////	200 2000	1 222/82
525	521	46 60	20.00	17 39	10.71	4 13	0.35	0	0	0	46.69	48 71	4.24	53 21	32.55	15 21	4.24	1 456814	9 4113/8	163 5106	237 2128	1 4507/8
525	524	45.03	19.92	17.50	12 34	4 52	0.44	0	0	0	45.67	49.71	4.55	54 24	34 98	17 2	4.55	1 537115	15 35632	246 49/3	379 6377	1 540126
520	520	53 27	21.65	16 17	7.05	1.68	0.17	0	0	0	53 27	40.57	1.90	46 72	25.07	27.5	1.90	1 215163	10 369/3	152 5222	182 8471	1 198877
529	529	55.27	21.00	10.17	1.05	1.00	0.17	0	U	U	55.27	44.07	1.00	40.72	25.07	0.9	1.00	1.213103	10.30343	132.3223	102.04/1	1.130022

>8um >16um >	>32um	>64um
Original Original 0.786676 0.759489 NO SHIFT NEEDED	0.73804	0.696085

	Original				
	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
>8um	0.786676	0.009322	-0.03262	0.251967	0.344453
>16um	0.759489	0.04078	0.0113	0.280017	0.328198
>32um	0.73804	0.049424	0.022696	0.268831	0.301973
>64um	0.696085	0.039014	-0.0047	0.201959	0.274014
andiv 1 Dianon 6 A

Depth	Real depth	A %Clay	%Very Fine	%Fine Silt	%Coarse S	%Very Fine	%Fine San	%Middle C	Coarse S	Very Coa	rse Sand	Cilt	Rond	DOF								
453	431	45.58	20.26	18.49	11.01	4.06	0.6	250-500 (11)	0	0	45.58	49.76	4.67	52.6								
455 457	434 436	48.14 50.56	20.92	18.31 15.94	9.4 7.63	2.9	0.33	0	0	0	48.14 50.56	48.63	3.23	44.2								
459 461	439 441	42.64 38.54	19.8 18.68	19.3 21.54	13.28 15.71	4.58 5.12	0.4 0.42	0	0	0	42.64 38.54	52.38 55.92	4.98 5.53	62.5 62.5								
463 465	444 446	32.97 32.1	17.76 16.35	23.39	19.45 16.89	6.02	0.41	0	0	0	32.97	60.6 55.27	6.43 12.63	62.5 105								
467	449	50.31	22.59	17.24	7.72	1.73	0.41	0	0	0	50.31	47.55	2.14	37.2								
469 471	452 454	53.25 51.66	22.85 21.41	15.53 16.67	6.2 7.55	1.77 2.14	0.39 0.58	0	0	0	53.25 51.66	44.59 45.63	2.16	37.2 44.2								
473 475	457 459	50.51 50.34	26.04 22.69	15.64 16.74	5.92 7.65	1.55 2.12	0.35 0.45	0	0	0	50.51 50.34	47.6 47.09	1.89 2.57	37.2 44.2								
477	462	52.18	21.28	16.36	7.83	2.08	0.28	0	0	0	52.18	45.47	2.35	44.2								
479	463	51.02	24.45	16.27	6.47	1.47	0.33	0	0	0	51.02	47.18	1.8	37.2								
483 485	470 472	49.51 47.87	20.72 19.95	17.77 17.66	9.38 11.04	2.43 3.36	0.19 0.12	0	0	0	49.51 47.87	47.88 48.65	2.61 3.48	44.2 52.6								
487 489	475 477	41.55 51.73	18.62	19.14 16.43	14.75	5.62 1.84	0.32	0	0	0	41.55	52.51 46.12	5.94 2.16	62.5 37.2								
403	480	50.29	21.83	17.42	8.25	2.08	0.14	0	0	0	50.29	47.49	2.22	44.2								
493 495	483	49.7 49.88	22.82	17.53 16.61	7.74	1.87	0.33	0	0	0	49.7	48.1 47.86	2.2	44.2 37.2								
497 499	488 490	48.8 45.64	21.07 20.32	17.44 17.77	9.39 10.75	2.96 4.91	0.34 0.62	0	0	0	48.8 45.64	47.9 48.83	3.3 5.53	44.2 62.5								
501	493	49.47	22.79	16.18	8.39	2.91	0.27	0	0	0	49.47	47.35	3.18	44.2								
505	498	53.05	22.14	15.69	6.88	1.87	0.37	0	0	0	53.05	44.71	2.24	37.2								
507 509	501 503	53.3 51.24	21.91 21.25	16.33 16.7	6.52 8.01	1.58 2.41	0.35 0.39	0	0	0	53.3 51.24	44.77 45.96	1.93 2.8	37.2 44.2								
511 513	506 508	51.46 47.47	21.96 21.52	16.05 17.81	7.71 10.26	2.34 2.87	0.47	0	0	0	51.46 47.47	45.73 49.58	2.82	44.2 44.2								
515	511	49.22	20.88	17.27	9.22	2.84	0.56	0	0	0	49.22	47.37	3.4	44.2								
517	514 516	46.47 48.71	20.19 21.06	17.78	10.95 9.43	3.97	0.64	0	0	0	46.47	48.93 47.65	4.6 3.64	52.6								
521 523	519 521	48.1 45.98	21.07 20.68	17.32 17.99	9.63 11.1	3.27 3.89	0.61 0.35	0	0	0	48.1 45.98	48.01 49.77	3.88 4.24	52.6 52.6								
525	524	46.69	20.62	17.38	10.71	4.13	0.47	0	0	0	46.69	48.71	4.59	52.6								
527	526	45.67	21.65	17.68	7.05	4.52	0.44	0	0	0	45.67 53.27	49.37	4.96	37.2								
		Al	Si	P	s	CI /	Ar	к	Ca	Sc ·	Ti	v	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	As	
453 455	431 434	0.000279 0.000186	0.000998 0.002436	0.000265 0.000236	0.007913 0.038046	5.34E-05 0.000108	0.009093 0.007102	0.014534 0.022147	0.168878 0.557835	0.000127 0.000173	0.017125 0.021617	0.000936 0.000887	0.001548 0.00171	0.020865 0.032802	1.005977 1.375094	0.01161 0.015651	0.000577 0.000488	0.000269 8.17E-05	0.005404 0.006521	0.001193 0.000863	0.003309 0.003826	
457	436	0.000212	0.00261	0.000119	0.00355	0	0.006014	0.034659	0.204641	3.48E-05	0.033293	0.001489	0.002297	0.037024	1.750361	0.017066	0.000906	0.000103	0.008885	0.001927	0.004358	
459 461	439	0.000283	0.00287	8.85E-05 0.000177	0.002322	7.08E-05 0	0.005296	0.037627	0.185191 0.157416	0 9.33E-06	0.03622	0.00125	0.002653	0.036562	1.871509	0.017924 0.014499	0.00079	0.000159	0.009828	0.002228	0.003369	
463 465	444 446	0.000283	0.002566	2.1E-05 7.22E-05	0.001097	1.78E-05 0	0.006464	0.033061	0.151002	1.94E-05 4.01E-05	0.035643	0.000965	0.0025	0.031111	1.549826	0.015627	0.000816	0.000692	0.008613	0.002031	0.002584	
467	449	0.000234	0.003046	0.000102	0.001243	0	0.006019	0.035315	0.161835	4.93E-05	0.03294	0.001409	0.00237	0.032283	1.531051	0.014605	0.001207	0.000265	0.008121	0.002261	0.003305	
469 471	452 454	0.00018	0.002438	0.000104 3.34E-05	0.004209	0	0.006027	0.033294 0.034127	0.225212 0.179882	2.89E-05 6.99E-05	0.031288	0.0011	0.002352	0.059377	1.808266	0.017656	0.000828	0.000212	0.008813	0.001141 0.001215	0.004618	
473	457 459	0.000327	0.001976	0.000101 7.86E-05	0.001171	9.48E-05	0.006845	0.031359	0.168759	5.22E-05	0.030685	0.001397	0.002314	0.052807	1.72602	0.016218	0.000806	0.000182	0.008623	0.002031	0.003324	
475	462	0.000165	0.001666	8.72E-05	0.001174	6.46E-06	0.005966	0.030805	0.158572	1.61E-05	0.030708	0.001348	0.001824	0.083613	1.796201	0.015323	0.000315	0.000253	0.008365	0.001395	0.004296	
479 481	465 467	0.000164 0.0002	0.001494 0.00141	0.000117 0.000139	0.001877 0.003722	9.47E-05 0	0.006527 0.006389	0.027067 0.025166	0.136505 0.17086	8.52E-05 8.48E-05	0.028847 0.026673	0.001175 0.001333	0.001994 0.002031	0.03922 0.033427	1.477465 1.461418	0.014688 0.013436	0.000857 0.000622	0.00035	0.008783 0.00777	0.001573 0.001464	0.00252 0.003362	
483 485	470 472	0.00016	0.001975	0.000109 7.14E-05	0.001434	1.9E-05 1.9E-05	0.006409	0.032568	0.133882	5.08E-05 7.61E-05	0.033591	0.001442	0.002171	0.044242	1.836048	0.016512	0.00052	0.000321	0.008589	0.00175	0.004973	
487	475	0.000221	0.002546	7.49E-05	0.001507	7.97E-06	0.007159	0.032388	0.147868	7.97E-06	0.033648	0.001233	0.002508	0.035374	1.651799	0.015702	0.000854	0.000481	0.009004	0.001913	0.002684	
489 491	477	0.000216	0.002604	4.64E-05 6.02E-05	0.001199	4.96E-05 0	0.006952	0.033535	0.140169	1.44E-05 3.01E-05	0.033034	0.001456	0.002839	0.04291	1.687294	0.016405	0.001145	0.000334	0.008373	0.001871	0.003449	
493 495	483 485	0.000204 0.000423	0.003178 0.00332	5.7E-05 0.000189	0.002127 0.001596	1.11E-05 0.0006	0.006264 0.006127	0.039335 0.043044	0.174767 0.145874	0	0.037837 0.04071	0.001417 0.001825	0.0026 0.002746	0.053499 0.062914	1.840842 2.106777	0.017057 0.019191	0.000798 0.000377	0.000242 0.000426	0.008913 0.00978	0.002185 0.002235	0.003233 0.003266	
497 499	488 490	0.000214	0.003568	5.76E-05 7.33E-05	0.000816	1.28E-05	0.005297	0.047412	0.188156	8.96E-05	0.042076	0.001558	0.003188	0.039775	1.973269	0.018526	0.001011	0.001062	0.011123	0.002306	0.003922	
501	493	0.00014	0.003767	0.000109	0.001006	1.66E-05	0.005939	0.045934	0.198502	5.74E-05	0.041531	0.00178	0.002686	0.052714	2.069338	0.018962	0.000773	0.000273	0.009976	0.002007	0.003938	
503 505	495 498	0.000218	0.003759 0.004149	4.71E-05 1.59E-05	0.001061 0.001199	0	0.005381 0.004468	0.050029	0.203465	1.3E-05 0	0.044823	0.001884 0.002069	0.002908	0.06835	2.397613 2.309025	0.020988	0.00059	0.000247	0.00962	0.00222	0.003512	
507 509	501 503	0.000301	0.003536	7.26E-05 6.71E-05	0.00122	9.47E-06 0	0.00476	0.050179	0.17232	0	0.046217	0.001969	0.003119	0.057126	2.23808 2.174706	0.021588 0.019241	0.001123 0.001312	0.00077	0.010891 0.011082	0.003304	0.004282	
511	506	0.000167	0.002914	6.25E-05	0.000859	2.19E-05	0.004821	0.046817	0.156238	6.25E-06	0.044615	0.001841	0.003182	0.047566	2.139168	0.019154	0.001315	0.00065	0.011237	0.002641	0.004736	
513	508	0.00032	0.003137	5.81E-05	0.000974	6.27E-05	0.005334	0.046223	0.155249	1.38E-05	0.039759	0.001425	0.002784	0.05501	1.86745	0.021102	0.000808	0.000773	0.01082	0.002264	0.003505	
517 519	514 516	0.000152 0.000186	0.00249 0.002984	3.92E-05 8.69E-05	0.000854 0.000967	9.42E-06 9.48E-06	0.005044 0.00552	0.042428 0.046687	0.159188 0.161419	0 1.9E-05	0.041708 0.044339	0.002044 0.00177	0.002831 0.00275	0.046831 0.076026	2.021575 2.357035	0.019173 0.020474	0.001328 0.000849	0.000444 0.000428	0.010926 0.010849	0.002732 0.002933	0.003412 0.004396	
521	519	0.000156	0.002867	9.21E-05	0.001173	1.49E-05	0.005084	0.043195	0.157584	5.8E-05	0.042629	0.001502	0.002929	0.050116	1.988029	0.018837	0.001042	0.000207	0.01102	0.001547	0.003076	
525	524	0.000232	0.002023	6.1E-05	0.000906	0.00027	0.005562	0.032829	0.154491	1.24E-05	0.035153	0.001323	0.002719	0.036141	1.671128	0.016063	0.001002	0.000396	0.009133	0.002185	0.004481	
527 529	526 529	0.000138 0.000245	0.002121 0.002536	4.13E-05 9.66E-05	0.001024 0.001693	7.94E-06 7.79E-06	0.005647 0.005478	0.032992 0.038895	0.158759 0.148554	1.91E-05 2.49E-05	0.034046 0.037296	0.001032 0.001888	0.002554 0.002553	0.055899 0.050122	1.767259 1.870595	0.017168 0.017861	0.000727 0.000916	0.000324 0.00045	0.009837 0.010368	0.00195 0.002114	0.005417 0.004254	
		Se	Br	Rb	Sr :	Zr /	Ag	Cd	Sn :	Sb (Cs	Ва	Та	w	Ir	Au	Hg	Pb	D1	Mo inc	Mo coh 🛛	Zr/Rb
453 455	431 434	0.003444	0.001342	0.031329	0.041754	0.052438	0.000425	0.000507	0.000601	0.000942	1.44E-05 0	0.0007	0.00556	0.008756	0.00267	0.002896	0.002539	0.002122	0.00155	0.742778	0.257222	1.673786
457	436	0.005043	0.001047	0.033911	0.046055	0.045993	0.000466	0.000453	0.000455	0.000913	0	0.000913	0.007189	0.01169	0.002844	0.003819	0.003523	0.002916	0.002964	0.754098	0.245902	1.356318
459	439	0.005462	0.0001108	0.0333531	0.047809	0.060762	0.000551	0.000272	0.00045	0.000591	0	0.001377	0.007428	0.012021	0.002841	0.004154	0.003464	0.003765	0.002693	0.748876	0.249127	1.82733
463 465	444 446	0.004652 0.003691	0.000879 0.001127	0.033084 0.031834	0.049999	0.055994 0.058793	0.00016	0.000307 0.000416	0.000139 0.000191	0.000462 0.00034	0	0.001427 0.001116	0.007053 0.006934	0.012824 0.012146	0.002474 0.002895	0.003936 0.004361	0.003715 0.002925	0.004025 0.003545	0.002264 0.001565	0.748808 0.751824	0.251192 0.248176	1.692488 1.846883
467	449 452	0.004737	0.001117	0.032606	0.0474	0.052387	0.000216	0.000404	0.000353	0.000558	0	0.001328	0.006382	0.011982	0.002209	0.003475	0.003394	0.003813	0.00248	0.757953	0.242047	1.606679
405	454	0.004876	0.001295	0.03223	0.047723	0.043348	0.000275	0.000718	0.000461	0.000574	0	0.000855	0.006644	0.010657	0.002753	0.004175	0.003133	0.003147	0.002621	0.7551	0.2449	1.34495
473 475	457 459	0.005175 0.00492	0.001137 0.001041	0.032057 0.032356	0.047925 0.047	0.041433 0.04175	6.16E-05 0.000478	0.000528	0.000334 0.000119	0.000507	0	0.000795 0.000989	0.006059 0.006039	0.010238 0.011059	0.002309 0.002802	0.003857 0.004335	0.003261 0.003222	0.003418 0.00314	0.002567 0.002952	0.757905 0.755167	0.242095 0.244833	1.292456 1.290331
477	462 465	0.004354	0.000612	0.033516	0.047153	0.04145	0.000647	0.000323	0.00027 8.84E-05	0.000208	0	0.001046	0.006559	0.010775	0.002951	0.003836	0.004087	0.003106	0.003053	0.756436	0.243564	1.236731
481	467	0.004304	0.000681	0.032099	0.042763	0.044179	0.000233	0.000365	0.000297	0.000685	0	0.00051	0.00656	0.009943	0.002244	0.004496	0.002687	0.002755	0.0021	0.75965	0.24035	1.376345
483 485	470	0.004889	0.001338	0.034543	0.044424	0.04407	0.000162	0.000476	8.89E-05 0.000165	0.000382	0	0.001009	0.00666	0.011526	0.00271	0.003845	0.002893	0.002328	0.003251	0.758507	0.241493	1.338066
487 489	475 477	0.003674	0.000836	0.034289 0.034368	0.046132	0.048702	0.000266	0.000714	0.000147 8.79E-05	0.000384	0 1.28E-05	0.001259 0.001022	0.006132	0.010892	0.002216 0.00231	0.004019 0.004312	0.003164 0.0035	0.00282	0.003256	0.75578	0.24422	1.420341 1.338621
491	480	0.005021	0.001412	0.035879	0.044848	0.045464	0.000445	0.000655	0.000219	0.000566	0	0.001715	0.006645	0.01145	0.001897	0.00423	0.003271	0.003666	0.003691	0.758655	0.241345	1.26715
493	483	0.004646	0.000388	0.034135	0.04441	0.04573	0.000313	0.000372	0.000331	0.000496	0	0.00148	0.006765	0.011245	0.003092	0.004046	0.003731	0.003229	0.002985	0.755034	0.244966	1.274814
497 499	488 490	0.005424 0.005284	0.000411 0.000755	0.035952 0.036341	0.048944 0.050249	0.047276 0.048927	0.000611 0.000413	0.000178 0.000558	0.000274 0.000344	0.000606 0.000621	0	0.001478 0.001458	0.006647 0.007019	0.012744 0.012984	0.002412 0.002603	0.00357 0.004033	0.003647 0.003629	0.003775 0.00354	0.003298 0.003108	0.753627 0.752368	0.246373 0.247632	1.314975 1.346338
501	493	0.005031	0.001126	0.035372	0.050077	0.044963	0.000424	0.00063	0.000254	0.000767	0	0.001155	0.006759	0.012469	0.002469	0.004297	0.00342	0.002843	0.003257	0.755173	0.244827	1.271152
503	495	0.005183	0.000631	0.03803	0.047297	0.044426	0.000859	0.000188	0.000496	0.000523	0	0.001436	0.006871	0.011966	0.002393	0.00458	0.003722	0.003055	0.003446	0.752413	0.247587	1.168165
507 509	501 503	0.004381 0.005678	0.000615 0.001108	0.038952 0.039947	0.044627 0.04376	0.045039 0.045731	0.000696 0.000513	0.000323 0.000365	0.000112 0.000119	0.000806 0.000354	0	0.001448 0.001278	0.006994 0.006944	0.011871 0.011592	0.001911 0.002696	0.004362 0.004775	0.004018 0.004034	0.003984 0.003613	0.002813 0.003867	0.754956 0.755946	0.245044 0.244054	1.156264 1.144804
511 513	506 508	0.005467	0.000776	0.039607	0.045955	0.046796	0.000403	0.000283	0.000187 6.68E-05	0.000461	0	0.001273	0.007316	0.01256	0.002658	0.004824	0.004218	0.003962	0.003776	0.755941 0.753262	0.244059	1.181517 1.249717
515	511	0.00505	0.000826	0.036006	0.045771	0.045016	0.000246	0.000539	0.000135	0.000603	0	0.001036	0.007635	0.012273	0.002234	0.004013	0.003369	0.003654	0.002648	0.757907	0.242093	1.250234
517 519	514 516	0.005305	0.000958	0.038675	0.04715	0.047654	0.000479	0.000364	0.000181	0.000473	0	0.001311	0.007018	0.012481	0.002393	0.00452	0.003707	0.003985	0.003085	0.755342 0.751365	0.244658	1.296384
521 523	519 521	0.005291 0.005428	0.000826	0.037626 0.037641	0.047202 0.046034	0.048816 0.050371	0.000557 0.000416	0.000363 0.000182	0.000282	0.000538	0	0.001207 0.001008	0.007744 0.006807	0.012356 0.012538	0.003164 0.002249	0.00451 0.004276	0.003837 0.004008	0.004594 0.004891	0.003087 0.00346	0.754489 0.753046	0.245511 0.246954	1.297377 1.338202
525	524	0.005456	0.001287	0.035006	0.047119	0.050998	0.000267	0.000369	0.000319	0.000506	0	0.000765	0.007561	0.012907	0.002295	0.003871	0.003132	0.002723	0.002932	0.755647	0.244353	1.456814
527	529	0.005095	0.001252	0.036794	0.044597	0.044711	0.000389	0.00026	0.000338	0.000793	0	0.001266	0.006939	0.011183	0.002318	0.004489	0.003289	0.00376	0.003042	0.756332	0.243668	1.215163

Appendix	1 - Bienen 5 B																	1	1								
Depth	Real depth 9	%Clav	%Verv Fin∉ %	6Fine Silt	%Coarse &%	Verv Fin∉%	Fine San %I	Middle C%C	Coarse S%Ve	erv Coarse	e Sand		1					Original					Shifted Gra	ph			
		< 8 fm	B-16 才m 1€	6-32 † m	32-63 fm 63	-125 fm 12	25-250 † n 25	0-500 † n 50	0-1000 1 1000	0-2000 CI	ay S	ilt Sa	and	>8um >	16um >	32um	>64um	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
35	7 341	50.74	20.26	16.53	9.28	3.09	0.12	0	0	0	50.74	46.06	3.2	49.28	29.02	12.49	3.2	1.209674	27.95862	207.1172	212.8276	1.027571	1.207495	20.42387	152.6749	142.5391	0.933612
35	9 343	49.06	20.34	17.16	9.92	3.37	0.15	0	0	0	49.06	47.42	3.52	50.94	30.6	13.44	3.52	1.207495	20.42387	152.6749	142.5391	0.933612	1.214384	14.49485	105.9768	105.1005	0.991731
36	1 346	52.89	21.19	16.46	7.42	1.92	0.12	0	0	0	52.89	45.07	2.04	47.11	25.92	9.46	2.04	1.214384	14.49485	105.9768	105.1005	0.991731	1.159693	15.1493	113.5014	102.6704	0.904574
36	3 348	52.34	20.55	16.36	8.04	2.39	0.31	0	0	0	52.34	44.95	2.7	47.65	27.1	10.74	2.7	1.159693	15.1493	113.5014	102.6704	0.904574	1.135805	20.01172	161.8125	145.5117	0.899261
36	5 351	50.56	20.42	16.75	8.85	3.1	0.32	0	0	0	50.56	46.02	3.41	49.44	29.02	12.27	3.41	1.135805	20.01172	161.8125	145.5117	0.899261	1.089273	14.92073	130.3994	111.0793	0.851839
36	7 353	50.74	21.14	17.15	8.31	2.34	0.32	0	0	0	50.74	46.6	2.66	49.26	28.12	10.97	2.66	1.089273	14.92073	130.3994	111.0793	0.851839	1.115834	21.02917	178.6792	156.8583	0.877877
36	9 356	49.7	20.48	16.99	9.31	3.22	0.3	0	0	0	49.7	46.78	3.51	50.3	29.82	12.83	3.51	1.115834	21.02917	178.6792	156.8583	0.877877	1.237924	23.31933	184.5882	174.979	0.947942
37	1 358	45.82	19.02	16.85	11.11	5.75	1.45	0	0	0	45.82	46.98	7.19	54.18	35.16	18.31	7.19	1.237924	23.31933	184.5882	174.979	0.947942	1.264256	21.97308	153.6192	154.5115	1.005809
37	3 361	48.99	19.54	16.41	9.92	4.16	0.98	0	0	0	48.99	45.87	5.14	51.01	31.47	15.06	5.14	1.264256	21.97308	153.6192	154.5115	1.005809	1.158997	15.23324	126.1749	110.3615	0.874671
37	5 363	47.64	19.45	16.64	10.35	4.2	1.58	0.14	0	0	47.64	46.43	5.92	52.36	32.91	16.27	5.92	1.158997	15.23324	126.1749	110.3615	0.874671	1.206359	18.79355	138.4806	124.971	0.902444
37	7 365	45.02	19.39	18.34	12.12	4.59	0.55	0	0	0	45.02	49.84	5.14	54.99	35.6	17.26	5.14	1.206359	18.79355	138.4806	124.971	0.902444	1.214395	20.68641	154.5226	138.4495	0.895982
37	9 368	47.69	20.18	17.88	10.21	3.58	0.46	0	0	0	47.69	48.27	4.04	52.31	32.13	14.25	4.04	1.214395	20.68641	154.5226	138.4495	0.895982	1.343456	18.48366	132.9673	135.4608	1.018752
38	1 370	40.71	17.82	18.93	15.57	6.29	0.69	0	0	0	40.71	52.31	6.98	59.3	41.48	22.55	6.98	1.343456	18.48366	132.9673	135.4608	1.018752	1.390087	17.58286	116.2686	126.5257	1.088219
38	3 373	47.48	20.52	18.17	10.22	3.21	0.4	0	0	0	47.48	48.91	3.61	52.52	32	13.83	3.61	1.390087	17.58286	116.2686	126.5257	1.088219	1.15601	18.58966	146.9793	131.0517	0.891634
38	5 375	52.11	21.71	16.92	7.72	1.54	0.01	0	0	0	52.11	46.34	1.55	47.9	26.19	9.27	1.55	1.15601	18.58966	146.9793	131.0517	0.891634	1.187209	19.70782	159.5638	149.7984	0.938799
38	7 378	51.62	20.86	16.43	8.15	2.49	0.45	0	0	0	51.62	45.44	2.94	48.38	27.52	11.09	2.94	1.187209	19.70782	159.5638	149.7984	0.938799	1.202469	16.14763	106.532	107.6964	1.01093
38	9 380	46.72	19.52	17.06	11.54	4.76	0.41	0	0	0	46.72	48.12	5.17	53.29	33.77	16.71	5.17	1.202469	16.14763	106.532	107.6964	1.01093	1.355241	17.94576	119.7492	127.4983	1.064712
39	1 383	45.79	18.81	18.01	12.27	4.21	0.92	0	0	0	45.79	49.09	5.12	54.22	35.41	17.4	5.12	1.355241	17.94576	119.7492	127.4983	1.064712	1.282906	19.02024	131.8826	149.004	1.129823
39	3 385	53.02	21.49	14.97	6.88	2.63	1.01	0	0	0	53.02	43.34	3.64	46.98	25.49	10.52	3.64	1.282906	19.02024	131.8826	149.004	1.129823	1.143311	24.94975	214.8191	195.1558	0.908466
39	5 387	50.11	20.55	17.02	8.77	2.96	0.59	0	0	0	50.11	46.34	3.55	49.89	29.34	12.32	3.55	1.143311	24.94975	214.8191	195.1558	0.908466	1.245141	19.8412	162.6438	163.867	1.007521
39	7 390	50.28	19.71	16.9	9.4	3.21	0.5	0	0	0	50.28	46.01	3.71	49.72	30.01	13.11	3.71	1.245141	19.8412	162.6438	163.867	1.007521	1.123378	22	180.0571	174.7762	0.970671
39	9 392	51.23	21.74	15.72	8.64	2.53	0.13	0	0	0	51.23	46.1	2.67	48.76	27.02	11.3	2.67	1.123378	22	180.0571	174.7762	0.970671	1.314298	16.11355	133.8352	140.8755	1.052604
40	1 395	47.99	21.56	17.14	9.51	3.24	0.56	0	0	0	47.99	48.21	3.8	52.01	30.45	13.31	3.8	1.314298	16.11355	133.8352	140.8755	1.052604	1.233094	16.25862	155.944	167.8017	1.076039
40	3 397	47.41	20.46	17.57	9.55	3.55	1.46	0	0	0	47.41	47.58	5.02	52.59	32.13	14.56	5.02	1.233094	16.25862	155.944	167.8017	1.076039	1.147404	17.81008	150.1318	145.876	0.971653
40	5 400	50.45	21.82	17.81	8.04	1.75	0.13	0	0	0	50.45	47.67	1.87	49.55	27.73	9.92	1.87	1.147404	17.81008	150.1318	145.876	0.971653	1.135415	20.04265	167.1611	158.7536	0.949704
40	7 402	49.89	20.86	16.75	7.96	2.9	1.62	0.03	0	0	49.89	45.56	4.55	50.12	29.26	12.51	4.55	1.135415	20.04265	167.1611	158.7536	0.949704	1.724387	19.41729	144.5188	198.4925	1.373472
40	9 405	49.6	20.81	17.69	8.83	2.64	0.42	0	0	0	49.6	47.33	3.06	50.39	29.58	11.89	3.06	1.724387	19.41729	144.5188	198.4925	1.373472	1.310461	18.47692	131.1462	151.3885	1.154349
41	1 407	46.76	19.22	17.75	11.36	4.19	0.72	0	0	0	46.76	48.33	4.91	53.24	34.02	16.27	4.91	1.310461	18.47692	131.1462	151.3885	1.154349	1.238813	22.12435	178.5492	186.0466	1.041991
41	3 409	50.76	20.43	16.78	8.53	2.88	0.62	0	0	0	50.76	45.75	3.49	49.24	28.81	12.03	3.49	1.238813	22.12435	178.5492	186.0466	1.041991	1.188719	14.52924	112.652	115.9766	1.029512
41	5 412	50.19	22.73	16.59	7.8	2.2	0.49	0	0	0	50.19	47.12	2.69	49.81	27.08	10.49	2.69	1.188719	14.52924	112.652	115.9766	1.029512	1.154966	19.33721	152.4884	150.7364	0.988511
41	7 414	50.6	21.11	17.25	8.95	2.06	0.03	0	0	0	50.6	47.31	2.1	49.4	28.29	11.04	2.1	1.154966	19.33721	152.4884	150.7364	0.988511	1.156567	17.08127	137.8657	136.5689	0.990594
41	9 417	50.21	20.86	16.5	8.58	3.04	0.81	0	0	0	50.21	45.94	3.85	49.79	28.93	12.43	3.85	1.156567	17.08127	137.8657	136.5689	0.990594	1.286926	20.99298	143.5088	142.6456	0.993985
42	1 419	45.21	19.86	18.56	11.64	4.21	0.53	0	0	0	45.21	50.06	4.74	54.8	34.94	16.38	4.74	1.286926	20.99298	143.5088	142.6456	0.993985	1.250047	24.09649	174.5789	174.9956	1.002387
42	3 422	48.89	20.8	17.33	9.26	3.29	0.44	0	0	0	48.89	47.38	3.73	51.12	30.32	12.99	3.73	1.250047	24.09649	174.5789	174.9956	1.002387	1.157522	26.58571	189.2762	174.1905	0.920298
42	5 424	49.41	20.8	16.75	8.88	3.5	0.66	0	0	0	49.41	46.43	4.16	50.59	29.79	13.04	4.16	1.157522	26.58571	189.2762	174.1905	0.920298	1.220151	16.95641	110.2821	96.69231	0.876773
42	7 427	48.93	21.7	15.99	8.88	3.66	0.84	0	0	0	48.93	46.57	4.5	51.07	29.37	13.38	4.5	1.220151	16.95641	110.2821	96.69231	0.876773	1.190826	21.90671	141.7085	127.9913	0.903201
42	9 429	48.29	22.62	15.94	8.37	3.85	0.93	0	0	0	48.29	46.93	4.78	51.71	29.09	13.15	4.78	1.190826	21.90671	141.7085	127.9913	0.903201					

	Original					Shifted				
	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
>8um	0.322911	-0.00287	-0.14744	-0.10094	0.089799	0.319491	0.088393	-0.12957	0.00648	0.238375
>16um	0.323142	0.032624	-0.09852	-0.04975	0.099016	0.310755	0.070914	-0.14974	-0.02315	0.220627
>32um	0.276425	0.061952	-0.08964	-0.05782	0.063247	0.323192	0.073123	-0.15812	-0.04124	0.202523
>64um	0.197411	0.101228	-0.03247	-0.02572	0.015103	0.361464	0.129007	-0.10359	0.013989	0.201267
						Upper part	: (shifted)			
						Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
					>8um	0.731762	-0.05189	-0.3197	-0.10985	0.562768
					>16um	0.728455	-0.07115	-0.34173	-0.12946	0.570099
					>32um	0.719153	-0.03656	-0.31064	-0.098	0.56302
					>64um	0.598501	0.068642	-0.18451	-0.00808	0.441699

		>8um	>16um	>32um	>64um
Original (Original	0.322911	0.323142	0.276425	0.197411
Shifted U	Jpper part	0.319491	0.310755	0.323192	0.361464
		0 721762	0 7029/0	0.602514	0 5 8 1 0 6 8

part 2	0.731762	0.703849	0.692514	0.581068	
part 1	-0.05433	-0.02547		0.262926	

Appendix 1 - I Depth Re	Bienen 5 / al depth 9	A %Clay < 8 tm	%Very Fine 8-16 tm	%Fine Silt	%Coarse S	%Very Fine 63-125 tm 1	%Fine San '	%Middle C	%Coarse S	%Very Coa	rse Sand	Silt	AVG STDEV Sand	P95								
357	341	50.74	20.26	16.53	9.28	3.09	0.12	230-300 411	0	000-2000	50.74	46.06	3.2	44.2								
359 361	343 346	49.06 52.89	20.34 21.19	17.16 16.46	9.92 7.42	3.37 1.92	0.15	0	0	0	49.06 52.89	47.42 45.07	3.52 2.04	52.6 37.2								
363	348	52.34	20.55	16.36	8.04	2.39	0.31	0	0	0	52.34	44.95	2.7	44.2								
365	351	50.56 50.74	20.42 21.14	16.75 17.15	8.85 8.31	3.1 2.34	0.32	0	0	0	50.56 50.74	46.02 46.6	3.41 2.66	52.6 44.2								
369	356	49.7	20.48	16.99	9.31	3.22	0.3	0	0	0	49.7	46.78	3.51	52.6								
371 373	358	45.82 48.99	19.02 19.54	16.85 16.41	11.11 9.92	5.75 4.16	1.45 0.98	0	0	0	45.82 48.99	46.98 45.87	7.19 5.14	74.3 62.5								
375	363	47.64	19.45	16.64	10.35	4.2	1.58	0.14	0	0	47.64	46.43	5.92	62.5								
379	368	47.69	20.18	17.88	10.21	3.58	0.35	0	0	0	47.69	49.84	4.04	52.6								
381	370	40.71	17.82	18.93	15.57	6.29	0.69	0	0	0	40.71	52.31	6.98	62.5								
385	375	52.11	21.71	16.92	7.72	1.54	0.01	0	0	0	52.11	46.34	1.55	37.2								
387	378 380	51.62 46.72	20.86	16.43 17.06	8.15 11.54	2.49	0.45	0	0	0	51.62 46.72	45.44	2.94	44.2								
391	383	45.79	18.81	18.01	12.27	4.21	0.92	0	0	0	45.79	49.09	5.12	62.5								
393 395	385 387	53.02 50.11	21.49 20.55	14.97 17.02	6.88 8.77	2.63	1.01	0	0	0	53.02 50.11	43.34 46.34	3.64	44.2 44.2								
397	390	50.28	19.71	16.9	9.4	3.21	0.5	0	0	0	50.28	46.01	3.71	52.6								
399 401	392 395	51.23 47.99	21.74 21.56	15.72 17.14	8.64 9.51	2.53	0.13	0	0	0	51.23 47.99	46.1 48.21	2.67	44.2 52.6								
403	397	47.41	20.46	17.57	9.55	3.55	1.46	0	0	0	47.41	47.58	5.02	62.5								
405	400	49.89	21.82	17.81	7.96	2.9	1.62	0.03	0	0	49.89	47.67	4.55	52.6								
409	405	49.6	20.81	17.69	8.83	2.64	0.42	0	0	0	49.6	47.33	3.06	44.2								
411 413	407	50.76	20.43	16.78	8.53	2.88	0.62	0	0	0	50.76	48.33	3.49	44.2								
415	412	50.19 50.6	22.73	16.59 17.25	7.8	2.2	0.49	0	0	0	50.19 50.6	47.12	2.69	44.2 44.2								
419	414	50.21	20.86	16.5	8.58	3.04	0.81	0	0	0	50.21	45.94	3.85	52.6								
421	419	45.21	19.86	18.56 17.33	11.64 9.26	4.21	0.53	0	0	0	45.21 48.89	50.06 47.38	4.74	52.6 52.6								
425	424	49.41	20.8	16.75	8.88	3.5	0.66	0	0	0	49.41	46.43	4.16	52.6								
427 429	427 429	48.93 48.29	21.7 22.62	15.99 15.94	8.88 8.37	3.66 3.85	0.84 0.93	0	0	0	48.93 48.29	46.57 46.93	4.5 4.78	52.6 52.6								
257									<u>_</u>						-				-	~		
357	341	0.000203	0.005682	P 5.75E-05	0.003274	2.38E-05	Ar 0.006157	K 0.05144	Ca 0.231043	6.59E-05	0.042093	V 0.001816	Cr 0.002692	Mn 0.043898	Fe 1.970676	Co 0.019196	0.0009	6.87E-05	Zn 0.010141	Ga . 0.001793	As 0.004293	
361	346	0.000301	0.006148	5.45E-05	0.002013	4.95E-06	0.002325	0.054411	0.202253	3.84E-05	0.045956	0.001848	0.002974	0.038152	2.093014	0.020083	0.001137	8.55E-05	0.010903	0.00179	0.005267	
363 365	348 351	0.000421	0.006103	8.79E-05 4.21E-05	0.005191 0.002952	4.99E-05 1.82E-05	0.002025	0.053196	0.202834	4.45E-05 1.14E-05	0.044624	0.002109	0.002938	0.035382	2.046219 2.147032	0.018968	0.000924	0.000174 9.33E-05	0.009346	0.001702	0.005153	
367	353	0.000293	0.005869	7.56E-05	0.00133	1.37E-05	0.002115	0.054698	0.192568	6.87E-06	0.047459	0.002061	0.003265	0.041464	2.219632	0.020648	0.001139	6.3E-05	0.011567	0.002392	0.004889	
369 371	356 358	0.000372	0.005546	0.000162 7.81E-05	0.001243	0	0.001971	0.0546	0.136469	1.13E-05 0	0.048468	0.002047	0.003359	0.043438	2.326195	0.022493	0.001041	0.000155 3.51E-05	0.010931	0.001979	0.004506	
373	361	0.000259	0.006047	2.94E-05	0.00108	0	0.00211	0.056356	0.232629	0	0.04787	0.001904	0.003058	0.049508	2.117058	0.020907	0.001256	0	0.011466	0.002181	0.004728	
375	363 365	0.000295	0.006491	0.00012 1.36E-05	0.001093	0	0.002205	0.055018	0.234505	0 7.93E-06	0.045381	0.002012	0.00281	0.043949	1.973297	0.020173	0.001074	2.05E-05 7.13E-05	0.01057	0.002164	0.005276	
379	368	0.000351	0.006589	5.77E-05	0.001221	6.79E-06	0.001925	0.055476	0.124718	0	0.048553	0.001991	0.003383	0.058437	2.312465	0.021754	0.001152	0.000126	0.010329	0.001613	0.005033	
381	370	0.000322	0.006663	8.53E-05	0.001206	5.61E-06	0.002166	0.056528	0.15923	0	0.049773	0.001939	0.003065	0.03848	2.207202	0.021797	0.001226	6.06E-05	0.010833	0.002645	0.004936	
385	375	0.000334	0.006761	5.49E-06	0.001101	2.512-03	0.001751	0.051882	0.233233	0	0.047030	0.002194	0.003027	0.037337	1.980441	0.021100	0.001740	5.55E-05 0	0.010313	0.002390	0.005311	
387	378	0.000328	0.0061	6.45E-05	0.001051	9.05E-06 3.36E-05	0.001461	0.055058	0.200344	0	0.04823	0.002082	0.003094	0.0459	2.187119	0.021309	0.001225	7.35E-05	0.012027	0.001839	0.00504	
391	383	0.000415	0.006706	1.85E-05	0.001076	0	0.001342	0.053158	0.238371	5.78E-05	0.044245	0.001895	0.002755	0.05539	1.952927	0.019667	0.001305	0	0.010872	0.001388	0.005245	
393 395	385 387	0.000358	0.006433	4.13E-05 5.54E-05	0.00097	0 8.43F-06	0.001314	0.051735	0.255658	0 3.25E-05	0.042927	0.001837	0.002694	0.065667	1.955924	0.019246	0.000865	0	0.010235	0.001995	0.004302	
397	390	0.000221	0.005508	8.43E-05	0.00206	0	0.001109	0.055611	0.202786	5.55E-06	0.047421	0.002433	0.00317	0.049098	2.157289	0.021367	0.001074	0.000182	0.010712	0.001887	0.004866	
399 401	392 395	0.000267	0.005302	3.56E-05 7.95E-05	0.001137	0	0.00126	0.052212	0.236157 0.219568	2.29E-05 1.12E-05	0.043464 0.042327	0.001874 0.001991	0.002797	0.054857	2.001506 2.058546	0.02035	0.000826	0 5.93E-05	0.010769	0.001621 0.00195	0.004082	
403	397	0.00031	0.005002	5.69E-06	0.001042	9.1E-06	0.001029	0.047135	0.265461	0	0.041546	0.001619	0.002769	0.04691	1.972471	0.019927	0.000856	2.05E-05	0.010603	0.001763	0.004792	
405	400	0.000253	0.004115	5.78E-05 3.45E-05	0.001153 0.001114	0 5.57E-06	0.000831	0.043854	0.19862	1.31E-05 0	0.039472	0.001567	0.002522	0.048009	1.952996 2.040229	0.019548	0.00053	1.96E-05 3.56E-05	0.009762	0.001071 0.001377	0.004186	
409	405	0.000244	0.004883	6E-05	0.001141	4.62E-06	0.000841	0.047917	0.272782	0	0.040727	0.001778	0.002473	0.077277	2.153371	0.021718	0.00051	0	0.010533	0.001741	0.005122	
411 413	407	0.000304	0.005908	4.12E-05 5.49E-05	0.001178	1.83E-05	0.000884	0.045788	0.227834	1.49E-05 0	0.039003	0.00175	0.002582	0.046951	1.808467	0.017899	0.000812	4.69E-05 0	0.010378	0.001669	0.004708	
415	412	0.000224	0.004947	4.4E-05	0.001109	5.79E-06	0.000931	0.045978	0.255562	3.59E-05	0.03992	0.001801	0.002588	0.087163	2.217691	0.021257	0.000705	7.07E-05	0.009781	0.001631	0.005304	
419	414	0.000285	0.005505	3.2E-05	0.001175	1.99E-05	0.000919	0.049265	0.186472	0	0.041333	0.001330	0.002763	0.056654	2.057769	0.02108	0.000602	0	0.011138	0.001657	0.004817	
421 423	419 422	0.000315	0.005389	2.23E-05 4.4E-05	0.001147	2.12E-05 0	0.001049	0.049983	0.188815	0 1.35E-05	0.043492	0.001974	0.002753	0.043314	2.041709	0.020406	0.000861	2.23E-05 0	0.011168	0.001507	0.004857	
425	424	0.000261	0.006298	2.75E-05	0.00239	4.59E-06	0.001050	0.052601	0.228924	6.65E-05	0.045628	0.002081	0.002877	0.04845	2.169326	0.020407	0.000962	5.96E-05	0.011408	0.001416	0.005314	
427	427	0.000244	0.006475	0 9.41E-06	0.001215	1.86E-05	0.002372	0.052943	0.207454	3.13E-05	0.0461	0.001971	0.003071	0.047778	2.218722	0.021279	0.001079	0 4 47E-05	0.011008	0.001543	0.004758	
425		0.000376	0.008226	1.42E-05	0.002668	0	0.003675	0.06042	0.194657	0	0.053213	0.002167	0.003458	0.051913	2.319492	0.021471	0.001327	9.42E-05	0.01185	0.001606	0.003986	
	L	Se	Br	Rb	Sr	Zr /	Ag	Cd	Sn	Sb	Cs	Ва	Та	w	Ir	Au	Hg	Pb	D1	Mo inc	Mo coh	Zr/Rb
357	341	0.004826	0.001194	0.035756	0.049568	0.043254	0.000214	0.000335	0.00082	0.001627	1.26E-05	0.001374	0.005109	0.008216	0.002146	0.00468	0.003944	0.003332	0.004589	0.754177	0.245823	1.209674
359	343	0.004252	0.000855	0.035532	0.048203	0.042905	0.000604	0.000208	0.00079	0.001176	0	0.001166	0.005521	0.008524	0.001583	0.005058	0.003802	0.003109	0.003981	0.756862	0.24667	1.207495
363	348	0.004725	0.000894	0.035747	0.046083	0.041456	0.000181	0.000394	0.000863	0.001439	0	0.000959	0.005159	0.008561	0.001967	0.004802	0.003427	0.003569	0.003897	0.757531	0.242469	1.159693
367	353	0.005087	0.001004	0.037904	0.031004	0.042078	0.000207	0.000335	0.000723	0.000456	0	0.001210	0.005528	0.009203	0.001310	0.004352	0.003657	0.003574	0.004435	0.75634	0.244007	1.089273
369 371	356	0.003998	0.001672	0.038174	0.047322	0.042596	0.000316	0.000161	0.000566	0.000895	0	0.001762	0.005772	0.009057	0.001619	0.003837	0.003692	0.002592	0.004003	0.756408	0.243592	1.115834
373	361	0.004568	0.001215	0.036104	0.051271	0.045570	0.000273	0.000221	0.000668	0.001557	0	0.001186	0.005796	0.009796	0.001393	0.004063	0.003556	0.002851	0.004489	0.754516	0.245484	1.264256
375	363	0.00445	0.001429	0.036983	0.050919	0.042863	0.000377	0.000179	0.000551	0.001025	0	0.001855	0.005391	0.00894	0.001719	0.004352	0.003606	0.00339	0.003717	0.756646	0.243354	1.158997
379	368	0.004258	0.001475	0.036722	0.046626	0.044595	0.000345	0.000299	0.000378	0.000718	0	0.001726	0.005096	0.009874	0.001558	0.003939	0.003426	0.00335	0.004203	0.756028	0.243972	1.214395
381 383	370 373	0.003207	0.001263	0.035683	0.054195	0.047938	0.00029	0.000165	0.000884	0.001728	0	0.001385	0.00534	0.009659	0.001359 0.001528	0.003812	0.003399	0.003064	0.00377	0.752	0.248	1.343456
385	375	0.004684	0.001325	0.0372	0.050965	0.043003	0.000319	0.000327	0.000648	0.001368	0	0.001244	0.005393	0.00873	0.001584	0.004486	0.003806	0.003528	0.004833	0.754874	0.245126	1.15601
387 389	378 380	0.004338	0.001378 0.001144	0.035552 0.037197	0.053121 0.053778	0.042208	0.000601	0.000243	0.000879	0.001591 0.001727	0	0.000867	0.004996	0.008387	0.001329 0.00145	0.004404 0.004792	0.003779	0.003273 0.003246	0.004117 0.004064	0.751355 0.751742	0.248645	1.187209 1.202469
391	383	0.003941	0.00115	0.033725	0.055817	0.045705	0.000446	0.000175	0.00079	0.002338	0	0.001	0.004705	0.008703	0.001049	0.00427	0.003405	0.003472	0.003252	0.749161	0.250839	1.355241
393 395	385 387	0.004407	0.001105	0.034535 0.03768	0.054544 0.050748	0.044305	0.000222	0.000388	0.00089	0.001848 0.001231	0	0.00087	0.003876	0.007827	0.001365	0.004485	0.003589	0.003075	0.003561 0.004405	0.748868	0.251132 0.245695	1.282906 1.143311
397	390	0.003879	0.001236	0.035169	0.052035	0.043791	0.000251	0.000265	0.000781	0.001707	0	0.000998	0.005133	0.008383	0.001694	0.004151	0.004003	0.003393	0.003061	0.75301	0.24699	1.245141
399 401	392 395	0.003742 0.004396	0.001506 0.00162	0.036573 0.033274	0.049102 0.0529	0.041086 0.043732	0.000334 0.000412	0.000148	0.000748 0.001014	0.001502 0.002166	0	0.001185	0.00486 0.004794	0.00798 0.008369	0.001404 0.001424	0.004134 0.004289	0.003154 0.003606	0.003234 0.003584	0.003328	u.756133 0.753069	0.243867 0.246931	1.123378 1.314298
403	397	0.003992	0.001831	0.034445	0.050747	0.042474	0.000332	0.000147	0.000585	0.001426	0	0.001225	0.004527	0.007669	0.001418	0.004446	0.003469	0.003833	0.003318	0.754214	0.245786	1.233094
405 407	400 402	0.004369	0.000789	0.036512	0.050546	0.041895 0.038679	0.000483	0.000273	0.000925	0.001532	0 0	0.001001	0.004952	0.008375	0.001686	0.004171	0.00425	0.003799	0.00384	0.755505 0.751157	0.244495 0.248843	1.14/404 1.135415
409	405	0.00439	0.001393	0.035025	0.055467	0.060397	0.000493	0.000165	0.000752	0.001804	0	0.0008	0.004433	0.0079	0.001159	0.004318	0.003735	0.002871	0.002994	0.751509	0.248491	1.724387
411 413	407 409	0.004644	0.001136	0.034356 0.033577	0.055546 0.056204	0.045023	0.000448	0.000218	0.00089	0.00226	0 0	0.000885	0.004349	0.008176	0.001343	0.00427	0.003741	0.002912	0.003874	0.751327 0.751125	0.248673 0.248875	1.310461 1.238813
415	412	0.004439	0.001087	0.035988	0.052468	0.042779	0.00029	0.000279	0.000632	0.001743	0	0.000889	0.00497	0.008098	0.001473	0.003964	0.003667	0.002966	0.003484	0.753064	0.246936	1.188719
417 419	414 417	0.004487	0.00144	0.037153	0.047246	0.042911	0.000306	0.000185	0.00069	0.001198	0	0.001183	0.004832	0.008138	0.001342	0.00391	0.003691	0.003/12	0.003598	0.756219	0.243781	1.156567
421	419	0.004586	0.001195	0.035633	0.051733	0.045858	0.000413	0.000387	0.000937	0.001715	0	0.001341	0.004999	0.008642	0.001907	0.004615	0.00367	0.002998	0.004304	0.754125	0.245875	1.286926
425	424	0.004575	0.001376	0.036652	0.047471	0.042426	0.000427	0.000372	0.000719	0.001249	0	0.002141	0.004768	0.008351	0.002189	0.00392	0.003446	0.003341	0.00431	0.754874	0.245126	1.157522
427 429	427 429	0.005147	0.001225	0.036341 0.04036	0.051662 0.049842	0.044342 0.048062	0.000302	0.000368 0.000412	0.000775	0.001804	0 0	0.003535 0.003114	0.005002	0.009129 0.00945	0.001598 0.002092	0.004621	0.003769 0.003812	0.003838	0.005798	0.74836	0.25164 0.245431	1.220151 1.190826
											5	*										=

Appendi	ix 1- Bienen	4 - B																	1	1								
Depth	Real dep	th %Clay	%Very F	ine %Fine	Silt %C	Coarse S%V	ery Fine%	6Fine San %	Middle C%Coa	rse S %	Very Coarse	Sand			1				Original					Shifted Gra	ph			
		< 8 才m	8-16 才m	16-32 オ	m 32	2-63 fm 63-1	125 fm 1	25-250 才n 25	0-500 tri 500-1	000 \$ 10	000-2000 Cla	ay Si	ilt :	Sand	>8um	>16um	>32um	>64um	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
26	67 24	41 42	.04 20.	29 20).77	12.9	3.76	0.24	0	0	0	42.04	53.95	4	57.96	37.67	16.9	4	1.606415	3.593333	43.74667	99.83333	2.282079	1.380133	13.46995	126.1366	150.7814	1.195382
26	69 24	44 42	.79 21.	58 22	.12	11.09	2.21	0.1	0	0	0	42.79	54.89	2.32	57.2	35.52	13.4	2.32	1.380133	13.46995	126.1366	150.7814	1.195382	1.479459	6.717172	89.4697	140.7727	1.573412
27	71 24	46 39	.03 20.	77 23	.35	13.27	3.06	0.51	0	0	0	39.03	57.4	3.57	60.96	40.19	16.84	3.57	1.479459	6.717172	89.4697	140.7727	1.573412	1.468896	19.03871	179.1677	194.9935	1.08833
27	73 24	49 48	.54 22.	41 1	8.5	8.61	1.86	0.07	0	0	0	48.54	49.53	1.94	51.45	29.04	10.54	1.94	1.468896	19.03871	179.1677	194.9935	1.08833	1.580784	11.11945	102.4608	123.0853	1.201292
27	75 25	52 48	.36 22.	24 18	.92	8.23	1.84	0.41	0	0	0	48.36	49.38	2.25	51.64	29.4	10.48	2.25	1.580784	11.11945	102.4608	123.0853	1.201292	1.365692	14.38767	137.2159	139.9383	1.019841
2	77 25	55 46	.91 22.	45 1	9.4	8.72	2.06	0.46	0	0	0	46.91	50.57	2.52	53.09	30.64	11.24	2.52	1.365692	14.38767	137.2159	139.9383	1.019841	1.248697	11.06803	109.6735	104.2959	0.950968
27	79 25	57 46	.92 22.	21 1	9.2	8.91	2.52	0.25	0	0	0	46.92	50.32	2.77	53.09	30.88	11.68	2.77	1.248697	11.06803	109.6735	104.2959	0.950968	1.188192	29.37864	307.7184	292.699	0.951191
28	81 26	50 48	.36 23.	16 1	9.1	7.12	1.75	0.51	0	0	0	48.36	49.38	2.26	51.64	28.48	9.38	2.26	1.188192	29.37864	307.7184	292.699	0.951191	1.147691	10.64479	118.6641	113.1429	0.953472
28	83 26	53 50	.79 21.	37 17	.05	7.19	2.57	0.54	0	0	0	50.79	46.1	3.11	49.22	27.35	10.3	3.11	1.147691	10.64479	118.6641	113.1429	0.953472	1.177483	12.5	133.5134	127	0.951215
28	85 26	56 49	.97 20.	18 15	.47	8.36	4.58	1.46	0	0	0	49.97	44	6.03	50.05	29.87	14.4	6.03	1.177483	12.5	133.5134	127	0.951215	1.354623	12.9304	116.7436	123.0623	1.054124
28	87 26	68 55	.57 21.	65 14	.97	6.16	1.56	0.08	0	0	0	55.57	42.78	1.64	44.42	22.77	7.8	1.64	1.354623	12.9304	116.7436	123.0623	1.054124	1.090083	17	159.608	139.3116	0.872835
28	89 27	71 56	.01 21.	91 14	.89	5.04	1.6	0.56	0	0	0	56.01	41.83	2.16	44	22.09	7.2	2.16	1.090083	17	159.608	139.3116	0.872835	1.088847	14.27309	129.8795	117.2369	0.902659
29	91 27	74 5	4.6 22.	15 15	.37	5.06	2.16	0.67	0	0	0	54.6	42.58	2.83	45.41	23.26	7.89	2.83	1.088847	14.27309	129.8795	117.2369	0.902659	1.124359	17.90244	162.6878	146.4244	0.900033
29	93 27	76 47	.47 19.	34 13	.31	6.19	7.68	5.94	0.06	0	0	47.47	38.84	13.69	52.52	33.18	19.87	13.69	1.124359	17.90244	162.6878	146.4244	0.900033	1.126776	12.49495	110.4916	97.70707	0.884294
29	95 27	79 51	.17 22.	31 16	6.97	7.19	1.93	0.43	0	0	0	51.17	46.47	2.36	48.83	26.52	9.55	2.36	1.126776	12.49495	110.4916	97.70707	0.884294	1.157386	16.89352	152.6806	140.3009	0.918918
29	97 28	82 47	.57 22.	17 17	.94	8.23	2.8	1.27	0.03	0	0	47.57	48.33	4.09	52.44	30.27	12.33	4.09	1.157386	16.89352	152.6806	140.3009	0.918918	1.219799	17.71579	162.4421	164.2684	1.011243
29	99 28	85 5	1.2 22.	34 17	.14	7.41	1.77	0.13	0	0	0	51.2	46.89	1.9	48.79	26.45	9.31	1.9	1.219799	17.71579	162.4421	164.2684	1.011243	1.251441	16.92547	158.2112	182.1118	1.151068
30	01 28	87 50	.82 22	.6 17	.29	6.93	2.08	0.29	0	0	0	50.82	46.81	2.37	49.19	26.59	9.3	2.37	1.251441	16.92547	158.2112	182.1118	1.151068	1.252251	18.74675	189.3701	198.7013	1.049275
30	03 29	90 50	.78 22.	49 17	.29	7.38	1.88	0.19	0	0	0	50.78	47.16	2.06	49.23	26.74	9.45	2.06	1.252251	18.74675	189.3701	198.7013	1.049275	1.22522	12.87755	128.9347	125.4776	0.973187
30	05 29	93 52	.81 21.	94 16	6.64	6.79	1.49	0.33	0	0	0	52.81	45.37	1.82	47.19	25.25	8.61	1.82	1.22522	12.87755	128.9347	125.4776	0.973187	1.140241	10.53737	107.605	102.1388	0.949201
30	07 29	95 50	.98 21.	51 17	.16	7.78	2.1	0.47	0	0	0	50.98	46.44	2.57	49.02	27.51	10.35	2.57	1.140241	10.53737	107.605	102.1388	0.949201	1.176808	12.21097	125.135	123.962	0.990626
30	09 29	98 52	.84 21.	78 16	5.31	6.58	2.13	0.36	0	0	0	52.84	44.67	2.49	47.16	25.38	9.07	2.49	1.176808	12.21097	125.135	123.962	0.990626	1.128471	10.66415	117.3585	107.9585	0.919904
33	11 30	01 54	.25 22.	05 15	.78	5.85	1.46	0.61	0	0	0	54.25	43.68	2.07	45.75	23.7	7.92	2.07	1.128471	10.66415	117.3585	107.9585	0.919904	1.072459	16.8303	190.5576	171.6909	0.900992
3:	13 30	04 54	.25 22.	39 15	.72	5.67	1.46	0.5	0	0	0	54.25	43.79	1.96	45.74	23.35	7.63	1.96	1.072459	16.8303	190.5576	171.6909	0.900992	1.114485	19.92857	224.4571	202.9	0.903959
3:	15 30	06 55	.94 24.	02 1	4.7	4.06	0.76	0.51	0	0	0	55.94	42.79	1.26	44.05	20.03	5.33	1.26	1.114485	19.92857	224.4571	202.9	0.903959	1.058657	11.66667	132.193	123.0921	0.931155
3:	17 30	09 5	6.3 21.	18 14	.76	6.12	1.45	0.19	0	0	0	56.3	42.06	1.64	43.7	22.52	7.76	1.64	1.058657	11.66667	132.193	123.0921	0.931155	1.163431	17.48201	189.7194	204.8058	1.079519
3:	19 33	12 55	.69 21.	02 14	.88	6.58	1.69	0.13	0	0	0	55.69	42.48	1.82	44.3	23.28	8.4	1.82	1.163431	17.48201	189.7194	204.8058	1.079519	1.25563	10.96629	127.8371	152.5449	1.193276
32	21 33	15 53	.57 20.	32 15	.91	7.11	2.23	0.36	0	0	0	53.57	43.84	2.59	46.43	25.61	9.7	2.59	1.25563	10.96629	127.8371	152.5449	1.193276	1.196213	11.3271	120.2196	130.1916	1.082948
32	23 33	17 53	.78 21.	04 15	.19	6.87	2.49	0.64	0	0	0	53.78	43.09	3.13	46.23	25.19	10	3.13	1.196213	11.3271	120.2196	130.1916	1.082948	1.183179	22.49057	239.6509	252.0283	1.051647
32	25 32	20 53	.66 21.	09 15	.35	6.97	2.39	0.54	0	0	0	53.66	43.4	2.94	46.34	25.25	9.9	2.94	1.183179	22.49057	239.6509	252.0283	1.051647	1.099335	9.311538	102.3462	95.30385	0.931191
32	27 32	23 55	.95 21.	35 14	.99	5.6	1.63	0.49	0	0	0	55.95	41.94	2.11	44.06	22.71	7.72	2.11	1.099335	9.311538	102.3462	95.30385	0.931191	1.206817	11.28125	128.6406	139.4063	1.083688
32	29 32	25 54	.99 24	.2 13	.05	5.28	2.22	0.25	0	0	0	54.99	42.53	2.47	45	20.8	7.75	2.47	1.206817	11.28125	128.6406	139.4063	1.083688	1.360539	16.15385	201.6077	237.4769	1.177916
33	31 32	28 49	.62 20	.6 16	i.41	9.34	3.61	0.43	0	0	0	49.62	46.34	4.04	50.39	29.79	13.38	4.04	1.360539	16.15385	201.6077	237.4769	1.177916	1.259185	13.1989	141.4586	160.1878	1.132401
33	33 33	31 49	.98 20.	31 16	.29	9.12	3.9	0.4	0	0	0	49.98	45.72	4.3	50.02	29.71	13.42	4.3	1.259185	13.1989	141.4586	160.1878	1.132401	1.472492	13.45652	155.2826	215.6667	1.388866
33	35 33	34 44	.67 19.	05 17	.15	11.72	6.42	1	0	0	0	44.67	47.92	7.41	55.34	36.29	19.14	7.41	1.472492	13.45652	155.2826	215.6667	1.388866	1.403233	11.56627	98.249	117.8434	1.199436
33	37 33	36 43	.38 18.	79 1	8.3	12.88	5.76	0.89	0	0	0	43.38	49.97	6.65	56.62	37.83	19.53	6.65	1.403233	11.56627	98.249	117.8434	1.199436	1.316693	14.31193	114.656	135.3899	1.180836
33	39 33	39 48	.71 20.	22 17	.11	10.03	3.68	0.25	0	0	0	48.71	47.36	3.93	51.29	31.07	13.96	3.93	1.316693	14.31193	114.656	135.3899	1.180836					

							Original					Shifted				
		>8um	>16um	>32um	>64um		Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
Original	Original	0.717176	0.700221	0.5530465	0.110655	>8um	0.717176	-0.22125	-0.26113	-0.00085	0.609866	0.638443	-0.03146	-0.17068	-0.02397	0.415501
Shifted	Shifted	0.638443	0.622511	0.5205392	0.138961	>16um	0.700221	-0.27019	-0.30398	-0.02648	0.626561	0.622511	-0.06013	-0.2152	-0.05768	0.433535
						>32um	0.553047	-0.24633	-0.27488	-0.0258	0.529087	0.520539	-0.08084	-0.24394	-0.09313	0.372565
						>64um	0.110655	-0.03018	-0.07523	-0.00968	0.127846	0.138961	-0.0791	-0.21674	-0.18611	0.043038

|

 | 267 | 241 | < 8 才m
42.04
 | 8-16 łm
20.29 | 16-32 tm
20.77 | 32-63 fm
12.9 | 63-125 łm
3.76
 | 125-250 ‡n
0.24 | 250-500 tn | 500-1000 t
 | 1000-2000
0 | Clay
42.04 | Silt
53.95 | Sand 4 | P95
52.6
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No. 1 No. 2 No.2 No. 2 No. 2		

 | 269
271 | 244
246 | 42.79
 | 21.68 | 22.12 | 11.09
13.27 | 2.21
 | 0.1 | 0 | 0 | 0 | 42.79
 | 54.89
57.4 | 2.32 | 44.2
52.6
 | | | |
 | | |
 | |
|

 | 273 | 249 | 48.54
 | 22.41 | 18.5 | 8.61 | 1.86
 | 0.07 | 0 | 0
 | 0 | 48.54 | 49.53 | 1.94 | 44.2
 | | |
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| 1 1 2

 | 277 | 255 | 46.91
 | 22.45 | 19.4 | 8.72 | 2.06
 | 0.46 | 0 | 0
 | 0 | 46.91 | 50.57 | 2.52 | 44.2
 | | |
 | | | |
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|

 | 279 | 260 | 46.92
48.36
 | 22.21 | 19.2 | 8.91
7.12 | 1.75
 | 0.25 | 0 | 0
 | 0 | 46.92 | 50.32
49.38 | 2.77 | 44.2
37.2
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 | 283
285 | 263
266 | 50.79
49.97
 | 21.87
20.18 | 17.05
15.47 | 7.19
8.36 | 2.57
4.58
 | 0.54
1.46 | 0 | 0
 | 0 | 50.79
49.97 | 46.1
44 | 3.11
6.03 | 44.2
62.5
 | | |
 | | | |
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|

 | 287
289 | 268
271 | 55.57
56.01
 | 21.65
21.91 | 14.97
14.89 | 6.16
5.04 | 1.56
1.6
 | 0.08
0.56 | 0 | 0
 | 0 | 55.57
56.01 | 42.78
41.83 | 1.64
2.16 | 37.2
37.2
 | | |
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 | |
|

 | 291
293 | 274 | 54.6
47 47
 | 22.15 | 15.37 | 5.06 | 2.16
 | 0.67 | 0 | 0
 | 0 | 54.6
47.47 | 42.58 | 2.83 | 37.2
 | | |
 | | | |
 | |
|

 | 295 | 279 | 51.17
 | 22.31 | 16.97 | 7.19 | 1.93
 | 0.43 | 0.00 | 0
 | 0 | 51.17 | 46.47 | 2.36 | 37.2
 | | |
 | | | |
 | |
|

 | 297 | 282 | 47.57
51.2
 | 22.17 | 17.94 | 8.23
7.41 | 2.8
 | 0.13 | 0.03 | 0
 | 0 | 47.57
51.2 | 48.33
46.89 | 4.09 | 52.6
37.2
 | | |
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|

 | 301
303 | 287
290 | 50.82
50.78
 | 22.6
22.49 | 17.29
17.29 | 6.93
7.38 | 2.08
1.88
 | 0.29
0.19 | 0 | 0
 | 0 | 50.82
50.78 | 46.81
47.16 | 2.37
2.06 | 37.2
37.2
 | | |
 | | | |
 | |
|

 | 305
307 | 293
295 | 52.81
50.98
 | 21.94
21.51 | 16.64
17.16 | 6.79
7.78 | 1.49
2.1
 | 0.33
0.47 | 0 | 0
 | 0 | 52.81
50.98 | 45.37
46.44 | 1.82
2.57 | 37.2
44.2
 | | |
 | | | |
 | |
|

 | 309 | 298 | 52.84
 | 21.78 | 16.31 | 6.58 | 2.13
 | 0.36 | 0 | 0
 | 0 | 52.84 | 44.67 | 2.49 | 37.2
 | | |
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 | 313 | 301 | 54.25
 | 22.03 | 15.72 | 5.67 | 1.46
 | 0.5 | 0 | 0
 | 0 | 54.25 | 43.79 | 1.96 | 37.2
 | | |
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 | 315
317 | 306
309 | 55.94
56.3
 | 24.02
21.18 | 14.7
14.76 | 4.06
6.12 | 0.76
1.45
 | 0.51 | 0 | 0
 | 0 | 55.94
56.3 | 42.79
42.06 | 1.26
1.64 | 31.3
37.2
 | | |
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|

 | 319
321 | 312
315 | 55.69
53.57
 | 21.02
20.82 | 14.88
15.91 | 6.58
7.11 | 1.69
2.23
 | 0.13
0.36 | 0 | 0
 | 0 | 55.69
53.57 | 42.48
43.84 | 1.82
2.59 | 37.2
44.2
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 | 323
325 | 317 | 53.78
53.66
 | 21.04 | 15.19
15.35 | 6.87 | 2.49
 | 0.64 | 0 | 0
 | 0 | 53.78
53.66 | 43.09 | 3.13 | 44.2
44.2
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 | 327 | 323 | 55.95
 | 21.35 | 14.99 | 5.6 | 1.63
 | 0.49 | 0 | 0
 | 0 | 55.95 | 41.94 | 2.11 | 37.2
 | | |
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|

 | 329
331 | 325
328 | 54.99
49.62
 | 24.2
20.6 | 13.05
16.41 | 5.28
9.34 | 2.22
3.61
 | 0.25 | 0 | 0
 | 0 | 54.99
49.62 | 42.53
46.34 | 2.47
4.04 | 37.2
52.6
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 | 333
335 | 331
334 | 49.98
44.67
 | 20.31
19.05 | 16.29
17.15 | 9.12
11.72 | 3.9
6.42
 | 0.4
1 | 0
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 | 0
0 | 49.98
44.67 | 45.72
47.92 | 4.3
7.41 | 52.6
74.3
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 | 337
339 | 336
339 | 43.38
48.71
 | 18.79
20.22 | 18.3
17.11 | 12.88
10.03 | 5.76
3.68
 | 0.89
0.25 | 0 | 0
 | 0 | 43.38
48.71 | 49.97
47.36 | 6.65
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52.6
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 | 267 | 241 | AI 0.0005
 | Si
0.001797 | P 0.00016 | S 0.001154 | 0.00016
 | Ar
0.015633 | K 0.023562 | Ca
0.08944 | Sc 0.000173 | Ti
0.021878
 | V 0.000827 | Cr | Mn
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 | 269 | 241 | 0.000325
 | 0.004376 | 6.92E-05 | 0.002549 | 1.24E-05
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| 15 2 0.0007 0.0002 0.0003 0.00033 0.00033

 | 271
273 | 246
249 | 0.000366 0.000259
 | 0.002462 0.00493 | 0.000117
9.86E-05 | 0.001512 0.001201 | 5.37E-05
1.5E-05
 | 0.006947
0.006193 | 0.033467
0.04891 | 0.126356 0.180713
 | 3.89E-05
1.34E-05 | 0.03279
0.046396 | 0.001136 0.001492 | 0.002427
0.002728 | 0.033843 0.060377
 | 1.509011
1.950086 | 0.013521
0.017911 | 0.000879 0.000952
 | 0.000652 0.000421 | 0.011676 0.015002 | 0.002673 0.002322 | 0.003537
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| Dist Dist <thdist< th=""> Dist Dist <th< td=""><td>275</td><td>252</td><td>0.00047</td><td>0.005225</td><td>6.25E-05</td><td>0.001198</td><td>4.81E-05</td><td>0.006279</td><td>0.050677</td><td>0.166662</td><td>0</td><td>0.048147</td><td>0.001639</td><td>0.002803</td><td>0.051715</td><td>1.871563</td><td>0.01585</td><td>0.00093</td><td>0.000678</td><td>0.014735</td><td>0.002301</td><td>0.003342</td><td>0.00529</td></th<></thdist<>

 | 275 | 252 | 0.00047
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 | 0.014735 | 0.002301 | 0.003342
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 | 279 | 255 | 0.000303
 | 0.005031 | 0.000124 | 0.001247 | 2.63E-05
 | 0.006214 | 0.05593 | 0.156249
 | 0 | 0.049790 | 0.001434 | 0.003028 | 0.002447
 | 2.174358 | 0.019770 | 0.000730
 | 0.000490 | 0.014649 | 0.002649 | 0.00448
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283</td> <td>260
263</td> <td>0.000158 0.000393</td> <td>0.004638 0.004179</td> <td>9.2E-05
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1.06E-05</td> <td>0.006043 0.005737</td> <td>0.053252 0.05221</td> <td>0.133563
0.134425</td> <td>9.2E-06
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2.124903</td> <td>0.01869
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0.003071 | 0.041721
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2.124903 | 0.01869
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287 | 266
268 | 0.000358
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 | 0.005448 | 0.053413 | 0.146028 | 2.08E-05
0 | 0.047771
 | 0.001468 | 0.002763 | 0.036893
 | 2.133111 | 0.019714 | 0.000749 | 0.000423
 | 0.013467 | 0.002 | 0.004551
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 | 0.005109 | 2.42E-05 | 0.000976 | 3.02E-05
 | 0.005389 | 0.056636 | 0.183147
 | 0 | 0.047969 | 0.001723 | 0.002947 | 0.046981
 | 2.303221 | 0.020988 | 0.00039
 | 0.000414 | 0.01252 | 0.002179 | 0.003984
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293 | 274 | 0.000375
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4.97E-05 | 0.00109 | 1.05E-05
0
 | 0.005967 | 0.058629
0.059847 | 0.169743
0.159419 | 2.56E-05
0
 | 0.04868 | 0.001636 | 0.002813 | 0.045534
0.046188
 | 2.269989
2.337813 | 0.020374 | 0.000531 | 0.000262
 | 0.011505 0.011845 | 0.002243 | 0.005294 0.005189
 | 0.00502 |
| 929 930 0.00029 0.0012

 | 295
297 | 279
282 | 0.000445
0.000329
 | 0.00556
0.005551 | 0.000114
6.24E-05 | 0.001166
0.001534 | 1.65E-05
2.59E-05
 | 0.00544
0.004944 | 0.058819
0.057952 | 0.178698
0.169818
 | 0 | 0.049166
0.050173 | 0.001626
0.001608 | 0.003269
0.003175 | 0.044989
0.046563
 | 2.265623
2.225074 | 0.0209
0.020476 | 0.000812
0.000939
 | 0.000556
0.000173 | 0.011031
0.011593 | 0.00233
0.002509 | 0.004922
0.003365
 | 0.00534 |
| See 0.0022 0.0027 0.00

 | 299
301 | 285 | 0.00029
 | 0.005143 | 3.82E-05 | 0.0039 | 0
 | 0.005458 | 0.053752 | 0.212509
 | 0
1 82E-05 | 0.047161 | 0.001595 | 0.002993 | 0.04211
 | 2.013878 | 0.017945 | 0.00068
 | 0.000593 | 0.010942 | 0.002457 | 0.005009
 | 0.00495 |
| bit bit< bit< </td <td>303</td> <td>290</td> <td>0.000233</td> <td>0.004365</td> <td>4.69E-05</td> <td>0.006922</td> <td>3.02E-05</td> <td>0.005348</td> <td>0.050416</td> <td>0.265083</td> <td>3.63E-05</td> <td>0.044098</td> <td>0.001615</td> <td>0.002548</td> <td>0.034829</td> <td>1.936139</td> <td>0.018755</td> <td>0.000541</td> <td>0.000497</td> <td>0.010308</td> <td>0.00217</td> <td>0.003777</td> <td>0.00520</td>

 | 303 | 290 | 0.000233
 | 0.004365 | 4.69E-05 | 0.006922 | 3.02E-05
 | 0.005348 | 0.050416 | 0.265083 | 3.63E-05 | 0.044098
 | 0.001615 | 0.002548 | 0.034829
 | 1.936139 | 0.018755 | 0.000541 | 0.000497
 | 0.010308 | 0.00217 | 0.003777
 | 0.00520 |
| 199 200 000000000000000000000000000000000000

 | 305 | 293 | 0.000367
 | 0.004727 | 5.92E-05 | 0.001587 | 2.37E-05
 | 0.003799 | 0.053964 | 0.210017
 | 0.000118 | 0.047324 | 0.001491 | 0.002748 | 0.043428
 | 2.174478 | 0.019143 | 0.000502
 | 0.000751 | 0.010428 | 0.002198 | 0.004066
 | 0.0048 |
| 11 13 140 0.00242 0.00486 7.87-5 0.0017 0.0018 0.0017 0.0018 0.0018 0.0018 0.0018

 | 309
311 | 298
301 | 0.000352 0.000389
 | 0.004298 0.004151 | 4.01E-05
0.000109 | 0.002587
0.00207 | 0
4.99E-05
 | 0.005807
0.004388 | 0.049854 0.052146 | 0.1872
0.18334
 | 3.86E-05
8.81E-06 | 0.044047
0.045687 | 0.001606 0.001755 | 0.002869 0.002909 | 0.045412
0.044973
 | 2.125642
2.205407 | 0.020389
0.019459 | 0.00064
 | 0.000434 0.000219 | 0.010132 0.010191 | 0.003048
0.002198 | 0.004629 0.005086
 | 0.00538 |
| 131 132 133 133 134 <td>313
315</td> <td>304
306</td> <td>0.000242</td> <td>0.004068</td> <td>7.03E-05</td> <td>0.00208</td> <td>7.32E-06</td> <td>0.005278</td> <td>0.052315</td> <td>0.15472</td> <td>0
2.52E-05</td> <td>0.046061</td> <td>0.001749</td> <td>0.00286</td> <td>0.037367</td> <td>2.21915</td> <td>0.019277</td> <td>0.000435</td> <td>7.47E-05</td> <td>0.009776</td> <td>0.002126</td> <td>0.004972</td> <td>0.00555</td>

 | 313
315 | 304
306 | 0.000242
 | 0.004068 | 7.03E-05 | 0.00208 | 7.32E-06
 | 0.005278 | 0.052315 | 0.15472
 | 0
2.52E-05 | 0.046061 | 0.001749 | 0.00286 | 0.037367
 | 2.21915 | 0.019277 | 0.000435
 | 7.47E-05 | 0.009776 | 0.002126 | 0.004972
 | 0.00555 |
| 111 111 100072 000736 0.9936 0.9937 0.09376 0.09386 0.09386 0.09386 0.09386 0.09386 0.09386 0.09386 0.09386 0.09386 0.09386 0.09386 0.00386 0.00386 0.00386 0.00386 0.00138 0.00386 0.00386 0.00138 0.00146 0.00049 0.00038 0.00148 0.0

 | 317 | 309 | 0.000337
 | 0.003934 | 0.000124 | 0.002652 | 7.39E-06
 | 0.005584 | 0.051199 | 0.164868
 | 2.66E-05 | 0.044574 | 0.001908 | 0.002585 | 0.034112
 | 2.124526 | 0.018371 | 0.000476
 | 0.000297 | 0.010762 | 0.002198 | 0.003665
 | 0.00532 |
| 11 0.00036 0.00036 0.00036 0.00037 0.00038 0.0

 | 321 | 312 | 0.000207
 | 0.003827 | 5.96E-05 | 0.005996 | 0
 | 0.00558 | 0.045166 | 0.221452
 | 4.63E-05
3.13E-05 | 0.035667 | 0.001545 | 0.002313 | 0.038802
 | 1.89507 | 0.017839 | 0.000425
 | 0.000355 | 0.009278 | 0.001893 | 0.004213
 | 0.00515 |
| 212 212 0.000936 0.000545 0.7716-0 0.000567 0.000570<

 | 323
325 | 317
320 | 0.00032 0.000161
 | 0.00363 | 0.000103
4.27E-05 | 0.00208 | 4.04E-05
0
 | 0.005816
0.005088 | 0.045233 0.045522 | 0.201255
0.194588
 | 0 | 0.038526
0.038695 | 0.001569
0.001199 | 0.00246 0.00255 | 0.043699
0.038463
 | 1.96054
1.958833 | 0.018963
0.01848 | 0.00035
0.000431
 | 0.000304
0.000174 | 0.00949 0.009156 | 0.002007
0.001552 | 0.004552
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 | 0.00549 |
| 313 312 0.000316 0.00141 7.38-6 0.00054 0.00344 0.00135 0.00154 0.00036 0.00036 0.00034 0.00034 0.00035 0.00036 0.00037 0.00036 0.00036 0.00037 0.00036 0.00037 0.00036 0.00037 0.00036 0.00037 0.00037 0.00036 0.00037 0.00037 0.00036 0.00037 0.00037 0.00037 0.000316 0.00036 0.000

 | 327
329 | 323
325 | 0.000393
 | 0.003658 | 7.71E-05 | 0.001605 | 1.21E-05
0
 | 0.004954 0.005613 | 0.045065 | 0.220653
 | 9.37E-05 | 0.040211 | 0.001476 | 0.00262 | 0.05619
 | 2.075638 | 0.017874 | 0.000488
 | 0.000369 | 0.008967 | 0.002017 | 0.003648
 | 0.00461 |
| 313 0.0000000 0.0004000 0.000540 0.0000540 0.0000540 <td>331</td> <td>328</td> <td>0.000106</td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td>1.7.10 -1.01</td> <td>0.038108</td> <td></td> <td>0.002018</td> <td>0.0085777</td> <td></td> <td>0.019404</td> <td>0.0005</td> <td>9.26E-06</td> <td>0.008355</td> <td>0.002017</td> <td></td> <td>0.00630</td>

 | 331 | 328 | 0.000106
 | | | | -
 | | |
 | 1.7.10 -1.01 | 0.038108 | | 0.002018 | 0.0085777
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 | 0.00630 |
| 337 336 0.000480 0.000481 0.00022 0.000888 0.00135 0.000819 0.00022 0.000881 0.00135 0.00135 0.00136 0.00137 0.00136 0.00137 0.00136 0.00137 0.00135 0

 | | 2.24 | 0.000190
 | 0.003161 | 0 | 0.001141 | 7.53E-06
 | 0.005613 | 0.044452 | 0.203284
 | 0 | 0.038108 | 0.001513 | 0.002818 | 0.039503
 | 1.93254 | 0.019404 0.01759 | 0.0005
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 | 333
335 | 331
334 | 0.000275
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7.28E-05
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 | 0.005613
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2.12E-05
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| 227 241 0.000097 0.03140 0.00518 0.001370 0.749154 0.2558 1.66415 271 246 0.000097 0.03249 0.000150 0.001370 0.001370 0.749154 0.25486 1.80133 271 246 0.000096 0.03472 0.000141 0.000158 0.000127 0.000271 0.000125 0.023237 0.000270 0.000125 0.201352 0.000286 0.002141 0.000286 0.001375 0.749154 0.20228 1.478453 271 250 0.000145 0.000346 0.000246 0.000246 0.000286 0.000142 0.000386 0.000286 0.000287 0.000286 0.000285 0.000286 0.000286 0.000371 0.000286 0.000286 0.000287 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.000286 0.0000286 0.0000286 <td>333
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| 214 0.0095 0.01412 0.004135 0.004135 0.004135 0.004135 0.004135 0.004135 0.004135 0.004135 0.004135 0.004135 0.003145 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00335 0.001415 0.00355 0.00337 0.001415 0.00135 0.00135 0.00135 0.00355 0.00357 0.00135 0.00355 0.00357 0.00135 0.00135 0.00357 0.00135 0.00357 0.00135 0.0

 | 333
335
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339 | 0.000275
0.000215
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Br
 | 0.003161
0.003624
0.002899
0.004646
0.004915
Rb | 0
7.28E-05
9.37E-05
0.00015
5.83E-05
Sr | 0.001141
0.000874
0.001168
0.001652
0.00348
Zr | 7.53E-06
5.46E-05
0.000161
4.19E-05
3.15E-05
Ag
 | 0.005613
0.006131
0.006722
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0.007071 | 0.044452
0.043845
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Sn | 0.203284
0.197542
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0.189466
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Sb
 | 0
2.12E-05
9.37E-06
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Cs | 0.038108
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0.033451
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Ba | 0.001513
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0.001116
0.001203
0.001052 | 0.002018
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 | 1.93254
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0.01759
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0.013714
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0.016861 | 0.0005
0.000572
0.000358
0.000431
0.000819
0.000619
Pb
 | 9.26E-06
0.000509
0.000326
0.000209
0.000252
0.00026 | 0.008355
0.009145
0.009674
0.007231
0.008483
0.009672
Mo inc | 0.002017
0.001936
0.002681
0.00175
0.001786
0.001353
0.003496
Mo coh | 0.003966
0.003043
0.003128
0.003415
0.003964
Zr/Rb
 | 0.00530
0.00506
0.0051
0.00481
0.00436
0.00491 |
| 249 0.000998 0.03479 0.001949 0.001949 0.001940 0.001941 0.001940 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.001941 0.00141 0.00141 0.00141 0.00141 0.00141 0.00141 0.00141 0.00141 0.00141 0.00141 0.00141 0.00141 0.001411 0.001411

 | 333
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Br
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 | 0.003161
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0.004915
Rb
0.03108
0.035494 | 0
7.28E-05
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0.00015
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Sr
0.038912
0.046632 | 0.001141
0.000874
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Zr
0.049928
0.048986 | 7.53E-06
5.46E-05
0.000161
4.19E-05
3.15E-05
Ag
0.00051
0.000476
 | 0.005613
0.006131
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Cd
0.00059
0.000415 | 0.044452
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Sn
0.00023
0.000486 | 0.203284
0.197542
0.164535
0.189466
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Sb
8E-05
0.000442
 | 0
2.12E-05
9.37E-06
0
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Cs
3.33E-05 | 0.038108
0.039447
0.038835
0.033451
0.039462
0.039379
Ba
0.000663
0.001005 | 0.001513
0.001513
0.001473
0.001116
0.001203
0.001052
Ta
0.004791
0.00589 | 0.002018
0.002187
0.002272
0.002075
0.002399
0.002623
W
0.008789
0.010927 | 0.068577
0.039503
0.031644
0.029216
0.045648
0.037698
Ir
0.002357
0.002357
 | 1.93254
1.88618
1.618065
1.876758
1.853006
Au H
0.003007
0.003602 | 0.019404
0.01759
0.016916
0.013714
0.016534
0.016861
tg
0.003044
0.003419 | 0.0005
0.000572
0.000358
0.000431
0.000819
0.000619
Pb
0.005518
0.004357
 | 9.26E-06
0.000509
0.000326
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D1
0.001357
0.002707 | 0.008355
0.009145
0.009674
0.007231
0.008483
0.009672
<u>Mo inc</u>
0.749154
0.750515 | 0.002017
0.001936
0.001936
0.00175
0.001786
0.001353
0.003496
Mo coh
0.250846
0.249485 | 0.003966
0.003043
0.003128
0.003415
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Zr/Rb
1.606415
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 | 0.00630
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| 277 255 0.000736 0.03716 0.04725 0.000287 0.000287 0.000286 0.000296 0.000296 0.000376 0.00137 0.00396 0.001286 0.00138 0.000216 0.001287 0.001518 0.001276 0.001128 0.00128 0.001218 0.001318 0.001218 0.001218 0.001318 0.001218 0.001311

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246 | 0.000275
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Br
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Rb
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0.035494
0.034872 | 0
7.28E-05
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5.83E-05
Sr
0.038912
0.046632
0.044114 | 0.001141
0.000874
0.001168
0.001652
0.00348
Zr
0.049928
0.049928
0.049928 | 7.53E-06
5.46E-05
0.000161
4.19E-05
3.15E-05
Ag
0.00051
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 | 0.005613
0.006131
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0.006338
0.007071
Cd
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Appendix :	L - Bienen 3	в																									
Depth Re	al depth	%Clay	%Very Fine Silt	%Fine Silt	%Coarse S%	6Very Fin€%	%Fine San %I	Middle C%Co	oarse S%Vei	ry Coarse	Sand							Original					Shifted grap	hs			
		< 8 才m	8-16 † m	16-32 † m	32-63 fm 6	3-125 才m 1	I 25-250 才n 25	0-500 才n 500-	1000 11000	-2000 Cla	y Silt	1	Sand	>8um >	16um :	>32um >	>64um	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
167	156	37.07	16.28	17.17	14.35	9.7	4.88	0.56	0	0	37.07	47.79	15.13	62.94	46.66	29.49	15.13	2.267076	1	0.42953	253.0604	589.1563	2.276946	0.919463	0.57047	273.6309	479.6588
169	158	40.71	16.92	16.82	13.68	8.67	3.16	0.05	0	0	40.71	47.42	11.87	59.3	42.38	25.56	11.87	2.276946	0.919463	0.57047	273.6309	479.6588	2.227606	0.658537	0.45935	150.626	327.9115
171	161	45.3	18.89	19.99	12.66	3.06	0.1	0	0	0	45.3	51.54	3.16	54.7	35.81	15.82	3.16	2.227606	0.658537	0.45935	150.626	327.9115	1.608038	5.677524	59.70358	151.5798	2.538873
173	163	44.92	20.45	18.81	9.96	3.5	2.1	0.25	0	0	44.92	49.23	5.85	55.07	34.62	15.81	5.85	1.608038	5.677524	59.70358	151.5798	2.538873	1.454148	15.88398	130.3591	165.1823	1.267133
175	165	41.83	19.88	19.3	11.19	4.31	2.84	0.65	0	0	41.83	50.36	7.8	58.17	38.29	18.99	7.8	1.454148	15.88398	130.3591	165.1823	1.267133	1.318156	16.39931	174.3194	196.7257	1.128536
177	168	48.87	22.76	18.69	7.24	1.77	0.67	0	0	0	48.87	48.69	2.44	51.13	28.37	9.68	2.44	1.318156	16.39931	174.3194	196.7257	1.128536	1.327495	12.91367	136.3621	151.5827	1.111619
179	170	47.6	22.05	19.36	9.24	1.72	0.05	0	0	0	47.6	50.64	1.76	52.42	30.37	11.01	1.76	1.327495	12.91367	136.3621	151.5827	1.111619	1.256725	21.22993	203.8796	215.0146	1.054616
181	172	47.7	22.45	19.44	7.87	1.79	0.75	0	0	0	47.7	49.76	2.54	52.3	29.85	10.41	2.54	1.256725	21.22993	203.8796	215.0146	1.054616	1.175155	17.18266	176.3313	177.5975	1.007181
183	174	47.87	23.4	19.9	7.65	1.15	0.03	0	0	0	47.87	50.95	1.18	52.13	28.73	8.83	1.18	1.175155	17.18266	176.3313	177.5975	1.007181	1.32949	18.24934	165.2175	175.2493	1.060719
185	177	33.47	17.29	21.83	19.09	7.71	0.6	0	0	0	33.47	58.22	8.31	66.52	49.23	27.4	8.31	1.32949	18.24934	165.2175	175.2493	1.060719	1.604662	18.31604	136.4481	171.7783	1.258928
187	179	51.24	23	17.36	7.05	1.32	0.03	0	0	0	51.24	47.4	1.36	48.76	25.76	8.4	1.36	1.604662	18.31604	136.4481	171.7783	1.258928	1.136858	16.83657	177.2548	170.9917	0.964666
189	181	44.69	21.2	19.27	11.62	3.17	0.06	0	0	0	44.69	52.09	3.22	55.32	34.12	14.85	3.22	1.136858	16.83657	177.2548	170.9917	0.964666	1.509341	20.79885	171.7443	208.0115	1.21117
191	184	43.68	19.04	19.55	13.65	3.98	0.1	0	0	0	43.68	52.24	4.08	56.32	37.28	17.73	4.08	1.509341	20.79885	171.7443	208.0115	1.21117	1.223319	16.54865	160.8297	161.4351	1.003764
193	186	47.5	21.62	19.33	9.68	1.84	0.03	0	0	0	47.5	50.63	1.87	52.5	30.88	11.55	1.87	1.223319	16.54865	160.8297	161.4351	1.003764	1.238907	14.20815	133.133	136.4313	1.024774
195	188	46.72	22.45	20.18	8.82	1.52	0.3	0	0	0	46.72	51.46	1.82	53.27	30.82	10.64	1.82	1.238907	14.20815	133.133	136.4313	1.024774	1.365843	19.02865	165.9115	174.1094	1.049411
197	191	46.57	22.52	19.83	8.92	1.84	0.32	0	0	0	46.57	51.27	2.16	53.43	30.91	11.08	2.16	1.365843	19.02865	165.9115	174.1094	1.049411	1.230675	18.07073	156.0659	154.7829	0.99178
199	193	49.22	22.16	18.45	8.79	1.38	0	0	0	0	49.22	49.4	1.39	50.78	28.62	10.17	1.39	1.230675	18.07073	156.0659	154.7829	0.99178	1.300381	16.95269	140.5957	145.886	1.037628
201	195	40.05	20.06	20.38	13.28	5.53	0.69	0	0	0	40.05	53.73	6.22	59.94	39.88	19.5	6.22	1.300381	16.95269	140.5957	145.886	1.037628	1.380082	17.67391	144.4565	153.5024	1.06262
203	198	43.15	21.41	20.62	11.23	3.24	0.35	0	0	0	43.15	53.26	3.59	56.85	35.44	14.82	3.59	1.380082	17.67391	144.4565	153.5024	1.06262	1.329841	14.80754	130.8313	135.248	1.033758
205	200	46.52	21.82	19.43	9.32	2.39	0.52	0	0	0	46.52	50.57	2.91	53.48	31.66	12.23	2.91	1.329841	14.80754	130.8313	135.248	1.033758	1.256648	16.70283	158.5024	161.1533	1.016725
207	202	51.66	23.15	17.19	6.28	1.4	0.31	0	0	0	51.66	46.63	1.71	48.33	25.18	7.99	1.71	1.256648	16.70283	158.5024	161.1533	1.016725	1.144192	17.683	154.9193	168.3314	1.086575
209	204	50.2	23.35	17.52	6.85	1.7	0.38	0	0	0	50.2	47.72	2.08	49.8	26.45	8.93	2.08	1.144192	17.683	154.9193	168.3314	1.086575	1.135542	18.16782	162.8897	147.0828	0.902959
211	207	49.12	22.38	18.67	7.89	1.6	0.34	0	0	0	49.12	48.94	1.94	50.88	28.5	9.83	1.94	1.135542	18.16782	162.8897	147.0828	0.902959	1.181963	17.24885	145.47	141.871	0.975259
213	209	50.67	23.44	18.23	6.17	1.17	0.33	0	0	0	50.67	47.84	1.49	49.34	25.9	7.67	1.49	1.181963	17.24885	145.47	141.871	0.975259	1.171474	15.067	152.6873	144.129	0.943949
215	211	53.28	22.66	16.69	6.29	1.05	0.04	0	0	0	53.28	45.63	1.09	46.73	24.07	7.38	1.09	1.171474	15.067	152.6873	144.129	0.943949	1.129714	14.5232	158.8866	146.3737	0.921246
217	214	51.39	21.98	17.28	7.61	1.68	0.06	0	0	0	51.39	46.87	1.74	48.61	26.63	9.35	1.74	1.129714	14.5232	158.8866	146.3737	0.921246	1.212236	21.36392	192.9684	193.6203	1.003378
219	216	45.31	19.66	17.15	11.11	5.95	0.82	0	0	0	45.31	47.93	6.77	54.69	35.03	17.88	6.77	1.212236	21.36392	192.9684	193.6203	1.003378	1.316982	17.91957	152.9303	167.7828	1.09712
221	218	49.38	23.36	19	7.08	1.13	0.04	0	0	0	49.38	49.44	1.18	50.61	27.25	8.25	1.18	1.316982	17.91957	152.9303	167.7828	1.09712	1.207283	16.87576	178.3788	178.2242	0.999134
223	221	45.09	22.43	20.4	10.04	2	0.04	0	0	0	45.09	52.87	2.04	54.91	32.48	12.08	2.04	1.207283	16.87576	178.3788	178.2242	0.999134	1.295924	20.64983	192.9461	206.0606	1.06797
225	223	52.91	23.19	16.74	6.08	1.04	0.04	0	0	0	52.91	46.01	1.08	47.09	23.9	7.16	1.08	1.295924	20.64983	192.9461	206.0606	1.06797	1.192314	15.79082	144.3316	147.926	1.024904
227	225	56.25	24.11	15.6	4.01	0.03	0	0	0	0	56.25	43.72	0.03	43.75	19.64	4.04	0.03	1.192314	15.79082	144.3316	147.926	1.024904	1.14197	12.29343	127.561	130.0023	1.019138
229	227	52.39	21.61	16.35	7.55	1.84	0.26	0	0	0	52.39	45.51	2.1	47.61	26	9.65	2.1	1.14197	12.29343	127.561	130.0023	1.019138	1.179101	16.85032	162.6561	177.6274	1.092043
231	230	55.06	21.87	15.18	6.11	1.61	0.17	0	0	0	55.06	43.16	1.78	44.94	23.07	7.89	1.78	1.179101	16.85032	162.6561	177.6274	1.092043	1.448841	15.92562	132.7052	170.3526	1.283692
233	232	56.07	21.92	14.94	5.82	1.2	0.05	0	0	0	56.07	42.68	1.24	43.93	22.01	7.07	1.24	1.448841	15.92562	132.7052	170.3526	1.283692	1.188961	16.09059	158.9373	181.1777	1.139932
235	234	55.64	21.55	14.48	5.8	2.17	0.36	0	0	0	55.64	41.83	2.53	44.36	22.81	8.33	2.53	1.188961	16.09059	158.9373	181.1777	1.139932	1.199894	11.17277	116.7173	135.6728	1.162405
237	237	48.28	20.09	15.53	7.79	3.77	3.44	1.1	0	0	48.28	43.41	8.31	51.72	31.63	16.1	8.31	1.199894	11.17277	116.7173	135.6728	1.162405	1.35873	13.15953	145.1518	218.2374	1.503512
239	239	42.04	17.41	14.62	10.17	7.14	6.68	1.94	0	0	42.04	42.2	15.75	57.96	40.55	25.93	15.75	1.35873	13.15953	145.1518	218.2374	1.503512	-				

	Original					Shifted				
	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti	Zr/Rb	Si/Al	Ti/Al	Zr/Al	Zr/Ti
>8um	0.461224	-0.29373	-0.33379	0.361666	0.412453	0.644679	-0.19678	-0.34452	0.337021	0.427794
>16um	0.539429	-0.3863	-0.4211	0.425641	0.49444	0.723982	-0.30849	-0.45094	0.362854	0.504796
>32um	0.578639	-0.46452	-0.48621	0.519166	0.563077	0.805674	-0.44371	-0.57204	0.41232	0.625023
>64um	0.539442	-0.51009	-0.50386	0.575667	0.566567	0.834349	-0.58763	-0.66298	0.484758	0.758034

		>8um	>16um	>32um	>64um
Original	Original	0.46	0.54	0.58	0.54
Shifted	Shifted	0.64	0.72	0.81	0.83
zonder bo	venstuk:	0.631805	0.684728	0.691671	0.559718
/al + shift		0.427794	0.504796	0.625023	0.758034

Appendix 3	1 - Bienen 3	А													1
BienenIII			is naval												
Depth	Real depth	%Clav	%Very Fine	Fine Silt	%Coarse 5	%Verv Fine	%Fine San	%Middle C	%Coarse S	%Verv Coa	rse Sand			1	1
		< 8 m	8-16 fm	16-32 † m	32-63 tm	63-125 tm	125-250 tr	250-500 <i>t</i> n	500-1000 #	1000-2000	Clav	Silt	Sand	Silt +Sand	P95
167	156	37.07	16.28	17.17	14.35	9.7	4.88	0.56	0	0	37.07	47.79	15.13		125
169	158	40.71	16.92	16.82	13.68	8.67	3.16	0.05	0	0	40.71	47.42	11.87		88.4
171	161	45.3	18.89	19.99	12.66	3.06	0.1	0	0	0	45.3	51.54	3.16		52.6
173	163	44.92	20.45	18.81	9.96	3.5	2.1	0.25	0	0	44.92	49.23	5.85		62.5
175	165	41.83	19.88	19.3	11.19	4.31	2.84	0.65	0	0	41.83	50.36	7.8		88.4
177	168	48.87	22.76	18.69	7.24	1.77	0.67	0	0	0	48.87	48.69	2.44		37.2
179	170	47.6	22.05	19.36	9.24	1.72	0.05	0	0	0	47.6	50.64	1.76		44.2
181	172	47.7	22.45	19.44	7.87	1.79	0.75	0	0	0	47.7	49.76	2.54		44.2
183	174	47.87	23.4	19.9	7.65	1.15	0.03	0	0	0	47.87	50.95	1.18		37.2
185	177	33.47	17.29	21.83	19.09	7.71	0.6	0	0	0	33.47	58.22	8.31		74.3
187	179	51.24	23	17.36	7.05	1.32	0.03	0	0	0	51.24	47.4	1.36		37.2
189	181	44.69	21.2	19.27	11.62	3.17	0.06	0	0	0	44.69	52.09	3.22		52.6
191	184	43.68	19.04	19.55	13.65	3.98	0.1	0	0	0	43.68	52.24	4.08		52.6
193	186	47.5	21.62	19.33	9.68	1.84	0.03	0	0	0	47.5	50.63	1.87		44.2
195	188	46.72	22.45	20.18	8.82	1.52	0.3	0	0	0	46.72	51.46	1.82		37.2
197	191	46.57	22.52	19.83	8.92	1.84	0.32	0	0	0	46.57	51.27	2.16		44.2
199	193	49.22	22.16	18.45	8.79	1.38	0	0	0	0	49.22	49.4	1.39		37.2
201	195	40.05	20.06	20.38	13.28	5.53	0.69	0	0	0	40.05	53.73	6.22		62.5
203	198	43.15	21.41	20.62	11.23	3.24	0.35	0	0	0	43.15	53.26	3.59		52.6
205	200	46.52	21.82	19.43	9.32	2.39	0.52	0	0	0	46.52	50.57	2.91		44.2
207	202	51.66	23.15	17.19	6.28	1.4	0.31	0	0	0	51.66	46.63	1.71		37.2
209	204	50.2	23.35	17.52	6.85	1.7	0.38	0	0	0	50.2	47.72	2.08		37.2
211	207	49.12	22.38	18.67	7.89	1.6	0.34	0	0	0	49.12	48.94	1.94		37.2
213	209	50.67	23.44	18.23	6.17	1.17	0.33	0	0	0	50.67	47.84	1.49		37.2
215	211	53.28	22.66	16.69	6.29	1.05	0.04	0	0	0	53.28	45.63	1.09		37.2
217	214	51.39	21.98	17.28	7.61	1.68	0.06	0	0	0	51.39	46.87	1.74		37.2
219	216	45.31	19.66	17.15	11.11	5.95	0.82	0	0	0	45.31	47.93	6.77		62.5
221	218	49.38	23.36	19	7.08	1.13	0.04	0	0	0	49.38	49.44	1.18		37.2
223	221	45.09	22.43	20.4	10.04	2	0.04	0	0	0	45.09	52.87	2.04		44.2
225	223	52.91	23.19	16.74	6.08	1.04	0.04	0	0	0	52.91	46.01	1.08		37.2
227	225	56.25	24.11	15.6	4.01	0.03	0	0	0	0	56.25	43.72	0.03		26.3
229	227	52.39	21.61	16.35	7.55	1.84	0.26	0	0	0	52.39	45.51	2.1		37.2
231	230	55.06	21.87	15.18	6.11	1.61	0.17	0	0	0	55.06	43.16	1.78		37.2
233	232	56.07	21.92	14.94	5.82	1.2	0.05	0	0	0	56.07	42.68	1.24		37.2
235	234	55.64	21.55	14.48	5.8	2.17	0.36	0	0	0	55.64	41.83	2.53		37.2
237	237	48.28	20.09	15.53	7.79	3.77	3.44	1.1	0	0	48.28	43.41	8.31		105
239	239	42.04	17.41	14.62	10.17	7.14	6.68	1.94	0	0	42.04	42.2	15.75	1	177

BienenIII																						
Depth	Real depth	Normalized	l counts																			
		Al	Si	Р	S	CI	Ar	К	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	As	
167	156	0.000225	0.000225	0.00016	0.000484	0.000118	0.014034	0.000198	0.000157	0.000104	9.65E-05	0.000133	0.000534	0.000173	0.021934	0.001674	2.86E-05	7.39E-05	0.002519	0.001046	0.001185	
169	158	0.000207	0.00019	0.000227	0.000611	5.27E-05	0.013006	0.000162	0.000377	4.16E-05	0.000118	8.87E-05	0.000376	0.000227	0.016086	0.001249	0.000202	0.000128	0.00304	0.000835	0.001192	
171	161	0.000343	0.000226	0.000325	0.000597	5.58E-05	0.013317	0.000303	0.000461	5.72E-05	0.000158	7.82E-05	0.000476	0.000247	0.022018	0.000958	0.000193	0.000174	0.001341	0.000705	0.00148	
173	163	0.000306	0.001739	0.000111	0.000802	7.58E-05	0.009104	0.019531	0.095571	4.39E-05	0.018292	0.000706	0.00137	0.014941	0.907153	0.009488	0.001041	0.000485	0.00703	0.001648	0.002859	
1/5	165	0.000297	0.004/14	7.62E-05	0.000956	2.46E-05	0.005979	0.044273	0.155801	3.12E-05	0.038691	0.001225	0.002591	0.032193	1.568047	0.0147	0.001052	0.000588	0.011562	0.002236	0.003843	
1//	168	0.000227	0.003731	6.64E-05	0.001001	1.58E-05	0.005282	0.046066	0.1/5555	0	0.039656	0.001758	0.002526	0.031966	1.81/88	0.016809	0.000964	0.000598	0.012931	0.001935	0.00402	
1/9	170	0.000322	0.004163	0.000129	0.000947	3./1E-05	0.005059	0.048121	0.155807	2.4E-05	0.043963	0.001454	0.002721	0.0282	1.847786	0.015995	0.001358	0.000797	0.014949	0.003073	0.003854	
181	172	0.000213	0.004526	4.82E-05	0.000857	7.78E-00	0.004811	0.049414	0.188828	3.11E-00	0.043467	0.001553	0.002/7/7	0.035969	1.9022	0.017462	0.001152	0.000591	0.012975	0.002268	0.003746	
183	1/4	0.000247	0.004252	0.00014	0.000958	2.22E-05	0.004821	0.050462	0.183089	2.45E-05	0.043636	0.001675	0.002821	0.035648	1.957914	0.017787	0.001397	0.000491	0.013143	0.002146	0.004704	
185	1//	0.000291	0.005308	0.000111	0.001052	7.71E-06	0.004841	0.052301	0.1/0615	1E-05	0.048053	0.00144	0.002977	0.033274	1.922396	0.017797	0.001353	0.000876	0.014089	0.002664	0.00346	
187	1/9	0.000331	0.006064	8.36E-05	0.000959	3.59E-05	0.005361	0.048474	0.163638	1.64E-05	0.045176	0.001431	0.002888	0.061017	1.921397	0.01/351	0.001481	0.000773	0.014159	0.003195	0.003132	
189	181	0.000266	0.004481	7.52E-05	0.000924	5.16E-06	0.005368	0.052386	0.111691	3.1/E-05	0.04/18	0.001916	0.00294	0.047325	2.24/6/8	0.020955	0.001032	0.000615	0.01385	0.002902	0.004576	
191	184	0.000259	0.005384	3.94E-05	0.000913	0	0.005132	0.045966	0.136029	5.21E-06	0.044457	0.001445	0.002861	0.039909	1.830354	0.017685	0.001554	0.000526	0.016692	0.002304	0.003565	
193	186	0.000279	0.004613	6.1E-05	0.000868	1 625 05	0.005071	0.053019	0.176571	1.96E-05	0.044828	0.001836	0.002889	0.059097	2.281/02	0.020994	0.000802	0.000334	0.014795	0.002141	0.004813	
195	101	0.000344	0.004887	0.000132	0.000973	1.62E-05	0.004498	0.053467	0.1/4982	0 055 00	0.045792	0.001780	0.002786	0.042726	2.05/891	0.018474	0.000964	0.000599	0.013921	0.002095	0.004342	
197	191	0.000291	0.005537	0.000108	0.000992	1.59E-05	0.00523	0.05325	0.107231	9.85E-06	0.048277	0.001597	0.002948	0.043161	2.040737	0.018462	0.001193	0.000702	0.013045	0.002775	0.00407	
199	193	0.000302	0.005449	6.1E-05	0.00094	1.62E-05	0.004502	0.054446	0.182151	0	0.047058	0.001414	0.002859	0.046589	2.093762	0.019034	0.001085	0.000479	0.012684	0.001827	0.004335	
201	195	0.000339	0.005742	0.000125	0.0009	9.47E-06	0.004763	0.05372	0.108881	0	0.047624	0.001514	0.002936	0.033927	1.951515	0.0192	0.001364	0.000465	0.014074	0.002472	0.004932	
203	198	0.000309	0.00547	0.73E-05	0.001006	7.48E-00	0.004553	0.050545	0.194367	0	0.044708	0.001532	0.002777	0.049758	2.05/551	0.010442	0.001014	0.000372	0.013337	0.002727	0.003983	
205	200	0.00037	0.00548	0.000152	0.000994	2.285-05	0.004918	0.05094	0.108330	0	0.048422	0.001/0/	0.002961	0.038029	2.084441	0.019442	0.001262	0.000017	0.013255	0.002822	0.004864	
20/	202	0.000302	0.005052	0.000155	0.001001	2.3/E-05	0.004409	0.032158	0.064012	0	0.04/943	0.001513	0.00301/	0.02/808	1 960553	0.017507	0.000902	0.00074	0.014183	0.002507	0.0033333	
209	204	0.000256	0.004525	0.000172	0.000000	2.50E-U5	0.00435	0.04749	0.111104	0	0.053040	0.001012	0.002529	0.001/82	1.000552	0.01/59/	0.000901	0.000406	0.011299	0.002184	0.00483/	
211	207	0.000326	0.005461	0.0001/3	0.000905	1.46E-05	0.004838	0.05059	0.111104	0	0.05303	0.001884	0.003182	0.022928	2.220044	0.020709	0.001009	0.000742	0.012/4	0.002/9/	0.0048/1	
213	209	0.00031/	0.005401	0.000111	0.001062	1.40E-U5	0.004716	0.051511	0.142089	0	0.045057	0.001/19	0.002992	0.033044	2.113249	0.019524	0.001143	0.000511	0.012/00	0.001/08	0.004733	
215	211	0.000298	0.004480	7 255 05	0.000895	1.77E-05	0.004195	0.050743	0.130113	0	0.045403	0.001031	0.002954	0.04310	2.221044	0.020041	0.001020	0.000511	0.013498	0.002313	0.000152	
21/	214	0.000285	0.00414	7.35E-05	0.000991	3.55E-06	0.004563	0.051225	0.123102	1 695 05	0.045294	0.001504	0.002934	0.034400	2.3//880	0.021118	0.00100	0.000328	0.012452	0.0023/5	0.004923	
219	216	0.000241	0.00515	7.48E-05	0.000996	1.08E-05	0.004986	0.053286	0.153862	1.08E-05	0.040510	0.001504	0.002829	0.034499	2.009559	0.019374	0.000833	0.000604	0.013109	0.002839	0.0048/1	
221	218	0.000287	0.003137	7.625-05	0.001035	2.000-05	0.005105	0.051331	0.1/5028	4.01E-00	0.045042	0.001074	0.00204	0.034098	2.029640	0.010770	0.000032	0.000389	0.01303/	0.002248	0.004103	
225	221	0.000237	0.004907	0.000103	0.000854	1.025.05	0.005105	0.050200	0.130957	1.710-05	0.045771	0.001462	0.002813	0.034328	1.079262	0.016943	0.001015	0.0000000	0.013003	0.00210	0.004515	
225	223	0.000237	0.004897	0.000102	0.000957	2.055.05	0.00552	0.052469	0.162272	6 765 05	0.045759	0.001914	0.002593	0.0357	1.9/8302	0.010843	0.001062	0.000363	0.012702	0.002614	0.003051	
227	223	0.000304	0.004193	0.00013	0.000580	0.001242	0.005460	0.051081	0.105275	1 25 05	0.043404	0.001048	0.002088	0.033571	2.023303	0.010202	0.00035	0.000535	0.012542	0.002475	0.004734	
225	227	0.000346	0.004163	0.000105	0.001048	1 95 05	0.005505	0.032201	0.156005	1.20-05	0.045404	0.001425	0.00278	0.020055	1 000000	0.016696	0.000751	0.000340	0.011050	0.002323	0.004291	
231	230	0.000246	0.004152	7 575 05	0.000945	1.8E-05	0.005546	0.04857	0.105448	1.05E-05 3.525.05	0.040077	0.001384	0.00255	0.031903	1.680988	0.015103	0.000862	0.000493	0.011377	0.00231	0.004	
200	232	0.000230	0.004708	0 3EE 0E	0.001019	2 795 05	0.005501	0.043200	0.193737	1 215 05	0.035255	0.001222	0.00237	0.037561	1.091304	0.015152	0.000954	0.000491	0.0110/9	0.001881	0.00393	
200	234	0.000234	0.003773	0.235-05	0.000544	2.700-03	0.000135	0.044735	0.102345	2 25 05	0.037209	0.00137	0.002409	0.044021	1.900113	0.016303	0.000930	0.000052	0.010845	0.001850	0.003709	
237	237	0.000313	0.0035	8.2E-05	0.001014	3.28E-00	0.005781	0.043205	0.151051	3.2E-U5	0.030503	0.001226	0.002534	0.041545	1.8533507	0.010203	0.00059	0.000408	0.009792	0.001815	0.003872	
239	235	0.000210	0.002845	0.000104	0.001025	3.03E=00	0.000037	0.05455	0.103605	1.000-03	0.051564	0.001550	0.002097	0.050766	1.303045	0.015056	0.000585	0.000405	0.008178	0.002	0.00271	
		Se	Br	Rh	Sr	7r	Δσ	Cd	Sn	Sh	C s	Ra	Та	w	Ir	Διι	Hø	Ph	D1	Mo inc	Mo coh	7r/Rh
167	156	0.003269	0.001383	0.025076	0.037866	0.05685	0.000387	0.000467	9.95E-05	9.05E-06	5.28E-05	8.29E-05	0.001716	0.001818	0.001331	0.003798	0.002399	0.005307	0.001372	0.753406	0.246594	2.2670
169	158	0.003379	0.000933	0.024825	0.040478	0.056524	0.000291	0.000563	8.32E-05	3.05E-05	3.33E-05	9.98E-05	0.001492	0.001562	0.001314	0.00333	0.001992	0.005921	0.001192	0.744457	0.255543	2.276
171	161	0.002443	0.000963	0.023219	0.034091	0.051723	0.000515	0.000469	0.000158	3.35E-05	2.65E-05	9.91E-05	0.001473	0.001901	0.001103	0.002494	0.001579	0.003166	0.001139	0.745717	0.254283	2.227
173	163	0.003541	0.001034	0.028881	0.042798	0.046441	0.0003	0.000714	0.000123	0.000225	4.29E-05	0.000753	0.003689	0.006281	0.001752	0.002966	0.002304	0.003744	0.000986	0.749428	0.250572	1.6080
175	165	0.004071	0.000761	0.033715	0.044948	0.049026	0.00033	0.000551	0.000293	0.000453	0	0.002097	0.005342	0.01008	0.002208	0.00359	0.003175	0.004747	0.001981	0.75311	0.24689	1.4541
177	168	0.004162	0.000979	0.033951	0.044993	0.044753	0.000464	0.000299	0.000285	0.000668	0	0.001222	0.005704	0.009304	0.002261	0.003804	0.003081	0.005684	0.003056	0.755494	0.244506	1.318
179	170	0.004252	0.001068	0.036814	0.044272	0.048871	0.000479	0.000322	0.000181	0.000438	3.87E-06	0.001561	0.005492	0.009797	0.001876	0.003911	0.003202	0.006758	0.003004	0.754695	0.245305	1.327
181	172	0.004373	0.000921	0.036476	0.047638	0.045841	0.00058	0.000311	0.000254	0.000534	0	0.00123	0.005963	0.009867	0.002169	0.003981	0.003767	0.004854	0.003244	0.753456	0.246544	1.2567
183	174	0.004686	0.000849	0.037399	0.04763	0.043949	0.000398	0.000391	0.000171	0.000687	0	0.001427	0.006273	0.009555	0.00244	0.003886	0.00352	0.004367	0.003547	0.755687	0.244313	1.175
185	177	0.004887	0.0007	0.038339	0.045263	0.050971	0.00053	0.000487	0.000314	0.000514	0	0.001869	0.005782	0.010325	0.002516	0.004079	0.00393	0.006139	0.002759	0.753164	0.246836	1.32
187	179	0.004576	0.000483	0.035443	0.044215	0.056873	0.000375	0.000536	0.000101	0.000494	0	0.001766	0.005559	0.011158	0.00178	0.004148	0.003562	0.00655	0.003291	0.749728	0.250272	1.604
189	181	0.005242	0.001044	0.040034	0.041051	0.045513	0.000337	0.000607	3.47E-05	0.000267	0	0.001833	0.005805	0.00936	0.00223	0.003976	0.003591	0.005315	0.004049	0.754161	0.245839	1.136
191	184	0.004853	0.000812	0.035674	0.04205	0.053845	0.000266	0.000469	0.000164	0.00038	0	0.00145	0.006395	0.010477	0.002366	0.004675	0.003643	0.00634	0.003396	0.753784	0.246216	1.509
193	186	0.005018	0.000894	0.036783	0.046712	0.044997	0.000268	0.000378	0.00017	0.000445	0	0.001536	0.005988	0.009809	0.002511	0.00449	0.003758	0.005718	0.003792	0.753983	0.246017	1.223
195	188	0.004445	0.001186	0.037877	0.046669	0.046926	0.000727	0.000494	0.000304	0.00041	0	0.001438	0.005644	0.009665	0.002346	0.004614	0.003524	0.005393	0.003123	0.754726	0.245274	1.238
197	191	0.005075	0.000646	0.037092	0.04638	0.050663	0.000438	0.000514	0.000198	0.000477	0	0.001561	0.005967	0.01067	0.002135	0.004456	0.003544	0.004914	0.003737	0.752828	0.247172	1.365
199	193	0.004803	0.000769	0.037923	0.048465	0.046671	0.000541	0.00046	0.000114	0.000491	0	0.001328	0.005907	0.009992	0.002883	0.004326	0.004049	0.004733	0.003414	0.75274	0.24726	1.230
201	195	0.004491	0.000987	0.038001	0.045896	0.049416	0.000439	0.000546	0.000222	0.000556	0	0.001337	0.005974	0.010114	0.002282	0.004285	0.003676	0.004995	0.003483	0.756076	0.243924	1.300
203	198	0.005105	0.000904	0.034424	0.048369	0.047507	0.000523	0.000288	0.000466	0.000618	0	0.001201	0.005764	0.010614	0.002112	0.004201	0.003751	0.005276	0.003473	0.753269	0.246731	1.380
205	200	0.00481	0.001025	0.037641	0.04	0.050056	0.000352	0.000565	0.000137	0.000204	0	0.001599	0.006137	0.009895	0.00205	0.004491	0.003291	0.00528	0.003967	0.757644	0.242356	1.329
207	202	0.004531	0.001109	0.038789	0.040157	0.048745	0.000403	0.000287	7.92E-05	0.000154	n	0.001457	0.006053	0.009764	0.002297	0.004407	0.003523	0.005513	0.003062	0.75675	0.24325	1.256
209	204	0.004617	0.001283	0.037649	0.047605	0.043078	0.000495	0.000475	0.000395	0.000682	0	0.001246	0.005232	0.008885	0.002307	0.00434	0.003377	0.003844	0.003595	0.755139	0.244861	1.144
211	207	0.004919	0.001053	0.042169	0.041553	0.047884	0.000363	0.000463	0.000225	0.000312	0	0.00242	0.006165	0.010043	0.00242	0.004439	0.003579	0.004236	0.003922	0.753022	0.246978	1.135
213	209	0.005529	0.001138	0.038003	0.044749	0.044918	0.000473	0.000425	0.000273	0.000417	0	0.001921	0.006196	0.009734	0.002769	0.004169	0.00378	0.004578	0.00446	0.757492	0.242508	1.181
215	211	0.005272	0.000939	0.036633	0.042393	0.042914	0.000564	0.000348	0.000144	0.000257	0	0.001201	0.006271	0.009422	0.002623	0.004589	0.003912	0.004381	0.004485	0.758183	0.241817	1.171
217	214	0.004983	0.001038	0.036936	0.041929	0.041727	0.000381	0.000307	0.000118	0.000213	0	0.001274	0.006081	0.008992	0.00224	0.004275	0.00342	0.004286	0.004839	0.757642	0.242358	1.129
219	216	0.004612	0.000838	0.038502	0.04487	0.046673	0.000352	0.000394	0.000172	0.000285	0	0.001742	0.005746	0.009514	0.002218	0.004151	0.003923	0.004611	0.003636	0.7558	0.2442	1.212
221	218	0.004616	0.000741	0.036523	0.046306	0,0481	0.000354	0.000461	0.000323	0.000301	0	0.001271	0.00572	0.009941	0.002352	0.004126	0.003515	0.004737	0.00309	0.75436	0.24564	1,316
221	210	0.004589	0.000995	0.03789	0.043429	0.045737	0.000323	0.00044	0.000219	0.000266	0	0.001277	0.005072	0.009824	0.002497	0.004155	0.00344	0.005312	0.003403	0.754501	0.245499	1.207
223	221	0.004629	0.000789	0.03771	0.045659	0.048869	0.000331	0.000501	0.000405	0.000499	0	0.001675	0.005341	0.009921	0.002386	0.004126	0.003792	0.004655	0.003014	0,7508	0,2492	1.20
227	225	0.004301	0.000813	0.037709	0.043921	0.04496	0.000394	0.000414	0.000219	0.000575	0	0.001448	0.005728	0.009274	0.002427	0.004199	0.003046	0.004472	0.003546	0.753493	0.246507	1.193
229	223	0.004578	0.000863	0.038735	0.042229	0.044235	0.000517	0.000347	0.000212	0.000466	0	0.001847	0.005572	0.008878	0.002529	0.00434	0.003639	0.004374	0.00341	0.754025	0.245975	1.14
225	227	0.004481	0.000814	0.037118	0.045191	0.043766	0.000511	0.000541	0.000333	0.000574	0	0.001254	0.005292	0.008639	0.002065	0.003894	0.003364	0.004547	0.003123	0.755996	0.244004	1.179
231	230	0.004329	0.000969	0.034761	0.049894	0.050362	0.000306	0.000541	0.000555	0.000574	0	0.001721	0.005762	0.0000059	0.002003	0.003600	0.003004	0.003991	0.003123	0 750044	0.249956	1 4/9
235	232	0.004328	0.001202	0.035727	0.047754	0.042484	0.000390	0.000302	0.000307	0.000555	0	0.001731	0.005702	0.00501	0.002092	0.003009	0.002105	0.004414	0.00323	0 751 274	0.2493330	1 1 2 0
200	254	0.004519	0.0000954	0.035421	0.043770	0.042501	0.000554	0.000432	0.000416	0.000503	0	0.001275	0.005103	0.008281	0.002081	0.003935	0.003132	0.003803	0.003102	0.754526	0.245464	1,100
	-57	0.0044	0.000000	0.0004720	0.040470	0.042407	0.0000004	0.00000000	2.000.410	0.000023	0		2.000100		0.002200	0.0003754	0.002035		2.005105	2.7 54550	2.243434	1.1.5.5
220	2201	0 002743	11 11 11 10 2 -	11112/17/0	1112 11 10	1112/12/	11100122	111891/10/	0.000100	() ()()() / 2 /	~ ~	0 0001900	0.004.201	0.007701	() () () () () ()	() () () 276-1	111111111111111	0.003000	0.001651	0753905	0 746705	1 300

Appendix 11 XRF settings

XRF settings	Bienen X is missin	g! (no document.txt)										
Base path:	Sample name:	Section name	User ID		Base path: Sample name	e: Section name	User ID		Base path: Sample name	Section name	User ID	
C:\Data\Utrecht\Bie	en Bien I 0-100	Bien 0-100	sif		C:\Data\Utrecht\Bien Bien VI 4.3-5.	30 Bien VI 4.30-5.30	sif		C:\Data\Utrecht\Bien Bien VII 5.3-6.	2 Bien VII 5.30-6.20	sif	
Year	Month	Day	Time		Year Month	Day	Time		Year Month	Day	Time	
201	12	3	6	6	2012	4	3	23	2012	1	24	23
Voltage		60 kV			Voltage	60 kV			Voltage	60 kV		
Current		42 mA			Current	40 mA			Current	40 mA		
Exposure time		200 ms			Exposure time	200 ms			Exposure time	200 ms		
line camera signal le	eve 117	521 at 25 ms			line camera signal leve	110027 at 25 ms			line camera signal leve	105795 at 25 ms		
Step size		500 microns			Step size	1000 microns			Step size	1000 microns		
XRF	ON				XRF ON				XRF ON			
XRF exp. time		30 seconds			XRF exp. time	30 seconds			XRF exp. time	30 seconds		
Start coordinate		3 Stop coordinate		770	Start coordinate	1 Stop coordinate		786	Start coordinate	2 Stop coordinate		765
XRF voltage and cur	rei	30		30	XRF voltage and currei	30		30	XRF voltage and curre	30		30
Tube	Mo				Tube Mo				Tube Mo			
Optical Start		0.5 Optical End		789.5	Optical Start	0.6 Optical End	8	05.6	Optical Start	0.5 Optical End		784.5
Base path:	Sample name:	Section name	User ID		Base path: Sample name	e: Section name	User ID		Base path: Sample name	Section name	User ID	
C:\Data\Utrecht\Bie	en Bien II 0.80-1.55	Bien II 0.80-1.55	sif		C:\Data\Utrecht\Bien Bien IV 2.4-3.	4 Bien IV 2.4-3.4	sif3		C:\Data\Utrecht\Bien\Bien VIII	Bien VIII 6.2-7.2	sif	
Year	Month	Day	Time		Year Month	Day	Time		Year Month	Day	Time	
201	12	1	25	23	2012	4	12	23	2012	1	17	1
Voltage		60 kV			Voltage	60 kV			Voltage	60 kV		
Current		50 mA			Current	41 mA			Current	50 mA		
Exposure time		200 ms			Exposure time	200 ms			Exposure time	200 ms		
line camera signal le	eve 125	256 at 25 ms			line camera signal leve	112126 at 25 ms			line camera signal leve	127963 at 25 ms		
Step size	1	000 microns			Step size	1000 microns			Step size	1000 microns		
XRF	ON				XRF ON				XRF ON			
XRF exp. time		30 seconds			XRF exp. time	30 seconds			XRF exp. time	30 seconds		
Start coordinate		3 Stop coordinate		713	Start coordinate	1 Stop coordinate		777	Start coordinate	5 Stop coordinate		950
XRF voltage and cur	rei	30		30	XRF voltage and curre	30		30	XRF voltage and curre	30		30
Tube	Mo				Tube Mo				Tube Mo			
Optical Start		0.6 Optical End		732.6	Optical Start	0.5 Optical End	7	96.5	Optical Start	0.5 Optical End		966.5
Base path:	Sample name:	Section name	User ID		Base path: Sample name	e: Section name	User ID		Base path: Sample name	Section name	User ID	
C:\Data\Utrecht\Bie	en Bien III 155-240	Bien III 155-240	sif		C:\Data\Utrecht\Bien Bien V3.4-4.3	Bien V 3.4-4.3	sif		C:\Data\Utrecht\Bien Bien IX 7.2-8.2	Bien IX 7.2-8.2	sif	
Year	Month	Day	Time		Year Month	Day	Time		Year Month	Day	Time	
201	12	3	2	5	2012	1	18	16	2012	1	18	0
Voltage		60 kV			Voltage	60 kV			Voltage	60 kV		
Current		50 mA			Current	40 mA			Current	50 mA		
Exposure time		200 ms			Exposure time	200 ms			Exposure time	200 ms		
line camera signal le	eve 136	750 at 25 ms			line camera signal leve	104902 at 25 ms			line camera signal leve	12/789 at 25 ms		
Step size		500 microns			Step size	1000 microns			Step size	1000 microns		
XKF	UN	20			XKF UN	20			XKF UN	20		
XKF exp. time		30 seconds		720	XKF exp. time	30 seconds		751	XKF exp. time	30 seconds		0.40
Start coordinate		4 stop coordinate		/30	Start coordinate	3 Stop coordinate		20	Start coordinate	3 Stop coordinate		940
AKE VOITage and Cur	rei Ma	30		30	AKE voltage and currel	30		30	AKE VOITage and Currel	30		30
TUDE	IVIO	or outsided		740 5	Tube Mo	0.C. Outline I.F. d	_	TO 6	Tube Mo	0.0 0 - 1 - 1		050.5
Optical Start		0.5 Optical End		/49.5	Optical Start	0.6 Optical End	7	/0.6	Optical Start	0.6 Optical End		959.6

Appendix 10 Bienen III - B	lienen X	ALStandardized (normalized alemental count/ Al count)	Bienen III - Bienen X Denth Real Denth	ALStandardized (normalized elemental count) Al count)
167	156 Earl Depth	Ar-standarduze (internative central county of county) Si K Ca Ti Mn Fe Rb Sr Zr Pb 1 0.879195 0.697987 0.42953 0.771812 97.63758 111.6242 168.557 253.0604 23.62416	545 531	Si K Ca Ti Mn Fe Rb Sr Zr Pb 22.01515 168.7828 467.3687 146.3232 114.8232 5792.646 140.9192 166.5303 208.0859 15.61111
169 171	158 161	0.919463 0.785235 1.825503 0.57047 1.100671 77.87248 120.1745 195.953 273.6309 28.66443 0.658537 0.882114 1.341463 0.45935 0.719512 64.12195 67.61789 99.28049 150.626 9.219512	547 533 549 536	24 202.0539 549.0101 169.9226 165.3805 7022.327 126.7003 147.5589 150.6465 12.73064 15.53314 144.0778 465.0058 118.268 162.9395 5609.069 100.2939 122.0346 115.7205 7.925072
173 175	163 165	5.677524 63.74593 311.9349 59.70358 48.76547 2960.85 94.26384 139.6873 151.5798 12.2215 15.88398 149.1685 524.9337 130.3591 108.4669 5283.163 113.5939 151.442 165.1823 15.99448	551 538 553 541	18.71071 166.7464 575.2357 143.6071 201.9643 6936.25 115.9214 149.275 138.55 10.35 11.69583 101.9479 300.1188 86.49375 111.3417 3905.917 68.55208 82.28333 79.46667 6.09375
177	168 170	16.39931 202.4965 771.7014 174.3194 140.5174 7991.01 149.2431 197.7813 196.7257 24.98611 12.91367 149.259 483.271 136.3621 87.46763 5731.319 114.1871 137.3189 151.5827 20.96163	555 543 557 545	14.82308 134.7692 418.5538 114.4077 164.3821 5352.618 87.47179 101.5795 90.69487 7.489744 18.95156 174.7059 641.519 146.7024 166.3806 6646.014 114.0346 145.1765 126.6574 9.020761
181	172	21.22993 231.774 865.0934 203.8796 159.321 8922.241 171.0912 223.4735 215.0146 22.76842 17.18266 203.9133 739.8545 176.3313 144.0526 7911.839 151.1269 192.4706 177.5975 17.54706 19.2014 179.323 565.6104 155.1154 144.023 565.025 121.947 155.5232 115 2002 11.051	559 548 561 550	23.08044 215.2839 //5.2009 17/.0350 204.001/ 8312.805 137.8008 17.53424 152.0109 11.4001 14.5288 132.4738 463.212 109.4476 107.678 4986.445 85.81414 110.4398 95.14398 74.45026 15.2706 14.6703 5.84.312 132.032 151.672 5.765131 01.08565 118.2005 17.05672 0.420401
185	177	18/24934 1/9/8/2/3 366.5101 165/1/5 114/4032 6609.592 131.817 155.623 1/5/2493 2/1.1051 18/31604 146/408 494/2476 136/4481 184/2925 5803.316 107.0495 133.5448 171.7783 19/78302 16/9767 106/971 416/106/07 173/548 172/9806 8/4/4 65 160/071 166/271 167/271	563 552 565 555	16.27005 146.9973 348.123 122.393 151.607 5760.521 91.08556 118.2995 102.607 94.40481 18.58571 183.6286 585.9 157.5071 172.9464 7288.511 119.1179 148.4857 133.6107 11.55714 14.1906 115 2010 276 2744 100 5006 40.2420 467467 81.142, 02.02610 0.0510 7.05100
105	184	20.79885 177.5747 525.5029 177.1743 154.1753 7070.974 137.8161 162.4483 208.0115 24.49425 16.54865 190.162 633.2484 160.8297 212.0216 8186.011 31 4649 167.5892 161.4351 20.51351	569 560 571 562	21.85401 177.7153 734.865 157.8212 128.5985 6156.704 112.7299 167.9891 161.1496 10.10584 19.1761 156 5723 678.0189 136.7582 161.1925 5545 519 97 36478 142 5566 158.306
195 197	188 191	14.20815 155.4485 508.7339 133.133 124.2189 5983.013 110.1223 135.6845 136.4313 15.68026 19.02865 183 574.7135 165.9115 148.3281 7013.299 127.474 159.3932 174.1094 16.88802	573 564 575 567	19.49072 123.5172 647.374 111.5358 103.6737 3967.098 75.16446 133.1936 125.8249 4.328912 17.0989 141.3984 447.5055 131.3929 126.5137 4872.962 89.16484 111.1291 130.2115 8.222527
199 201	193 195	18.07073 180.5683 604.1 156.0559 154.5098 6943.9 125.7707 160.7341 154.7829 15.69756 16.95269 158.5914 498.5699 140.5957 100.1591 5761.267 112.1871 135.4946 145.886 14.74624	577 569 579 571	15.32827 143.4316 699.4681 121.5532 306.1033 6323.909 88.83283 130.4529 109.845 8.094225 16.70755 159.9811 488.6132 136.4528 267.761 6501.695 106.1572 123.2579 117.327 8.984277
203 205	198 200	17.67391 163.3164 628.0242 144.4565 160.7754 6648.196 111.2271 156.2874 153.5024 17.04589 14.80754 137.6349 292.7143 130.8313 102.75 5631.974 101.7024 108.0774 135.248 14.26587	581 574 583 576	23.06608 227.2467 727.3568 187.978 383.9295 9587.335 143.5727 174.8722 148.3789 13.65198 17.7623 144.6284 467.3825 123.6585 162.6721 5472.036 92.10656 113.7049 103.4645 9.379781
207 209	202 204	16.70283 172.4387 277.75 158.5024 92.13443 6845.208 128.2406 132.7618 161.1533 18.22642 17.683 185.5706 727.2017 154.9193 124.1902 7270.291 147.1182 186.0202 168.3314 15.02017	585 579 587 581	18.73375 164.6254 437.0805 141.2724 140.9009 6342.146 106.5913 121.5697 119.5882 8.377709 14.12366 138.5833 415.4704 119.4812 140.4247 5580.788 91.64516 111.078 99.10215 7.303763
211 213 215	209	18.10782 180.1793 341.209 102.8897 /0.4279 0615.147 127.526 127.534 147.545 149.1828 13.01149 17.24885 162.6935 450.6751 145.47 104.3664 6674.585 120.03 141.3364 141.871 14.45853 15.067 170.4718 426.0875 152.6873 414.0553 246.1465 123.0233 142.3270 144.120 147.146.	589 583 591 586 592 588	17.78931 106.737 440.7358 143.5885 103.4119 0512.374 108.2707 121.3396 110.257 8.141309 19.12541 174.0099 318.5083 159.8911 157.9406 6868.822 118.1122 121.7162 133.3366 11.20792 15.44 134 655 2575 117.96 0465 0565 23 89.375 09.455 07.615 7.6325
213 217 219	211 214 216	15.007 170.4216 490.5570 155.0875 144.5535 140.553 142.553 142.557 144.125 146.1373 144.125 146.1373 15.0351 145.352 146.3737 15.0351 145.352 146.3737 15.0351 145.352 146.3737 15.0351 145.352 146.3737 15.0351 145.352 146.3737 15.0351 145.352 146.3737 15.0351 145.352 146.3573 155.3551 145.352 145.352 145.355 145.352 145.3555 145.355 145.355 145 145.355 145.355 145.355 145.355 145.355 145.	595 590 597 593	13.44 135.025 357.39 117.80 56005 3053.53 665275 55.435 57.3025 76025 12.58391 117.7057 314.5264 100.6552 128.3379 4819.763 77.15862 87.11494 84.49195 5.714943 15.64266 145.6845 437.241 118.9972 104.984 557.0357 92.8892 111.2161 107.784 7.778393
221 223	218 221	17.91957 181.1475 624.4933 152.9303 118.9437 6885.74 127.3995 161.5255 167.7828 16.52279 16.87576 195.897 611.6121 178.3788 133.7818 7944.994 147.6242 169.2515 178.2242 20.70606	599 595 601 598	16.33125 153.5594 607.8875 126.6188 209.2688 6519.006 100.2656 136.0688 113.5625 7.7625 14.79634 138.0183 540.7415 110.5849 193.154 5827.974 88.08616 119.953 93.56136 9.469974
225 227	223 225	20.64983 221.2424 720.4613 192.9461 150.532 8341.973 159.0067 192.5253 206.0606 19.62626 15.79082 170.0383 537.1888 144.3316 118.3495 6657.204 124.0663 144.5051 147.926 14.71429	603 600 605 602	17.36607 151.8125 483.5863 127.6101 157.878 5600.378 98.0744 123.375 114.7619 8.285714 17.14245 150.4872 458.1567 128.6154 120.7236 5604.946 97.92023 114.7578 107.7863 8.641026
229 231	227 230	12.29343 153.4155 407.3498 127.561 82.40376 6002.387 113.8404 124.108 130.0023 12.70657 16.85032 197.1242 671.4777 162.6561 129.7229 7634.086 150.6465 183.4108 177.6274 18.45541	607 605 609 607	15.81313 138.1995 427.4571 116.404 89.93687 4808.604 87.83333 105.0707 96.67929 8.454545 23.63504 196.5876 644.9891 166.4781 219.8613 7516.219 122.2956 152.3139 141.1131 12.14234
233 235	232 234	15.92562 153.1129 662.1543 132.7052 128.4711 5721.763 117.5785 168.7328 170.3526 13.49862 16.09059 190.878 778.4948 158.9373 190.2892 8128.774 152.3833 203.6585 181.1777 18.83275 11.17377 128.1175 494.1474 115.1137 13.15248 150.688 113.0771 120.7570 156.7518 13.1777	611 609 613 612 615 614	14.41667 128.5116 392.9653 104.3148 113.588 4623.877 82.28009 95.57176 82.57639 5.37963 14.52788 131.7981 415.2433 108.4599 126.7494 4903.657 83.3528 101.3187 86.67883 8.270073 15.89708 126.0005 460.2695 112.4691 124.559 5.16523 80.00058 100.5167 2127202
239	239	13.15953 159.7938 489.3385 145.1518 142.393 7333.588 160.6187 195.0739 218.2374 18.07782 359333 47 1133 178 84 43 24667 44 0.0667 195.21 67 14667 77 80667 99 8333 110.333	613 614 617 617 619 619	13.86236 130.8003 400.2006 117.4061 124.335 3510.372 85.0076 105.033 55.1310 727350 16.4322 147.7034 465.1808 125.435 155.1243 5648.082 95.86723 115.2034 102.6215 8.293785 13.90431 12555 370.6531 106.3268 120.6675 4826.103 82 5573 92.8723 184.0191 5.868421
269 271	244 246	13.46995 140.776 582.4044 126.1366 102.0546 5303.661 109.2514 143.5355 150.7814 13.40984 6.717172 91.31818 344.7727 89.4697 92.34343 4117.449 95.15152 120.3687 140.7727 12.89394	631 621 633 623	9.512097 91.875 301.4597 79.37903 82.49194 3535.206 82.08468 103.4234 117.6129 9.326613 12.45552 119.6868 429.1032 99.91103 93.72242 4603.007 94.11744 122.0605 115.0819 10.04982
273 275	249 252	19.03871 188.8774 697.8645 179.1677 233.1613 7530.716 132.7484 185.2839 194.9935 27.81935 11.11945 107.8464 354.6724 102.4608 110.0546 3982.87 77.86348 98.91126 123.0853 13.93857	635 625 637 628	15.69841 151.2143 563.3056 126.496 129.4008 6015.032 115.5833 146.7897 132.0159 12.67063 16.96241 166.7744 797.1654 142.609 164.1278 7147.737 204.2782 264.6466 260.5489 24.2782
277 279	255 257	14.38767 153.5903 488.1145 137.2159 172.0749 6195.233 102.467 130.207 139.9383 15.837 11.06803 123.0408 343.7313 109.6735 109.3741 4783.35 83.52381 99.37755 104.2959 11.2449	639 630 641 632	14.5614 133.2939 605.8596 114.7149 115.25 5349.25 133.6053 175.4254 158.3991 12.4693 23.67708 229.8802 775.3333 194.6927 197.9063 8808.354 180.75 221.6042 200.1302 23.42708
281 283	260 263	29.37864 337.2816 845.9515 307.7184 264.2524 13285.5 246.3398 278 292.699 31.96117 10.64479 132.9923 342.4131 118.6641 96.73359 5412.66 98.58301 113.0193 113.1429 13.28185	643 634 645 637	16.14618 165.8073 559.9369 145.1761 179.3355 6756 117.4618 137.0266 124.3123 11.97342 11.41304 203.4826 625.3087 191.1565 201.2565 9216.778 162.113 186.1348 170.0652 13.71304
285	266 268	12.5 149.2813 408.1295 133.5134 103.1116 5961.768 107.8571 128.5938 127 16.41071 12.9304 132.2271 395.0293 116.7436 95.17582 4931.344 90.84615 118.8498 123.0623 12.48718	647 639 649 641	23.03252 399.4553 1088.48 376.1789 373.5203 17342.7 301.9268 342.4797 323.4634 26 31.38947 501.0421 1418.4 473.3368 667.5256 23575.22 366.3895 421.0947 434.8421 33.37895
289 291	271 274 276	17 188.4472 609.392 159.608 156.3216 7663.593 127.799 161.0503 139.3116 16.73367 14.27309 156.4217 452.8755 129.8795 121.4859 6056.357 107.6707 124.3213 117.2369 10.16466 17.00244 146 516.7302 142.6928 140.232 147.232 140.234 146.444 11.9278	651 643 653 645	14.59447 219.0922 608.1521 210.9631 143.0922 9405.788 166.0507 186.4885 201.106 14.85714 36.32632 513.7579 1546.232 500.1158 355.6737 21065.12 377.2842 451.0526 463.3579 35.35789 17.78660 2651 1382.652 123.256.061 238273 21065.12 377.2842 451.0526 463.3579 35.35789
293 295 297	279	1/30244 194 510.707 105.0878 149.722 7576.22 130.223 148.0244 140.4244 11.0878 12.49495 132.1852 401.5926 110.4916 101.1044 5091.603 86.7138 104.0707 97.70707 7.430976 16.89352 176.3519 516.7371 152.8086 141.6046 6771 106 131 13272 145.5206 140.2006 14.4814.8	657 650 659 652	17.26059 203.501 1363.543 205.3001 238.872 11840.8 207.5244 204.0854 233.001 17.34140 12.25888 175.8883 2005.487 172.2132 210.9543 8827.792 168.4315 219.9594 226.9594 15.38071 20.2517 416.8572 1514 348 306.713 447.5372 1886.933 305.313 380.313 372 33.44348
299 301	285	17.71579 185.1421 731.9632 162.4421 145.0421 6936.568 134.668 164.3 164.2684 11.08947 16.92547 180.9441 1440.317 158.2112 135.0745 7286.224 145.5217 198.7888 182.1118 9.865565	661 654 663 657	21.20732 289.8354 1037.774 277.6768 392.9756 14370.87 200.1037 265.7622 255.5061 23.14024 12.24908 186.2967 673.1245 176.3736 251.381 8109.795 124.967 162.9487 143.8791 11.87546
303 305	290 293	18,74675 216.5 1138.344 189.3701 149.5649 8314.357 158.6753 205.7338 198.7013 16.82468 12.87755 147.0245 480.8857 128.9347 118.3184 5924.335 102.4122 128.5878 125.4776 10.21224	665 659 667 661	32.18421 432.9737 1646.991 394.0439 382.886 16404.41 306.2632 421.807 381.7281 23.61404 27.98693 296.9281 1443.026 249.3791 291.3007 10020.86 197.1699 343.7516 306.6732 21.03268
307 309	295 298	10.53737 122.7402 505.0356 107.605 106.306 5041.363 89.57651 112.0142 102.1388 10.0427 12.21097 141.6329 531.8228 125.135 129.0127 6038.814 105.3376 133.6456 123.962 10.27004	669 663 671 666	15.14559 183.7241 736.6935 159.9464 161.5057 6977.387 129.4751 189.5517 188.0268 11.50575 16.34146 249.8439 884.561 225.6293 384.078 10733.86 174.7756 226.8 189.1951 17.18049
311 313	301 304	10.66415 133.9509 470.9547 117.3585 115.5245 5665.132 95.66792 120.4377 107.9585 9.188679 16.8303 216.4303 640.0848 190.5576 154.5879 9180.758 160.0909 184.6545 171.6909 13.64848	673 668 675 670	24.58519 382.3185 1005.933 365.0222 482.3852 15972.79 278.2815 317.4222 283.5259 27.13333 18.04734 268.6982 852.8935 260.0237 403.9645 12367.65 196.1716 238.0296 213.0237 15.54438
315	306 309	19.92857 254.0929 766.1286 224.4571 163.4786 10275.53 182.0571 216.6214 202.9 20.62143 11.66667 151.8421 488.9518 132.193 101.1667 6300.728 116.2719 130.6053 123.0921 11.83772	677 672 679 674	19.75595 286.8929 844.4464 291.5 359.6488 12756.96 207.9821 247.2202 251.0595 22.22024 18.185 245.875 719.74 232.315 175.89 9549.585 176.99 206.325 226.53 20.59
319 321 323	312 315 317	17,48201 217,705 1007,417 189,7194 187,0268 947,6391 776,036 228,6115 204,8058 13,2677 10,96629 149,0056 818,8146 127,8371 129,4551 6792,303 121,4888 166,8652 152,5449 9,516854 11,3721 141,1495 628,0187 120,2166 136,3645 6112 874 108,8364 151 1495 130,1916 8,588131	683 679 685 681	14:39434 210.0183 031.70/1 20/32/24 108:55/1 8/30.350 130.8126 104.8707 135.5708 10.52055 20.24571 295.1771 757.4571 284.1029 178.6 11476.58 211.3486 244.4629 266.7029 24.17714 33.05661 507 1616 1127 364 496.7778 308.3535 19136 03 370 3434 405.0203 484.101 35.86869
325	320	22.49057 281.934 1205.16 239.6509 238.217 12131.81 213.0094 297.1509 252.0283 16.45283 9.311538 114.7 561.6077 102.3462 143.0154 5282.931 86.69231 125.0885 95.30385 9.923077	687 683 689 686	21.80952 301.449 1123.714 302.2517 351.483 12963.42 228.7075 320.8776 318.2857 27.66667 23.79141 276.4969 1130.411 243.6012 318.9264 11027.49 195.3742 309.8834 273.5951 16.96933
329 331	325 328	11.28125 145.9427 657.5365 128.6406 231.4948 7912.406 115.5156 167.1719 139.4063 13.42188 16.15385 227.1846 1038.946 201.6077 201.8923 9876.823 174.5462 260.9 237.4769 15.8	691 688 693 690	13.15929 226.6991 387.7389 206.6991 219.7788 10117.91 171.854 178.9115 172.3097 15.88938 16.28729 260.8895 515.6796 260.3481 336.9392 13418.3 196.6851 224.6243 229.2044 19.04972
333 335	331 334	13.1989 159.7072 719.558 141.4586 115.2652 6870.53 127.2155 185.2044 160.1878 13.85083 13.45652 162.9638 763.7826 155.2826 135.6232 7511.174 146.4638 228.971 215.6667 16.24638	695 692 697 695	18.34177 298.6266 710.9494 282.8165 358.1392 13995.77 229.4114 257.981 241.8165 22.74051 13.82791 220.6605 503.4419 219.814 225.4698 10163.64 175.6651 195.6977 190.214 14.90698
337 339	336 339	11.56627 108.8193 471.7189 98.249 113.6506 4672.622 83.97992 131.8916 117.8434 8.160643 14.31193 131.2248 668.4771 114.656 109.7615 5395.239 102.8257 155.2294 135.3899 11.04587	699 697 701 699	22.62791 376.8527 944.4341 362.5969 368.4031 17082.62 279.4031 322.9612 305.0698 26.31008 28.10476 437.2381 974.7429 444.781 323.3143 18555.81 347.2095 367.8667 405.6571 34.5619
357	341 343	2/59862 253.1103 1136.841 20/.11/2 216 9996.648 1/5.93/9 243.8966 212.82/6 15.931 20.42387 180.7654 671.9259 152.6749 126.749 6953.424 118.0453 160.1399 142.5391 10.32922 4.40455 126.225 491 702 116.7259 40.7255 40.7255 100 5 66.2551 100 5019 100 7.732505	703 701 705 703 707 705	13.84689 231.5837 545,0048 221.3349 203.1914 10233.33 181./556 196.9925 193.300 16.40191 17.23429 277.8343 810.04 264.04 268.7771 12152.17 214.6571 247.1486 234.7086 21.77714 215.212 2514 2514 1038 1136 402 230 8003 232.7574 151543 237 030 242.326 232.114 5 55561
363 365	348 351	14-3945 120.3525 461.7030 105.3766 64.0253 4635.453 605.3639 1005.3763 105.1005 7.035363 15.1493 134.7127 515.5859 113.5014 95.06479 5317.394 88.53239 114.1296 102.6704 8.839437 20.0172 186.4922 656.5625 161.8125 141.3711 7567.852 128.1133 173.8984 145.5117 13.18359	709 708 711 710	17.78873 349.9155 841.4014 334.4014 336.1831 15804.35 273.1268 305.8662 286.8521 26.8662 32.80769 657.3718 1538.41 622.8205 647.8846 2970.38 505.8205 545.8718 492.7051 44.46154
367 369	353 356	14.92073 146.8963 367.1555 130.3994 116.8659 6258.387 101.9756 126.3293 111.0793 9.615854 21.02917 205.1792 683.2875 178.6792 168.0708 8365.538 140.575 174.2625 156.8583 9.545833	713 712 715 715	26.90476 507.381 1386.638 468.2286 526.2762 22101.82 370.181 389.6286 358.5333 36.44762 31.65934 470.2088 1496.253 439.5165 652.7143 20932.64 332.7033 386.5824 379.5934 41.53846
371 373	358 361	23.31933 217.3109 897.0294 184.5882 190.9076 8163.5 141.3487 198.6639 174.979 13.12185 21.97308 186.2423 793.8269 153.6192 148.7731 6679.831 122.2154 173.5577 154.5115 9.65	717 717 719 719	10.92105 111.4934 298.6053 98.46053 107.9342 4673.24 99.67434 115.8454 115.2401 7.555921 14.1769 108.2432 330.5946 92.42506 96.76904 3930.609 77.2457 94.9484 90.61179 7.027027
375 377	363 365	15.23324 147.0816 487.9883 126.1749 117.3003 5462.72 95.22157 131.102 110.3615 8.728863 18.79355 158.2258 355.7161 138.4806 166.671 6595.523 103.5935 131.5677 124.971 9.706452	737 721 739 723	20.48503 176.3353 709.7006 156.479 143.4192 6511.257 145.6647 190.8443 185.2515 16.62275 13.82236 108.1557 405.0359 88.51896 132.1976 4068.633 69.03792 86.78643 75.27545 6.323353
379	368	20.88641 1/5.4948 494.4415 154.5226 119.4634 8852.425 114.007 144.726 138.4495 10.4007 18.48366 155.1863 659.2222 132.9673 105.5033 5628.641 100.8301 153.1455 135.4608 8.656863	741 726 743 728	37./11/6 264.2529 1238.335 21/3941 239.6118 9/36.459 1/3.9235 225.5353 18/3647 22.264/1 15.91922 139.2689 589.9805 11/3376 137.4178 5044.148 95.85237 120.0167 101.1448 12.36769
383 385 387	375	17.58286 134.5229 033.0314 110.2080 100.10 5150.271 91.02 142.971 120.5257 7.34 18.58966 167.7862 610.5414 146.9793 139.8793 6665.176 113.3655 155.3138 131.0517 10.75172 19.70782 18.6596 878.5751 159.5638 724.7366 80.7264 216.177 188.5309 149.7984 116.1728	745 731 747 733 749 735	18.00526 147.3493 407.3254 122.5858 128.3156 5201.352 92.07695 111.1952 97.311 10.07/03 14.712 124.606 300.476 108.188 118.462 4545.682 81.784 92.202 86.568 11.208 17.2088 154.6543 338.3605 139.758 183.0864 6315.855 101.5642 111.9032 95.46667 12.19012
389 391	380 383	16.14763 127.9944 573.9499 106.532 133.3677 4702.256 89.56267 129.4875 107.6964 7.816156 17.94576 144.3186 713.1763 119.7492 183.1831 5456.2 94.07797 155.7051 127.4983 9.684746	751 738 753 740	14.2354 115.9872 343.9051 103.8248 103.7609 4132.693 76.51825 88.93796 73.55657 7.793796 14.5823 120.8539 369.2181 104.3539 96.57613 4446.669 81.49177 96.31687 79.04527 8.102881
393 395	385 387	19.02024 160.3927 785.2834 131.8826 150.8583 6008.874 116.1457 183.4413 149.004 10.34008 24.94975 251.9196 918.6332 214.8191 222.4171 9772.638 170.6935 229.8894 195.1558 16.74874	755 743 757 745	18.59211 164.9711 475.3132 141.9316 177.0053 6565.674 107.9026 122.9342 104.0237 10.97368 16.8186 144.4419 412.7326 129.1651 168.5442 5746.528 94.95116 108.0977 90.85349 9.583721
397 399	390 392	19.8412 195.3777 883.7039 162.6438 205.2747 7489.687 131.6052 194.7167 163.867 12.69528 22 221.7857 934.0333 180.0571 169.3619 8756.957 155.581 208.8762 174.7762 13.75714	759 747 761 750	14.36257 122.8187 299.9064 114.2144 126.4932 4467.092 81.23392 87.77973 83.02729 8.05653 17.95735 154.6422 369.0664 139.9882 112.0592 5499.787 100.1422 107.6611 104.7488 10.95735
401 403	395 397	16.11355 151.8388 855.1429 133.8352 151.1136 6354.007 107.1868 170.4103 140.8755 11.54579 16.25862 173.2543 784.694 155.944 189.6724 7715.767 136.0819 200.4871 167.8017 15.14224	763 752 765 755	15.52902 158.2723 415.942 120.308 147.0781 6072.788 98.34152 103.3348 72.76339 8.890625 17.72953 167.9454 391.268 126.4417 112.9727 5803.139 105.0769 105.3002 89.20099 8.029777
405	400 402 405	1/31008 1/3.00/8 /38.9109 150.1318 159.4496 /104.039 1/2/.135/ 1/6 145.8/6 15.2/2668 20.04265 196.6682 1119.602 167.1611 317.1754 8838.261 139.8199 231.7962 158.7536 13.14692 19.41729 150.4617 248.7669 144.5188 154.2006 5.942.44 1151.018 187.2865 198.4055 9.436708	767 757 769 759 771 762	15.542/9 13/.5/10/ 34.5423 115.31/8 86.4/6// 4963.252 95.1/359 116.709 88.300/3 8.03912 21.39519 209.7113 719.3402 166.6907 246.4296 8426.56 139.6942 174.3883 120.3333 12.55326 14.75506 13.4674 403.273 114.0134 07.06675 158.807 0.65247 111.2440 8.25673 0.396517
411 413	407	18.47692 152.5038 804.9192 131.1462 167.5154 6257.023 115.5231 186.7731 151.3885 9.792308 22.12455 205.6477 1143.057 178.5492 389.8549 991.098 150.1813 251.3834 186.0466 12.7513	773 764 775 767	13.26531 118.5673 393.8163 101.4143 127.4714 4975.006 82.08163 103.6265 73.98163 7.828571 18.70326 166 685.1632 141.4095 201.8961 7047.442 113.4748 149.4006 110.2611 9.074184
415 417	412 414	14.52924 128.1023 586.1784 112.652 172.7778 5314.096 97.56433 142.2427 115.9766 8.040936 19.33721 173.0581 655.0349 152.4884 199.0116 7228.481 130.5116 165.9651 150.7364 13.03876	777 769 779 771	19.9746 169.3619 797.8286 138.8984 169.2286 6426.863 118.7651 167.8063 106.5302 9.380952 17.29537 108.1815 588.7548 87.41313 95.01544 3570.481 70.70463 114.0019 81.82046 7.341699
419 421	417 419	17.08127 158.4417 598.523 137.8657 137.3004 6471.986 118.0813 151.8127 136.5689 10.85866 20.99298 161.8596 738.3754 143.5088 166.7965 6724.442 110.8421 160.9228 142.6456 9.326316	781 774 783 776	15.20899 131.4045 544.9011 104.3191 126.0225 5280.299 89.95056 121.7213 77.64045 7.08764 15.20042 120.3215 490.6743 98.13987 97.89562 4465.29 82.71608 113.5908 79.50522 7.757829
423 425	422	24.09649 201.2588 875.8991 174.5789 185.3772 8300.167 139.9912 192.0124 174.9956 11.58333 26.58571 217.3714 851.7619 189.2762 196.1667 9109.586 150.4857 194.0048 174.1905 13.71905	785 779 787 781 780 782	16.25159 130.6808 543.4524 103.7844 102.5391 4808.524 84.00846 116.1057 77.49471 8.334038 15.1299 132.6392 518.468 102.9134 78.28041 4589.779 84.39381 110.7546 72.27629 7.11134
427 429 453	427	10:55041 125./795 367.0026 110.2821 2/4.5940 0095.397 /92.4015 112.0536 90.09231 8.309251 21:90671 160.9009 518.379 141.7085 138.2449 6176.889 107.481 132.7318 127.9913 11.19825 32:7525 52:06:18 604.0625 6134552 74.74265 58:0726 66 112.2731 140.5725 187.9455 76.70241	789 783 791 786 793 788	15-91105 126-531 471-4555 102-2094 46.05308 4504-407 88.99553 120-4744 94.61186 8.450135 17.13333 137.7595 544.6024 113.8833 156.9214 5624.59 90.44048 122.9238 85.06905 10.95238 16.0777 140.8007 554.455 118.653 196.487 572.756 44.10563 123.5667 86.0748
455 457	434	13.12 119.3 3004.97 116.45 176.7 7407.41 180.05 241.4 251.35 10.87 12.2896 163.1641 963.3906 156.7344 174.2969 8240.18 159.6406 216.8125 216.5234 13.72656	795 791 797 793	23.01338 199.3411 890.7625 158.5318 183.1605 7368.391 130.2308 185.4482 118.7057 12.21739 18.745 150.0425 594.3275 122.47 112.665 5241.34 94.625 134.085 101.3 10.5325
459 461	439 441	10.13636 132.8864 654.0284 127.9148 129.125 6609.511 125.483 168.142 168.8011 13.29545 24.2987 286.3117 1314.221 304.5195 234.7273 13138.27 277.6104 399.1429 507.2857 32.15584	799 795 801 798	16.77488 146.2559 554.9455 119.6493 96.6564 5272.882 95.59716 127.4621 93.109 9.111374 14.27766 124.0292 490.286 97.58664 74.74322 4245.33 79.01253 107.8685 73.51566 7.325678
463 465	444 446	9.074286 116.9143 533.9886 126.0457 110.0171 5480.663 116.9943 176.8114 198.0114 14.23429 12.93836 142.6644 553.4589 152.4795 95.12329 5932.144 135.8082 190.9384 250.8219 15.12329	803 800 805 803	14.54776 130.7778 467.6979 102.115 72.58674 4380.144 80.31384 104.6589 70.12865 7.132554 17.63679 142.7524 477.3892 123.1415 128.0307 5465.983 92.33491 115.6745 91.99292 10.50236
467 469	449 452	13.01316 150.8553 691.3092 140.7105 137.9013 6540.197 139.2829 202.4803 223.7829 16.28947 13.57143 185.3214 1253.563 174.1518 330.5 10065.08 172.4732 270.7411 221.5714 14.22321	807 805 809 807	18.1945 132.8985 559.2008 112.1818 137.5539 5013.37 83.09725 116.9979 88.56448 8.970402 20.70055 149.4615 618.2005 127.3599 124.0907 5345.407 97.89286 138.7445 108.8736 9.876374
4/1 473	454	10.21233 14/.1301 //5.513/ 142.5008 211.28// /424.365 138.95/1 205.4666 186.8856 13.56849 6.038647 95.83575 515.7488 93.77778 161.3865 5274.942 97.97101 145.4688 126.6232 10.44444	811 810 813 812	20.06667 122.14/1 /21.8069 101.13/9 115./89 4063.129 /9.24598 139.0644 104.1/01 8.935632 16.41221 112.3874 529.8454 94.24618 102.0134 3851.141 70.51527 108.9256 80.48664 6.851145 20.2022 047.2
475 477 479	459 462 465	10.8 180-4907 1004-143 186./238 485.3333 1037/32 192.1019 279.1333 247.9324 18.64702 10.11765 187.0882 963.049 186.5 507.8039 10908.78 203.549 286.3725 251.7353 18.86275 9105759 16.9615 831 9272 175 8077 290.058 9104.652 200.1317 258 9712 270.1058 19.49038	815 815 817 817 819 819	21.380/33 143.2949 / 201.35/4 114.5213 119.4164 48/2.243 85.22131 139.1162 99.00949 10.81039 0.642857 1.797619 1.77381 0.380952 1.095238 7.464286 1.964286 2.72619 55.47619 75.95238 32.2652 265 6522 836.5266 235.432 280.6327 1.0407.44 181.372 228.4831 235.4541 17.4584
481 483	467	7.05303 125.8939 854.7273 133.4318 167.2197 7310.765 160.5758 213.9242 221.0076 13.7803 12.32673 203.2178 835.396 209.604 276.0594 11456.59 215.5446 277.198 274.9901 14.52475	821 821 823 823	15,42523 122,8715 460.5047 108,8621 132,271 4773.322 86,78972 115,7079 110,773 4,969526 16,88146 145,535 666,6839 125,462 148,6717 5707,517 97,56231 154,31 122,8967 9,431611
485 487	472 475	8.902299 122.2126 523.2241 123.431 113.3621 6602.764 120.6322 157.9598 161.4138 11.3046 11.4964 146.259 667.7482 151.9496 159.741 7459.237 154.8417 208.3237 219.9281 12.73381	825 825 827 827	18.2129 164.3129 1149.342 135.2645 194.8129 6929.716 110.3097 211.8258 126.7097 10.20568 17.71703 144.0165 1082.712 117.1923 131.1401 5361.838 91.68956 186.6291 114.8132 7.986264
489 491	477 480	12.06667 155.3704 649.4222 153.0519 198.8074 7817.459 159.2296 210.8 213.1481 16.14815 19.57471 281.1379 109.77 273.9425 360.3563 13737.55 260.2184 325.2644 329.7356 26.58621	829 829 831 831	25.01639 179.6667 1066.945 153.2295 94.05464 5778 151.5464 286.2787 250.0601 15.4918 23.209 195.2669 1020.855 161.6238 134.373 6231.19 127.5177 208.1125 165.4244 13.85209
493 495	483	15.55814 194.5746 855.6124 185.2403 261.9147 9012.248 167.1163 217.4186 223.8837 15.8062 7.85 101.7846 344.9423 96.2558 148.7692 4981.815 82.76923 100.4462 105.5154 8.903846 16.66495 201.164 877.091 165.200 197.201 00.601 00.601 00.0000 00000000	833 833 835 835	16./2019 15/39/3 14/4.155 116.0446 143.256 5436.271 95.10714 228.003 112.9613 11.0738 25.292 206.564 1967.376 154.92 201.088 7255.072 126.348 314.168 162.424 11.648 21.34146 155.221 148.756 123.142 10.3168 271 00.000 (201.000 10.3168)
49/ 499 501	485 490 493	9.430962 121.5021 508.8787 109.3305 115.2762 5165.042 95.45188 311.9833 128.5105 9.297071 26.82796 327.1075 1413.581 29.5757 375.8871 1478.677 751 8075 355.6130 30.1025 30.24771	837 837 839 839 841 841	24.54579 172.6703 1469.293 126.0916 175.4469 6291.553 106.989 234.0513 144.2381 10.94872 15.46953 130.4813 187.1174 107.4469 95.15576 4437.847 82.3278 167.1603 107.7646 9.29675
503	495 498	17.26119 229.7239 934.2761 205.8209 313.8507 11009.43 164.097 227.8507 205.4104 19.59701 13.17677 171.7626 623.096 148.8636 185.1313 7334.01 120.7929 150.2273 141.1061 9.70202	843 843 845 845	24.16054 179.612 1231.963 145.796 135.3813 5890.12 116.171 220.1003 168.2776 10.45151 23.30435 167.8043 515.1413 150.3288 101.9511 4895.774 110.451 133.7717 185.6168 10.0625
507 509	501 503	11.73298 166.5183 571.8429 153.3717 189.5707 7427.052 129.2618 148.0942 149.4607 13.2199 15.2 235.1111 690.0519 220.5778 189.763 10326.23 189.6815 207.7852 217.1481 17.15556	847 847 849 849	17.80046 134.8899 951.4839 104.5092 91.7156 4363.755 81.8945 162.5986 105.6009 8.688073 30.23396 165.0415 1430.004 110.7094 119.2113 4846.679 101.5057 211.5849 146.0415 9.8
511 513	506 508	17.43925 280.1963 935.0748 267.0187 284.6822 12802.82 237.0467 275.0374 280.0748 23.71028 9.810945 144.5672 485.5752 139.4826 172.0498 6777.109 118.6418 148.199 148.2687 10.46766		
515 517	511 514	9.674033 143.4144 545.7569 143.5746 145.8564 6743.536 130.0221 165.2818 162.558 13.19337 16.35052 278.5979 1045.299 273.8763 307.5155 13274.56 253.9588 309.6082 312.9175 26.16495		
519 521 523	516 519 571	10 2003723 0030023 237.7797 007.7119 1200022 196.178 244.966 249.422 18.77119 18.37143 276.8095 1009.857 273.181 321.1619 12740.03 241.1238 302.4857 312.8286 29.4381 9.41358 155.4753 564.2407 152.4444 199.7346 783.7994 149.6111 187.9641 70.070.07 0.074.074.877		
525 527	524 526	9.411348 152.7021 718.6028 163.5106 168.1064 7773.113 162.8298 219.1702 237.2128 12.66667 15.35632 238.8621 1149.425 246.4943 404.7126 12795.08 246.977 365.1149 379.6322 21.91954		
529	529	10.36943 159.0637 607.5159 152.5223 204.9745 7649.828 150.4713 182.3822 182.8471 15.3758		

Appendix 9 Correlation	N of grain size	1ay '14 with Zr/Rb I	atio (Subca	tchment co	ores)															Correlation (Al vs GS fractions)
Depth (cm)	%Fine Silt %	Coarse 5%	Very Fine%	Fine San%	Middle (%)	Coarse S%V	ery Coar	se Sand	h 0.		0	10-m			7./05		Konn	Coring: K	enn	>8um >16um >32um >64um
Kenn 10	13.94	10.76	-125 fm 12 6.69	2.68 2.68	0.06	0-1000 1100	0-20000	49.53	41.03	9.43	>8um >1 50.46	34.13	20.19	9.43	1.260812	70	Kenn	Deptn (cm)A	0.000208	-0.71995 -0.71204 -0.68076 -0.60742
15	12.22	10.15	7.05	4.7	6.42	2.8	0	42.6	36.44	20.96	57.41	43.34	31.12	20.96	1.18384	60	1.2	15	0.000261	
25	13.15	9.6	4.85	0.44	0	0	0	55.15	39.57	5.29	44.85	28.04	14.89	5.29	1.158955	50	1	25	0.000329	
30 35	13.71 13.62	10.21 8.1	4.74 2.7	0.35	0	0	0	53.97 57.39	40.95 39.61	5.08 3	46.04 42.6	29.01 24.71	15.3 11.09	5.08 3	1.121288 1.080812	40	0.8 SiltaSand	30 35	0.00035	
40	12.9	6.38	1.43	0.05	0	0	0	60.7	37.82	1.48	39.29	20.76	7.86	1.48	1.017096	30	0.6	40	0.00052	
45 50	12.83 11.53	6.36 5.62	1.49 2.26	0.06	0	0	0	60.74 62.31	37.7 34.63	1.56 3.06	39.25 37.7	20.74 20.21	7.91 8.68	1.56 3.06	0.939349	20	0.4	45 50	0.000563	
55	12.14	5.97	1.7	0.36	0	0	0	61.92	36.02	2.06	38.08	20.17	8.03	2.06	0.892513	10	0.2	55	0.000373	
60	11.86	8.04	4.46	0.67	U	0	0	58.35	36.52	5.13	41.66 0.81909 0	25.03).787306 (13.17 0.725028 0.	5.13 .602864	0.87594	0	10 15 20 25 30 35 40 45 50 55 60	Coring: K	0.000599 lein Krotze	enburg
Klein Krotze	17 0.4	25.52	14 75	4.02	0.08	0	0	27.16	53.00	18.85	72.83	62 31	44 37	18.85	2 272236			Depth (cm]A	0.000327	0.121625 0.116887 0.077395 0.17694
130	18.04	21.62	9.91	0.98	0	0	0	36.59	52.52	10.89	63.41	50.55	32.51	10.89	2.015957	_		130	0.000344	
135 140	20 16.98	28.42 21.31	14.49 13.43	1.43 6.37	0.25	0	0	24.92 30.81	59.16 49.14	15.92 20.05	75.08 69.19	64.34 58.34	44.34 41.36	15.92 20.05	2.578443 1.662665		Klein Krotzenburg	135 140	0.000262	
145	13.97	13.85	8.89	22.29	10.29	0.02	0	22.35	36.16	41.49	77.66	69.31	55.34	41.49	2.041123	90	3	145	0.000408	
150	20.11	23.27	8.82	0.67	0	0	0	33.89	56.62	29.94	66.1	52.87	32.76	29.94	2.292467	80	2.5	150	0.000228	
160	25.78	32.95	9.73	0.49	0	0	0	20.63	69.15	10.22	79.37	68.95 34.25	43.17	10.22	2.444199	60		160	0.000438	
100	18.76	24.2	11.31	1.32	ő	0	o	32.91	54.47	12.63	67.1	55.59	36.83	12.63	2.301642	50 40	1.5 —Silt+Sand	170	0.000281	
175 180	23.01 21.91	24.52 27.82	8.15 10.43	0.5 1.51	0	0	0	30.38 27.21	60.97 60.85	8.64 11.94	69.63 72.79	56.18 61.67	33.17 39.76	8.64 11.94	2.34884 2.378085	30	1Zr/Rb	175 180	0.000236	
185	21.33	24.84	7.61	0.38	0	0	0	33.86	58.15	7.99	66.14	54.16	32.83	7.99	2.324923	20	0.5	185	0.000347	
190 195	20.41 21.62	20.48 22.23	6.11 5.75	0.36	0	0	0	38.71 36.72	54.82 57.31	6.47 5.97	61.3 63.28	47.36 49.82	26.95 28.2	6.47 5.97	2.002297 2.047946	0	0	190 195	0.000296	
200	23.4	20.4	5.12	0.3	0	0	0	35.43	59.15	5.42	64.58	49.22	25.82	5.42	2.144204		202220222222222222222222222222222222222	200	0.000204	
205	24.29 21.91	23.92 12.66	5.48 2.52	0.17	0	0	0	32.28 42.34	62.07 54.82	2.84	57.67	53.86 37.42	29.57	2.84	1.867225			205	0.000227	
215	18.56	16.06	7.23	2.74	1.77	0.89	0	38	49.36	12.63	61.99	47.25	28.69	12.63	2.063737			215	0.000391	
Lauffen											0.005002		0.400475 0.					Depth (cm]A	d	0.327517 0.353133 0.413369 0.44204
100 105	11.79 11.26	15.19 14.86	17.28 17.28	16.79 17.78	5.42 9.5	0.02	0	24.82 20.8	35.67 33.75	39.51 45.45	75.17 79.21	66.49 71.58	54.7 60.32	39.51 45.45	2.394886 2.389468			100	0.0003	
110	12.05	15.92	17.3	14.82	5.95	0.15	0	25.26	36.52	38.22	74.73	66.19	54.14	38.22	2.418663		Lauffen	110	0.000341	
115 120	12.38 13.2	17.06 18.17	18.42 18.06	14.72 11.68	5.83 3.48	0.09	0	23.34 26.61	37.6 40.12	39.06 33.27	76.66 73.4	68.5 64.65	56.12 51.45	39.06 33.27	2.501277 2.536601	10	2.8	115	0.000448	
125	11.98	16.67	18.79	17.83	6.28	0.15	0	20.72	36.23	43.05	79.27	71.7	59.72	43.05	2.569767	8	2.7	125	0.000422	
130	17.77	20.46	14.03	5.91	0.05	0	0	28.7	46.57	21.11	71.3	60.51	42.74	21.11	2.491577	6	2.5	130	0.000368	
140 145	18.17 18.32	22.75 23.66	14.14 14.53	4.84 4.92	0.25	0	0	29.15 27.77	51.62 52.35	19.23	70.84	60.15 61.85	41.98	19.23 19.88	2.603208	5	0 2.4 —Silt+Sand	140	0.00027	
150	15.8	20.31	17.2	7.71	0.34	0	0	28.5	46.24	25.25	71.49	61.36	45.56	25.25	2.460227	3	0 2.3Zr/Rb	150	0.000272	
155	16.92	18.68	13.78	6.02 12.97	4.39	0.07	0	32.1 22.56	47.6	20.3 34.38	67.9 77.45	55.9 68.3	38.98 53.43	20.3 34.38	2.303282	2	- 2.1	155 1	0.000329	
165	12.67	17.03	18.29	17.5	6.53	0.41	0	19.65	37.61	42.74	80.34	72.43	59.76	42.74	2.477068	1	0	165	0.000368	
175	7.88	11.58	19.29	28.45	11.78	0.43	o	15.13	24.93	59.95	84.88	79.41	71.53	59.95	2.453688		*************	175	0.000265	
180 185	4.08	6.61 15.15	16.36 28.38	39.42 24.68	20.97 7.63	0.32	0	9.29 11.7	13.65 27.07	77.06	90.71 88.3	87.76 84.09	83.68 76.38	77.06 61.23	2.406705 2.547751			180 185	0.000459	
190	3.15	3.79	8.28	27.31	43.47	5.99	0	5.84	9.12	85.05	94.16	91.99	88.84	85.05	2.728846			190	0.000484	
Romerberg											0.200299 0	.198197	0.167021 0.	. 145906				Depth (cm]A	l I	0.25422 0.269998 0.253538 0.328053
148 153	12.7 11.87	9.6 10.04	5.62 7.49	1.15 4.91	0	0	0	48.44 46.75	44.79 39.87	6.77 13.38	51.56 53.24	29.07 35.28	16.37 23.41	6.77 13.38	1.419046	_		148 153	0.000136	
158	11.28	10.81	7.82	3.46	0.08	0	0	50.5	38.14	11.36	49.5	33.45	22.17	11.36	1.445302		Romerberg	158	0.000136	
163 168	10.89 9.44	12.31 9.13	9.32 6.94	5.21 4.05	0.59	0	0	49.01 57.51	35.86 31.21	15.13 11.27	50.98 42.48	38.32 29.84	27.43 20.4	15.13 11.27	1.356289	70	2.5	163 168	0.000136	
173	8.79	8.96	7.71	5.64	0.67	0	0	56.96	29.02	14.02	43.05	31.77	22.98	14.02	1.336268	60	2	173	0.000198	
183	12.37	9.56	7.52	6.13	4.3	0.9	0	42.49	38.65	18.85	57.51	40.78	28.41	18.85	1.446983	50		183	0.000249	
188	9.54	9.65	9.02	9.11	6.66	0.34	0	44.97 52 38	29.89	25.14	55.02	44.32	34.78	25.14	1.375558	40		188	0.000151	
198	8.83	6.82	5.16	3.01	0.29	0	0	62.71	28.83	8.46	37.29	24.11	15.28	8.46	1.302697	20	1Zr/Rb	198	0.000158	
203 208	9.04 9.23	7.36	5.46 5.78	2.6 3.29	0.06	0	0	60.74 60.47	31.14 30.32	8.12 9.21	39.25 39.53	24.52 25.97	15.48 16.74	8.12 9.21	1.311207 1.333333	10	0.5	203 208	0.000275	
213	9.27	7.5	5.56	2.6	0.05	0	0	60.77	31.02	8.21	39.23	24.98	15.71	8.21	1.363481	0	0	213	0.000296	
218	10.91	8.46	6.41	2.89	0.05	0	0	57.74	32.89	9.31	45.2	28.46	17.81	9.31	1.56877		2 2 2 2 3 5 5 6 6 6 6 7 7 9 6 7 7 7 8 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7	218	0.000275	
228	9.87	7.79	5.66	2.74	0.06	0	0	59.81	31.74	8.45	40.2	26.12	16.25	8.45	1.667433			228	0.000261	
238	12.63	9.33	5.87	2.54	0.06	0	0	55.56	35.97	8.47	44.44	30.43	17.8	8.47	1.89471			238	0.000181	
Sindlingen											0.052141 0	0.028362	-0.08948 -	0.11609				Coring: S Depth (cm]A	indlingen I	0.514547 0.473103 0.446411 0.44118
120	13.2	14.28	11.05	11.2	9	2.88	0	28.21	37.67	34.12	71.8	61.61	48.41	34.12	1.897486	_		120	0.000312	
125	15.85	16.93	11.99	9.51	3.41	0.49	0	30.27	41.67	25.18	69.73	57.96	47.98	25.18	1.660077		Sindlingen	125	0.000198	
135	14.03	15.9	12.61	12.32	6.96	1.63	0	26.26	40.22	33.52	73.73	63.45 55.08	49.42	33.52	1.74856	90	2.5	135	0.000258	
145	19.29	17.08	7.17	2.65	0.06	0	0	38.26	51.87	9.87	61.75	46.25	26.96	9.87	1.832547	80		145	0.000152	
150 155	19.29 20.47	19.38 19.81	8.79 8.39	3.23 3.2	0.06	0	0	35.59 33.83	52.33 54.52	12.08 11.65	64.41 66.17	50.75 51.93	31.46 31.46	12.08 11.65	1.869996 1.946514	60		150 155	0.000116	
160	20.12	17.38	7.41	3.02	0.07	0	0	36.1	53.4	10.5	63.9	48	27.88	10.5	2.10354	50	1.5Silt+Sand	160	0.000301	
165 170	19.55 16.93	20.36 19.25	9.27 12.12	4.93 13.17	0.61 6.37	0.1	0	32.16 22.26	53.04 45.97	14.8 31.76	ь7.85 77.73	54.72 67.94	35.17 51.01	14.8 31.76	∠.042807 2.164677	30	1Zr/Rb	165 170	0.000225	
175	21.27	16.87	6.46	4.18	0.49	0 12	0	34.2	54.66	11.14	65.79	49.27	28	11.14	2.066168	20	- 0.5	175	0.00035	
185	15.3	16.59	11.65	11.44	3.11	0.13	0	30.1	43.69	26.2	69.89	58.09	42.79	26.2	2.01556	0	0	185	0.000214	
190 195	18.01 20.17	15.86 20.04	9.32 9.2	8.4 4.85	3.71 0.55	0.07	0	30.18 30.92	48.33 54.47	21.49 14.61	69.84 69.08	55.37 54.81	37.36 34.64	21.49 14.61	1.983233		112 1131 1146 1155 1155 1155 1155 1155 1155 115	190 195	0.000306	
200	17.13	19.95	11.75	10.62	3.1	0	0	26.66	47.86	25.47	73.34	62.55	45.42	25.47	1.943111			200	0.000232	
205	12.24	11.26	ь.57	1.7	18.91	5.15	0	21.72	33.94	38.34	-0.0663	ь1.83 0.17588	49.59	38.34 0.44325	1.482265	L		205	u.UUU349	
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Appendix 7	may 2014											
Flood event data												
Depth (cm) Core (#)	Flood event	Clay	Silt	Sand	Silt+Sand	Zr/Rb						
446 Bienen 6	1784	32.1	55.27	12.63	67.9	1.846883						
560 Bienen 7	1729	34.95	57.21	7.83	65.04	1.42952						
564 Bienen 7	1726	29.43	62.1	8.48	70.58	1.673995						
659 Bienen 8	1682	20.3	29.32	50.39	79.71	1.555375	shifted					
683 Bienen 8	1671	36.96	46.71	16.32	63.03	1.400364	shifted					
	Normalized	(elemental	count / (Mc	inc count	+ Mo coh co	unt))						
Depth (cm) Flood even	Si	К	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Zn	
446 1784	0.003033	0.033441	0.129732	0.035742	0.022297	1.390508	0.031834	0.044756	0.058793	0.003545	0.008559	
560 1729	0.007159	0.058218	0.240734	0.051701	0.042128	2.016871	0.036929	0.055031	0.052791	0.003311	0.011441	
564 1726	0.008979	0.0569	0.298224	0.051381	0.047759	1.82751	0.034626	0.061358	0.057963	0.001994	0.010124	
659 1682	0.004726	0.050135	0.243651	0.042107	0.049185	1.691992	0.033292	0.058041	0.051781	0.003551	0.008654	
683 1671	0.004305	0.050033	0.204551	0.04408	0.057711	1.995458	0.035354	0.056074	0.049508	0.003071	0.009377	
	Al-Standardi	ized (norma	lized count,	/ Al count)								
Depth (cm) Flood even	Si	К	Ca	Ti	Mn	Fe	Rb	Sr	Zr	Pb	Zn	
446 1784	12.9	142.7	553.5	152.5	95.1	5932.1	135.8	190.9	250.8	15.1	36.5	
560 1729	12.6	117.7	314.5	100.7	128.3	4819.8	77.2	87.1	84.5	5.7	21.0	
564 1726	19.1	174.0	318.5	159.9	157.9	6868.8	118.1	121.7	133.3	11.2	35.6	
659 1682	28.0	296.9	1443.0	249.4	291.3	10020.9	197.2	343.8	306.7	21.0	51.3	
683 1671	23.8	276.5	1130.4	243.6	318.9	11027.5	195.4	309.9	273.6	17.0	51.8	

Appendix 6 Bienen III - Bienen	Al-standardization	italic = not <u>used</u>							
Depth Real De 167 : 169 : 171 : 173 : 177 : 179 : 181 : 183 : 185 : 187 : 189 : 191 :	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Jun Al Alshired Jun Al Alshired Jun 0.000232 0.000231 Al 0.000231 0.000316 Al 0.000230 0.000316 Al 0.000305 0.000330 Al 0.000305 0.000327 Al 0.000227 0.000322 Al 0.000230 0.000237 Al 0.000232 0.000231 Al 0.000231 0.000247 Al 0.000231 0.000247 Ja 0.000231 0.000246 Ja 0.000231 0.000247 Ja 0.000231 0.000247 Ja 0.000231 0.000246 Ja 0.000231 0.000246 Ja 0.000250 0.000259 Ja 0.000256 0.000259 Ja 0.000257 0.000259	titeden 3 <2µm <4µm <5µm norm 0.012028 0.01888 0.02996	Normalized Bilenen forain size: clay Core segme < 2 µm	fractions < € µm < € µm <th <="" <<="" td=""><td></td><td></td><td></td></th>	<td></td> <td></td> <td></td>			
195 197 199 201 203 205 207 211 213 213 215 217 219 211	60 12.37 20.774 191 12.23 27.74 193 13.14 29.38 195 11.02 24.11 196 12.68 28.06 102 13.81 30.94 103 13.37 29.66 100 13.37 29.66 111 44.39 33.3 111 43.92 31.24 112 12.07 27.33	46.72 (0.00034) 46.72 (0.00035) 46.72 (0.00035) 46.72 (0.00035) 40.00035 (0.00035) 40.62 (0.00035) 40.62 (0.00035) 40.62 (0.00035) 40.22 (0.00035) 40.		September Real Deput 545 1 547 2 551 2 555 2 557 2 561 2 563 2 565 2 565 2 567 2 567 2	$\langle 2 \mu m \rangle < 4 \mu m \rangle < \langle 2 \mu m \rangle < 4 \mu m \rangle < \langle 2 \mu m \rangle < 4 \mu m \rangle < \langle 2 \mu n \rangle $	Burn All shifted 43.03 0.000255 48.06 0.000318 51.14 0.000318 51.41 0.000328 54.64 0.000328 55.279 0.000456 51.51 0.000334 52.81 0.000274 51.85 0.000456 50.88 0.000445 52.96 0.000326	Bienen <u>(2 µm</u> norm 0.242	7 4 µm <8 µm 097 0.347369 0.374181	
223 225 227 229 231 233 235 237 237 239 239	10.00 26.86 121 12.04 26.86 223 13.86 31.48 224 14.57 33.18 225 13.71 31.31 230 14.47 33.08 232 14.76 33.86 234 14.65 33.48 237 12.55 28.89 239 11.29 25.3	45.09 (2003257 20003257 52.12 (2003027 2000304 52.19 (200302 2000304 52.19 (200304 200034 52.19 (200304 200034 55.07 (200256 2000313 42.18 (200313 2000313 42.18 (200315 2000315 42.19 (200316 2000315		571 573 575 577 579 581 583 583 585 585 587	10.43 2.3.96 564 9.01 18.66 564 9.01 18.66 567 10.88 25.03 569 10.14 25.06 571 9.51 25.28 576 9.1 24.86 579 14.18 31.38 581 15.03 33.8	37.85 0.000379 29.43 0.000432 42.6 0.000432 45.23 0.000373 48.24 0.000373 49.83 0.000275 47.69 0.000379 51.61 0.000379 55.57 0.000439			
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Agenda 5C Instart @ Montellade andré	
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 | Ba Ta W Ir Au Hg Pb D1 Moinc Mocoh |
| 120 | 0.000312 | 0.004978 | 5.52E-05 | 0.000984
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 | 0 0.001199 0.005688 0.010002 0.000886 0.004268 0.00328 0.010789 0.00259 0.757262 0.242738 |
| 125 | 0.000198 | 0.004607 | 4.16E-05 | 0.000899
 | 1.33E-05 0.00227

 | 8 0.049205 0

 | 0.153705 | 2.21E-05 0.046811

 | 0.001341 0 | .006444 0.022883 | 1.530522
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 | 0.002189 | 0.008933 0.00392 | 0.001207 0.03412
 | 3 0.052719
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 | 0 0.001217 0.005416 0.010536 0.001238 0.004348 0.004504 0.011779 0.001815 0.754863 0.245137 |
| 130 | 0.00033 | 0.005592 | 9.2E-06 | 0.001044
 | 0 0.00153

 | 1 0.056683 0

 | 0.170328 | 1.93E-05 0.052143

 | 0.001752 0 | .007905 0.023523 | 1.757757
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 | 0.002095 | 0.012112 0.004743 | 0.000889 0.03717
 | 4 0.053812
 | 0.061712 0 | 0.000686 0.000 | 0123 0.000764 0.000522
 | 0 0.001224 0.005869 0.010176 0.001065 0.004488 0.004058 0.008625 0.003417 0.755254 0.244746 |
| 135 | 0.000258 | 0.003788 0 | 0.000107 | 0.000816
 | 4.36E-06 0.00114

 | 5 0.043013 0

 | 0.135007 | 0 0.042647

 | 0.001555 0 | .004625 0.026173 | 1.567141
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 | 0.001482 | 0.008963 0.004147 | 0.000793 0.03514
 | 9 0.053638
 | 0.06146 0 | 0.000388 0.000 | 0213 0.000597 0.000433
 | 0 0.000868 0.004669 0.00894 0.000911 0.004717 0.004032 0.008348 0.003002 0.755384 0.244616 |
| 140 | 0.000246 | 0.003002 | 2.4E-05 | 0.000747
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 | 5 0.04019 0

 | 0.134183 | 0 0.041295

 | 0.001602 0 | .003317 0.027386 | 1.595692
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 | 0.002227 | 0.009466 0.004417 | 0.000891 0.03553
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 | 0 0.000771 0.004405 0.008442 0.000864 0.004504 0.00404 0.007573 0.002836 0.751433 0.248567 |
| 145 | 0.000152 | 0.002967 | 5.25E-05 | 0.000764
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 | 0.002155 | 0.011519 0.004486 | 0.000879 0.03495
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 | 0 0.000701 0.004296 0.008073 0.000938 0.004231 0.003473 0.007344 0.002816 0.751873 0.248127 |
| 150 | 0.000116 | 0.004063 | 4.77E-05 | 0.000717
 | 4.42E-06 0.00152

 | 3 0.04665 0

 | 0.153891 | 0 0.049017

 | 0.001568 0 | .003554 0.031729 | 1.732548
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 | 7 0.055054
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 | 0 0.001258 0.005393 0.009668 0.00139 0.004455 0.003499 0.007614 0.00351 0.751864 0.248136 |
| 155 | 0.000285 | 0.004321 | 6.9E-05 | 0.000861
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 | 8 0.045311 0

 | 0.155644 | 0 0.047143

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 | 0 0.000847 0.005253 0.009384 0.000595 0.004392 0.003946 0.007218 0.003252 0.756403 0.243597 |
| 160 | 0.000301 | 0.005165 | 0.00011 | 0.000884
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 | 0 0.000968 0.0051 0.01 0.00102 0.004322 0.003644 0.006818 0.003215 0.754837 0.245163 |
| 165 | 0.000225 | 0.003295 | 4.4E-05 | 0.000763
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 | 5 0.039408 0

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 | 0.001364 0 | .002686 0.021167 | 1.481792
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 | 0.002461 | 0.007587 0.004121 | 0.000737 0.03383
 | 9 0.049502
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| 170 | 0.000335 | 0.004722 | 2.67E-05 | 0.000904
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 | 7 0.045456 0

 | 0.123557 | 0 0.047825

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| 175 | 0.00035 | 0.005518 | 9.45E-05 | 0.000791
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 | 0.001392 0 | .002885 0.028887 | 1.573366
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 | 0 0.001014 0.005742 0.010608 0.000785 0.004873 0.004323 0.005671 0.00311 0.751831 0.248169 |
| 180 | 0.000301 | 0.00454 | 9.47E-05 | 0.000787
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| 185 | 0.000214 | 0.003404 | 6.7E-05 | 0.000754
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 | 0 0.001068 0.005584 0.0105 0.000913 0.004183 0.003914 0.00527 0.003022 0.753486 0.246514 |
| 190 | 0.000306 | 0.004485 | 3.39E-05 | 0.000824
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| 195 | 0.00028 | 0.004996 | 8.09E-05 | 0.000749
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| 205 | 0.000349 | 0.005222 | 7 1E-05 | 0.000803
 | 1.8E-05 0.00199

 | 5 0.053692

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 | 198.6657 1 | 235955 0.4 | 7191 1 716292 0 713483
 | 0 3 839888 18 22191 32 03933 2 837079 13 67135 10 50843 34 5618 8 297753 2425 772 777 5758 |
| 125 | 1 | 23.21429 | 0.209821 | 4.53125
 | 0.066964 11.4776

 | 8 247.9643

 | 774.5848 | 0.111607 235.9018

 | 6.758929 3 | 2.47321 115.317 | 7712.955
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 | 660714 6.90 | 0625 145.2902

 | 11.03125 | 45.01786 19.75446 | 6.080357 171.959
 | 8 265.6741
 | 321.7277 1 | .638393 1.05 | 8036 3.151786 1.727679
 | 0 6.133929 27.29464 53.09375 6.241071 21.91071 22.69643 59.36161 9.147321 3804.08 1235 348 |
| 130 | 1 | 16.93315 | 0.027855 | 3.16156
 | 0 4,63509

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 | 515.8134 | 0.058496 157.9081

 | 5,306407 2 | 3.93872 71.23677 | 5323.106
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 | 615599 2.518 | 8106 70.039

 | 6.345404 | 36.67967 14.36212 | 2.693593 112 576
 | 5 162.961
 | 186.8858 2 | .077994 0 37 | 3259 2.314763 1.582173
 | 0 3.707521 17.77437 30.81616 3.225627 13.59053 12.28969 26.11978 10.34819 2287 175 741 1755 |
| 135 | 1 | 14 66554 | 0.415541 | 3 158784
 | 0.016892 4.43581

 | 1 166 5101

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 | 5 736486 | 34 69595 16 05405 | 3 070946 136 067
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 | 237 9223 1 | 503378 0.82 | 4324 2 310811 1 675676
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| 140 | 1 | 12 19476 (| 0.007378 | 3 033708
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 | 8 163 2846

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 | 1 237 3333 1

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| 150 | , | 35 08307 0 | 0.412214 | 6 1908/
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 | 7 402 8473

 | 1328 030 | 0 423 2001

 | 13 54198 2 | 0.68702 274 | 14961 6
 | 152 1008 4

 | 496183 1 229 | 8244 133 1670

 | 17 84733 | 88.96183 33.38021 | 10.49618 306.450
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| 100 | 1 | 15 17702 (| 0 2422224 | 3 024845
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 | 5 242236 1 | 0 72081 104 2091 | 5694 462
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 | 500317 0.69 | 8323 48 61401

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 | 5 278107 9 | 300408 83 73660 | 5039.403
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 | 1 120 0 221
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 | 0 4.050/15 20.2010 40.05/3 5.040023 16.00/5/ 10.12 51.5020 11.14044 535.052 105.67 |
| 170 | - | 14.08242 | 0.07507 | 2.055055
 | 0.019231 8.34003

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 | 566667 U.L | 0625 49.1

 | 12.56667 | 30.35 18.38/5 | 2.32916/ 165./54
 | 2 216.1167
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 | | 111.4851 | 6473.397
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| Coring: | Klein Krotz (| (normalized o | counts) |
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 | A B | s se | Br RD
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| 125 | 0.000327 | 0.007503 0 | 0.000137 | 0.001116
 | 8.8E-06 0.00124

 | / 0.055582

 | 0.02404 | 0 0.056471

 | 0.001682 0 | .002611 0.009088 | 2.044956
 | 0.019152 0.

 | 000107 | 0 0.006753

 | 0.00219 | 0.004765 0.004932 | 0.000459 0.036
 | 0.032335
 | 0.083165 0 | 1.000633 5.84 | E-05 3.04E-05 0
 | 0 0.001503 0.005/12 0.011369 0.001029 0.004881 0.004685 0.002842 0.004155 0.750753 0.249247 |
| 130 | 0.000344 | 0.006556 0 | 0.000129 | 0.000859
 | 2.18E-05 0.00181.

 | 2 0.057085 1

 | 0.021614 | 11 11 ID61 / VX

 | 0.002109 0 | .002867 0.01075 | 1 6 7 7 7 8 1
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 | | 0.004040 0.00434 | 0.000040.000004
 |
 | 0 000400 0 | | 0400 B 00F 0F 0
 | 0 0 001103 0 005530 0 011003 0 001531 0 005101 0 001630 0 003001 0 003100 0 310030 0 051330 |
| 135 | 0.000262 | | |
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 | | 0 0.000750

 | | | 2.044303
 | 0.02348 3

 | .80L-03 | 0 0.007534

 | 0.0028/1 | 0.004819 0.00474 | 0.000618 0.03974
 | 7 0.031609
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 | 0 0.001187 0.005523 0.011297 0.001521 0.005101 0.004629 0.002894 0.007188 0.748278 0.251722 |
| 140 | | 0.007114 (| 0.000177 | 0.000698
 | 3.15E-05 0.0024

 | 5 0.05281 (

 | 0.017639 | 0 0.055916

 | 0.001856 0 | .002895 0.009675 | 2.000964
 | 0.019012 0.

 | 000192 | 0 0.006583

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0.004657 0.003986 | 0.000618 0.03974
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 | 7 0.031609
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 | 0.080129 0 | 0.000544 0.001 | 0102 7.39E-05 0
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 | 0 0.001187 0.005523 0.011297 0.001521 0.005101 0.004629 0.002894 0.007188 0.748278 0.251722
0 0.00151 0.005948 0.011894 0.001021 0.00494 0.004512 0.002557 0.00495 0.746836 0.253164 |
| 145 | 0.000274 | 0.007114 0 | 0.000177
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 | 6 0.05281 (
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 | 0.002871
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 | 7 0.031609
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| 150 | 0.000274 0.000408 | 0.007114 (
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 | 0 0.001187 0.005523 0.011297 0.001521 0.00510 0.004529 0.002849 0.007188 0.748278 0.251722
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Juliace J	inpies	(ppin)				
SAMPLE	Sr	Rb	Pb	Zn	Fe	Mn
9a	83.93	71.62	38.9	157.89	13209.57	479.38
9b	90.8	69.13	46.75	222.75	14174.58	550.84
18a	115.42	72.68	47.14	153.98	16452.15	493.14
18b	99.32	62.38	52.96	95	13313.63	462.91
AVG	97.3675	68.9525	46.4375	157.405	14287.48	496.5675

Appendix 5B

Appendix 5A				
Moselle				
Coring: Kenn (normalized counts)				
Depth (cm)Al Si P S Cl Ar K Ca Sc	Ti V Cr Mn Fe Co Ni Cu	Cu Zn Ga As Se Br Rb Sr Zr Ag Cd	Sn Sb Cs Ba Ta V	W Ir Au Hg Pb D1 Moinc Mocoh
10 0.000208 0.002231 0.000168 0.000905 0 0.000654 0.032573 0.014141	0 0.03412 0.001496 0.002544 0.018427 1.523494 0.015727 0.000182 0	0.001408 0.047371 0.000915 0.00397 0.004433 0.002064 0.033343 0.02578 0.042039 0.000211 9.620	2E-05 8.37E-05 1.02E-05 0 0.000664 0.00502	0.006501 0.00135 0.004717 0.00271 0.007612 0.00296 0.782105 0.217895
15 0.000261 0.003861 0.000211 0.00098 2.55E-06 0.000954 0.046159 0.012509	0 0.045012 0.001792 0.002707 0.025642 1.829588 0.01829 0.000399 0	0.000796 0.036032 0.001827 0.005508 0.005084 0.001997 0.039662 0.028712 0.046954 0.00031 0.000	J0112 7.77E-05 0 0 0.000699 0.005392	0.007695 0.00166 0.005053 0.003612 0.00699 0.00401 0.771014 0.228986
20 0.000283 0.004344 0.000183 0.000868 0 0.001502 0.053366 0.012508	0 0.050316 0.002104 0.003174 0.026995 2.033477 0.018742 0.000814	0.00068 0.03332 0.00209 0.005436 0.004858 0.001677 0.042317 0.029878 0.049187 0.000534 0.000	0122 0.000106 0 0 0.001019 0.006058	0.008674 0.001315 0.00479 0.003796 0.006856 0.004736 0.76545 0.23455
25 0.000329 0.005903 0.000182 0.000923 0 0.001801 0.063669 0.012859	0 0.054689 0.002297 0.003241 0.024867 2.043517 0.018689 0.000866 0	0.000742 0.02674 0.003259 0.005752 0.004914 0.000762 0.044433 0.030889 0.051496 0.000596 0.000	J0138 8.37E-05 0 0 0.001111 0.005363	0.010165 0.001067 0.004974 0.004626 0.006283 0.003774 0.75738 0.24262
30 0.00035 0.006788 0.000227 0.001021 4.25E-06 0.002295 0.072883 0.01133	0 0.062754 0.002277 0.003761 0.027571 2.322807 0.021722 0.001247 0	0.001111 0.024884 0.003439 0.006501 0.005289 0.000921 0.049185 0.032778 0.055151 0.000573 0.000	J0297 8.49E-05 0 0 0.001582 0.005925	0.010085 0.001463 0.005765 0.004484 0.005699 0.005389 0.75436 0.24564
35 0.000403 0.006907 0.000157 0.000942 6.47E-06 0.002355 0.076743 0.01095	0 0.067953 0.002694 0.003824 0.027768 2.679204 0.024327 0.000741 0	0.000495 0.019928 0.00288 0.006892 0.005548 0.000671 0.052793 0.033461 0.057059 0.000765 0.000	J0303 8.05E-05 0 0 0.001732 0.006116	0.009579 0.001879 0.005434 0.004542 0.00551 0.006528 0.750221 0.249779
40 0.00052 0.007441 0.000222 0.001023 3.81E-06 0.002006 0.082839 0.010007	0 0.073331 0.002896 0.004226 0.024944 2.864377 0.025986 0.000648	2.06E-05 0.017122 0.003039 0.008689 0.005791 0.000556 0.056179 0.0346 0.057139 0.000551 0.000	0247 0.000107 0 0 0.001832 0.006148	0.009757 0.001684 0.005334 0.004515 0.00398 0.00723 0.747988 0.252012
45 0.000563 0.008344 0.000149 0.000931 7.74E-06 0.002046 0.089463 0.009927	0 0.080084 0.003304 0.004394 0.021967 3.131638 0.028003 0.000741	1.7E-05 0.018168 0.003187 0.0074 0.006067 0.000759 0.06004 0.03654 0.056399 0.000501 0.000	J0241 9.75E-05 0 0 0.001752 0.005987	0.009591 0.002116 0.005622 0.004693 0.004659 0.007764 0.744 0.256
50 0.000422 0.007056 0.000135 0.000881 0 0.002168 0.085943 0.00927	0 0.07761 0.003249 0.004498 0.020821 3.210773 0.03047 0.001157	0 0.016675 0.003189 0.007462 0.006024 0.000657 0.060639 0.03685 0.055398 0.000494 0.000	J0187 3.37E-05 0 0 0.001676 0.006051	0.00961 0.00219 0.005857 0.004469 0.004547 0.008546 0.743751 0.256249
55 0.000373 0.006885 0.000185 0.000858 0 0.002272 0.084629 0.009291	0 0.077188 0.002978 0.004407 0.019932 3.148108 0.028189 0.000358	3.88E-06 0.017477 0.002588 0.007992 0.007089 0.000412 0.059414 0.036469 0.053028 0.000537 0.000	J0287 9.94E-05 0 0 0.001765 0.006068	0.009551 0.002877 0.00567 0.004807 0.004091 0.008605 0.745045 0.254955
60 0.000599 0.008687 0.000247 0.00105 0 0.001976 0.094887 0.011142	0 0.08313 0.003359 0.004827 0.022467 3.746324 0.033771 0.000326	0 0.017156 0.003477 0.010135 0.006485 0.000805 0.061741 0.038363 0.054082 0.000515 0.000	J0233 1.65E-05 0 0 0.001996 0.006107	0.009715 0.001894 0.005723 0.00454 0.00492 0.010466 0.73867 0.26133
Coring: Kenn (normalized counts + Al standardized)				
Depth (cm)Al Si P S Cl Ar K Ca Sc	Ti V Cr Mn Fe Co Ni Cu	Cu Zn Ga As Se Br Rb Sr Zr Ag Cd	Sn Sb Cs Ba Ta V	W Ir Au Hg Pb D1 Mo inc Mo coh
10 1 10.71311 0.808743 4.346995 0 3.142077 156.3825 67.89344	0 163.8115 7.18306 12.21585 88.46995 7314.363 75.5082 0.874317 6	6.759563 227.429 4.393443 19.06011 21.28142 9.909836 160.082 123.7705 201.8333 1.010929 0.461	i1749 0.401639 0.04918 0 3.185792 24.10109	31.21311 6.480874 22.64481 13.01093 36.54645 14.21038 3754.918 1046.126
15 1 14.78537 0.807317 3.75122 0.009756 3.653659 176.7756 47.90732	0 172.3829 6.860976 10.36585 98.20244 7006.805 70.04634 1.529268	3.04878 137.9927 6.997561 21.09268 19.47073 7.64878 151.8951 109.9585 179.8195 1.187805 0.429	.9268 0.297561 0 0 2.678049 20.64878	29.46829 6.356098 19.35122 13.83415 26.76829 15.35854 2952.766 876.9512
20 1 15.34732 0.645688 3.067599 0 5.305361 188.5268 44.18648	0 177.7506 7.433566 11.21445 95.36597 7183.667 66.20979 2.876457 2	2.403263 117.7086 7.382284 19.20513 17.16317 5.925408 149.4942 105.5501 173.7622 1.885781 0.431	1235 0.375291 0 0 3.601399 21.40093	30.64103 4.645688 16.92308 13.41026 24.21911 16.73193 2704.107 828.5944
25 1 17.95789 0.553684 2.808421 0 5.48 193.6884 39.11789	0 166.3705 6.987368 9.861053 75.64842 6216.653 56.85474 2.635789 2	2.256842 81.34737 9.915789 17.49684 14.94947 2.317895 135.1726 93.96842 156.6589 1.812632 0.418	.8947 0.254737 0 0 3.378947 16.31368	30.92421 3.246316 15.13263 14.07368 19.11368 11.48 2304.053 738.0821

				45.7966	7 4649.728		54.08366			93.07519	61.91851								11.40709		
60	1 14.50986 0.412615 1.754271 0	3.30092 158.4875 18.60972	0 138.8502 5.6110	38 8.061761 37.5256.	2 6257.38	56.40604 0.5453	35 0 28.6544	5.806833 16.9277	3 10.8318	1.344284 103.1248	64.07622 9	0.33114 0.86	6071 0.388962	0.027595	0 3.3	3771 10.19974 16.	22733 3.162943	9.558476 7.58	443 8.218134	17.48095 123	\$3.779 436.4928
55	1 18.46875 0.495833 2.302083 0	6.09375 227.0167 24.92292	0 207.0563 7.9895	83 11.82292 53.4666	7 8444.827	75.61667 0.9604	17 0.010417 46.88333	6.941667 21.437	5 19.01667	1.104167 159.3792	97.82708 1	42.2479 1.441	1667 0.76875	0.266667	0 4.7	5417 16.27708 25.	62083 7.716667	15.21042 12.8	375 10.975	23.08333 19	J98.59 683.9188
50	1 16.7119 0.319703 2.085502 0 5	5.133829 203.5539 21.95539 0	0 183.816 7.6951	67 10.65428 49.3141.	3 7604.615	72.16729 2.7397	77 0 39.49442	7.553903 17.6728	6 14.26766	1.555762 143.6208	87.27881 1	31.2082 1.171	1004 0.442379	0.079926	0 3.9	7026 14.33086 22.	76208 5.185874	13.87175 10.5	364 10.76952	20.24164 17	/61.55 606.9182
45	1 14.81181 0.26511 1.652473 0.013736	3.631868 158.8104 17.62225	0 142.1621 5.8653	85 7.800824 38.9945.	1 5559.152	49.71016 1.314	56 0.03022 32.25137	5.657967 13.1359	9 10.76923	1.347527 106.581	64.86401 1	00.1168 0.888	8736 0.427198	0.173077	0 3.3	0989 10.62775 17.	02473 3.756868	9.980769 8.33	044 8.270604	13.78297 132	20.718 454.4396
40	1 14.30352 0.426686 1.966276 0.007331	3.856305 159.2302 19.2346	0 140.9531 5.5659	82 8.123167 47.9457	5 5505.774	49.94868 1.2448	68 0.039589 32.91056	5.841642 16.7008	8 11.1305	1.068915 107.9839	66.50587 1	09.8299 1.058	8651 0.475073	0.205279	0 3.5	0528 11.81672 18.	75513 3.237537	10.25367 8.67	886 7.64956	13.89736 143	\$7.748 484.4062
35	1 17.12478 0.390374 2.335116 0.016043	5.83779 190.2709 27.14973	0 168.4777 6.6791	44 9.481283 68.8449.	2 6642.617	60.31551 1.8360	07 1.228164 49.4082	7.14082 17.0873	4 13.75579	1.663102 130.8913	82.96078 1	41.4688 1.896	6613 0.752228	0.199643	0 4.29	4118 15.16399 23.	75045 4.657754	13.47237 11.2	203 13.66132	16.18538 186	619.2834
30	1 19.41498 0.649798 2.921053 0.012146 6	6.564777 208.4615 32.40688	0 179.4899 6.5121	46 10.75709 78.858.	3 6643.698	62.12955 3.5668	02 3.178138 71.17206	9.836032 18.5951	4 15.12753	2.635628 140.6802	93.75304 1	57.7429 1.637	7652 0.850202	0.242915	0 4.5	4291 16.94534 28.	84413 4.184211	16.48785 12.8	389 16.2996	15.41296 215	57.621 702.581

SAMPLE	Sr 70.82	Rb	Pb	Zn	Fe	Mn
	70.82					
4a	10.01	71.41	177.62	400.76	24922.02	762.55
4b	80.85	74.19	221.26	489.89	28117.29	849.7
5a	65.01	78.49	65.87	235.18	17857.47	591.98
5b	66.25	78.04	65.86	183.58	17507.35	641.65
23a	109.44	74.86	54.89	164.58	18596.54	666.18
23b	102.59	71.85	68.38	226.04	19197.68	783.69
24a	108.68	84.45	86.6	327.72	24903.32	838.78
24b	113.81	84.78	160.74	478.42	26497.6	911.58
25a	120.73	80.6	65.6	271.18	24013.7	1230.35
25b	108.35	78.8	69.57	274.04	22998.68	1070.6
AVG	94.653	77.747	103.639	305.139	22461.17	834.706

Surface Samples (nom)

Appendix 4	

 Appendix 4

 Handhed XF elemental counts of surface samples

 Surface samples

 Location is given in relative Rhine kilometers

 Model
 Exact sampling locations are in Appendix 3

 Meckar
 In the most right column are the calculated mean error percentages (in bold the percentages < 15 %)</td>

 Main
 Main

	Oherrhein																																						
SAMPLE	4a	4h	5a 5ł	n 93	a 9b	11	a 11	h 12	2a 17	2h 13	ta 13	h 142	a 14h	16/	16b	17a	17b	18a	18h	19a	19h	20a 20	0h 21	a 21)	h 22a	22h	23a	3h 2/	da 74ł	25a	25h	762	26h 27	a 27	h 28a	2.8	h 29a	29h	MEAN ERROR%
LOCATION	412	412	412	412	433	433	311	311	311	311	410	410	418	418	395	305	305	305	476 4	76 46	5 465	465	465	515	515	515	515 570	570	570	570 5	70 5	0 613	613	613	613	655	655	655 6	5
Ch.	146.95	120.77	144.55	05.35	112.07	91.76	70.95	90.94	09.45	66.79	101.9	109.47	05.22	84.3	04.12	129.09	138.09 1	22.17 12	0.06 130	155.2	2 112 22	112.02	126.02	147.10	146.09	133.99 10	2 1 1 74 39	126.17	124.22	105.54 139	45 125 1	4 110.90	99.04	139.42	124.76	05.56	80.00	97.56 0.9	12
Sh Error	24.08	25.15	75.08	25.27	22.05	25 41	77.76	27.16	37.07	27.64	25.05	25.24	35.95	25.04	26.29	25.42	76.5	26.09	4.94 24	75 76.1	3 36.37	24.7	25.04	25.16	26.00	25.27 2	5.01 75.46	24.01	25.02	26.15 2	1 25.0	5 25.52	37.65	25.01	75.97	24.56	27.20	26.11 26	11
SD EITOI	16 2077	17 00 29	17 2504	25.57	23.55	23.41	27.50	27.10	27.07	41 2006	25.55	23.24	23.63	23.54	20.30	23.43	20.3	1 174 17	9679 19 07	16 931	2 20.37	24.7	19.0454	17.0047 1	19 2002 3	23.57 2	20.40	19 2022	10 2046 7	4 7772 20.21	07 10 00	5 21 2962	21.05	23.51	10 1071 2	24.30	27.55	20.11 25.0	22 06020
%error	-10.3977	-17.9938	-17.3504	-20.0072	-21.1810	-31.27 -	34.2042 -	33.5972 -	-27.4962	-41.3890 -	-25.4912 -	23.2091 -2	27.1103 -3	0.8076	-28.028 -1	9.8548 -21	0.5458 -2	1.174 -175	5028 -18.93	10.821	2 -23.4776	-21.099	-18.9454 -	-17.0947 -1	18.3803 -2	0.0402 -25.1	280 -30.022	-18.2933	-19.3046 -2	4.7773 -20.31	92 -18.88	5 -21.2802	-31.4062 -	20.1744 -	19.1971 -2	5.7011	-33.819 -23	.8190 -25.28	23.90929
Sn	-94.09	-83.54	-86.08	-/5.3	-86.85	-78.28	-60.09	-60.88	-66.99	-66.9	-73.19	-97.71	-58.9	-61.12	-66.53	-75.78	-68.35	-65.75 -10	18.92 -84.	48 -84.1	5 -80.91	-11.21	-81.51	-104.46	-91.81	-86.76 -	80.5 -54.95	-99.36	-93.76	-/8.06 -112	26 -96	4 -90.06	-59.71	-/4./1	-81.81	-65.43	-71.06	52.86 -64.6	o/
Sn Error	20.98	21.98	21.87	21.89	20.67	21.81	23.61	23.45	23.45	23.73	22.45	21.66	22.39	22.41	22.81	22.09	23.09	22.71 2	1.44 21.	47 22.8	4 22.8	21.38	22.59	21.78	23.34	21.94 2	2.34 22.88	21.57	22.53	22.68 22	47 22.2	6 22.09	24.01	22.59	22.54	21.25	23.55	22.64 21.6	54
%error	-22.2978	-26.3107	-25.4066	-29.0704	-23.7997 -	27.8615 -	39.2911 -	38.5184 -	-35.0052	-35.4709 -	-30.6736 -	22.1676 -	38.0136 -3	6.6656 -3	4.2853 -2	9.1502 -	33.782 -34	.5399 -19.	6842 -25.41	43 -27.14	2 -28.1795	-27.6692	-27.7144 -	-20.8501 -2	25.4221 -2	5.2882 -27.7	516 -41.6379	-21.7089	-24.0294 -2	9.0546 -20.0	16 -23.09	3 -24.5281	-40.211 -	30.2369 -	27.5516 -3	32.4775	-33.141 -42	8301 -33.467	29.55719
Cd	-38.64	-28.85	-36.49	-30.55	-33.33	-27.99	-17.74	-27.46	-30.17	-19.24	-31.84	-30.99	-21.13	-26.05	-36.58	-35.96	-29.94 -	44.14 -3	7.22 -31.	86 -40.6	8 -37.31	-22.19	-34.04	-31.6	-33.53	-33.54 -3	0.81 -22	-34.85	-37.01	-32.42 -26	34 -28.2	9 -35.2	-22.83	-28.39	-29.09	-27.24	-23.26	25.57 -25.7	37
Cd Error	8.13	8.58	8.49	8.54	8.07	8.55	9.3	9.13	9.11	9.35	8.73	8.51	8.8	8.75	8.79	8.57	9	8.68	8.38 8.	39 8.	8 8.82	8.44	8.78	8.57	9.11	8.56	8.72 8.95	8.43	8.74	8.79	8.9 8.3	5 8.59	9.36	8.81	8.81	8.3	9.27	8.83 8.4	18
%error	-21.0404	-29.74	-23.2666	-27.9542	-24.2124 -	30.5466	52.4239 -	33.2484 -	-30.1956	-48.5967 -	-27.4183 -	27.4605 -4	41.6469 -3	3.5893 -2	4.0295 -	23.832 -3	0.0601 -19	.6647 -22.	5148 -26.3	34 -21.632	3 -23.6398	-38.0352	-25.7932 -	-27.1203 -2	27.1697 -2	5.5218 -28.3	025 -40.6818	-24.1894	-23.6152 -2	7.1129 -33.78	89 -30.929	7 -24.4034	-40.9987 -	31.0321 -	30.2853 -3	80.4699 -3	39.8538 -34	1.5327 -33.425	30.00735
Ag	-25.72	-16.5	-17.72	-22.72	-16.13	-16.34	-16.57	-16.65	-13.78	-13.95	-16.39	-19.97	-16.26	-12.96	-15.94	-27.17	-16.93 ·	20.06 -2	0.96 -17.	22 -23.4	3 -20.31	-16.1	-17.69	-21.08	-17.7	-21.41 -1	8.34 -10.88	-20.85	-19.46	-15.73 -16	68 -13.8	5 -21.28	-11.41	-18.49	-21.86	-10.14	-16.53	-14.34 -18.6	54
Ag Error	5.09	5.46	5.43	5.33	5.17	5.43	5.82	5.79	5.84	5.91	5.57	5.37	5.54	5.6	5.65	5.31	5.71	5.56	5.31 5.	34 5.5	5 5.6	5.32	5.59	5.39	5.8	5.39	5.52 5.73	5.33	5.56	5.63 5	63 5	6 5.42	5.99	5.56	5.51	5.36	5.84	5.62 5.2	33
%error	-19.79	-33.0909	-30.6433	-23.4595	-32.0521 -	33.2313 -	35.1237 -	34.7748 -	-42.3803	-42.3656 -	-33.9841 -	26.8903 -3	34.0713 -4	3.2099 -3	15.4454 -1	9.5436 -3	3.7271 -27	.7168 -25	.334 -31.01	05 -23.730	3 -27.5726	-33.0435	-31.5998 -	-25.5693 -3	32.7684 -2	5.1752 -30.0	981 -52.6654	-25.5635	-28.5714 -3	5.7915 -33.7	53 -40.433	2 -25.4699	-52.4978 -	30.0703 -:	25.2059	-52.86 -3	35.3297 -39	3.1911 -28.59/	4 32.69997
Sr	70.82	80.85	65.01	66.25	83.93	90.8	134.55	123.9	110.19	110.81	115.87	121.98	119.32	118.81	162.99	164.12	175.52	209.3 11	5.42 99.	32 173.1	3 163.62	153.58	168.79	151.8	163.04	167.94 18	5.97 109.44	102.59	108.68	113.81 120	73 108.3	5 103.35	107.08	114.2	118.79	119.24	125.18	92.64 96.	9
Sr Error	3.46	3.79	3.47	3.48	3.63	3.94	4.96	4.76	4.54	4.6	4.48	4.46	4.5	4.49	5.25	5.14	5.51	5.87	4.33 4.	04 5.4	5 5.3	4.83	5.32	4.95	5.43	5.19	5.49 4.41	4.13	4.39	4.47 4	61 4.3	4 4.22	4.58	4.47	4.55	4.28	4.85	4.09 3/	Sr Sr
%error	4 885626	4 687693	5 33764	5 25283	4 325033 4	339207 3	686362 3	841808 4	1 1 20156	4 15125 3	8 866402 3	656337 3	771371 3	779143 3	221057 3 1	31855 3.1	39243 2.8	14587 3 75	1516 4.067	56 3 14792	1 3 2 3 9 2 1 3	3 144941	3 151845	3 26087 3	330471 3 0	090389 2 952	089 4 029605	4 025734	4 039382 3	27599 3.8184	38 4 00553	8 4 083212	4 277176 3	914186 3	830289	3 5894 3	874421 4	41494 4 141	3,835866
Rb	71.41	74 19	78.49	78.04	71.62	69.13	63.02	62.19	68.92	65.15	67.65	65.49	57.7	59.49	56.81	60.32	62.54	50.46 7	2 68 62	38 75 5	3 63.74	69.89	76.82	71.49	66.13	69.1 6	2 38 74 86	71.85	84.45	84.78 8	16 78	8 79.58	82.96	82.96	81.64	62.24	64.85	65.6 61	7
Ph Error	2 5 5	3.75	2.02	2.0	2.49	2.6	2.60	2 65	2 92	2 77	2 66	2 6 2	2.4	2.44	2.44	2.45	2.65	2 70	2.66	4 20	1 2.65	2 5 5	2.01	2.7	2.9	2.65	2 5 4 2 96	2.65	4.07	4.07	4 20	1 2.90	4 32	4.02		2.24	2 77	2.62 2.	ph ph
NO EITOI	4 071 202	5.73	3.02	3.0	3.40	3.0 5 30759 E	0000000	960111 6	3.04	5.77	5.00 E 4103 E	3.32	007EA0 E	3.44 707404 6	3.44	3.4J	3.03	3.20	5.00 : 5772 E 4E04	5.9	* 3.03 7 E 736300	5.55	5.51	3.7 175540 E	3.0	5.03	3.34 3.00	5.03	4.07	4.07	4 3.: 70 4 0610	0 4 999162	4.23	945700 4	900EE0 E 3	3.34	012416 EE	3.02 3.3 19303 E 4906	27 5 24929
Db	4.5/1255	221.26	4.800802 4	65 96	4.838578 .	AE 75	20	20.04	42 72	3.780040	39 39	40.10	44.9E	65 34 U.	12 72 3.7	12 54	46.10	17.42	3773 3.4304	05 5.2104	5.720388	3.075411	75 46	75.9	95 72	5.2822 5.074	7 00 54 90	5.080028	4.01542 4.	160.74 6	15 4.50152	7 100.60	171 11	.043705 4. 94.01	122.49	49.41	515410 3.5	25 59 26	3.34636
FD F	177.02	221.20	03.87	03.80	30.5	40.75		50.54	42.72	55.01	30.20	45.15	44.03	03.24	12.72	15.34	40.15	17.45 4		50 80.5	5 80.50	43.81	73.40	73.8	03.75	04.10 4	7.05 34.85	08.58	80.0	100.74 0		100.05	1/1.11	84.01	152.40	40.41	32.04	55.08 50.3	
PD Error	11.05	12.68	7.71	1.1	6.1	6.81	6.94	6.44	7.06	6.74	6.57	6.99	6.85	7.8	5.15	5.03	/.1/	5.48	6.79 7.	05 8.8	/ 8.64	6.68	8.32	8.15	9.05	7.68	7.03 7.48	1.14	8.82	11.3 /	96 8.0	9.18	12.17	8.65	10.4	6.68	7.69	6.48 b./	PD PD
%error	6.221146	5.730814	11./048/ 1	11.6914/ 1	15.68123 14	1.56684 1	.7.79487 2	0.81448 1	16.52622 1	19.25164 1	1/.16301 1	4.21021 15	5.2/313 11	1.95586 40	1.48/42 3/	.14919 15.	.52284 31.4	14005 14.	4039 13.311	93 10.2709	5 10.72493	14.58197	11.025/1 1	10.75198 1	10.5564 11	1.97007 14.92	2886 13.62725	11.3191	10.18476 7.	029986 12.134	15 11.513	8 9.11/092	7.112384 1	0.29639 7.	.850242 1	13.7988 14	1.60866 18.	16143 17.1459	19 14.51457
Se	-0.42	2.31	1.65	2.48	-0.21	0.69	2.87	1.73	0.82	1.09	0.52	3.77	0.47	1.49	0.71	-1.02	1.14	1.21	1.1 3.	44 -0.5	8 1.06	3.13	-0.35	1.09	-0.07	0.99	2.21 2.04	1.29	4.08	2.24 2	23 1.0	6 3.54	0.76	0.96	1.98	0.72	3.28	1.76 2.3	57
Se Error	2.13	2.47	2.29	2.35	2	2.18	2.54	2.43	2.37	2.42	2.23	2.42	2.22	2.32	2.26	2.05	2.35	2.3	2.2 2.	36 2.2	5 2.36	2.33	2.22	2.26	2.35	2.26	2.38 2.39	2.25	2.57	2.51 2	42 2.3	4 2.49	2.54	2.32	2.44	2.12	2.58	2.32 2.7	27
%error	-507.143	106.9264	138.7879 9	94.75806	-952.381	315.942 8	8.50174 1	40.4624 2	289.0244 2	222.0183 4	128.8462 6	4.19098 47	72.3404 15	5.7047 31	.8.3099 -	200.98 20	6.1404 190	.0826	200 68.604	65 -387.93	1 222.6415	74.44089	-634.286 2	207.3394 -	3357.14 22	8.2828 107.6	6923 117.1569	174.4186	62.9902 11	2.0536 108.52	02 140.963	9 70.33898	334.2105 2	41.6667 1	23.2323 29	94.4444 78	3.65854 13:	8182 95.7805	59 296.837
As	22.78	14.64	13.24	10.57	11.38	7.09	4.5	10.55	9.13	11.44	11.53	12.67	6.05	9.34	8.56	11.21	6.43	2.57 1	.0.45 13.	64 12.5	5 19.06	11.66	9.22	13.59	17.1	20.24 1	5.98 6.19	10.44	15.12	18.2 5	09 9.2	5 13.37	20.13	5.63	8.57	6.39	9.25	10.07 8.5	89
As Error	7.84	8.73	5.53	5.44	4.46	4.77	4.77	4.71	5.04	4.95	4.81	5.06	4.77	5.48	3.84	3.88	4.99	3.73	4.87 5.	12 6.2	8 6.32	4.83	5.82	5.82	6.55	5.75	5.23 5.18	5.47	6.29	7.94 5	45 5.6	2 6.46	8.58	5.91	7.12	4.65	5.43	4.69 4./	18
%error	34.41615	59.63115	41.76737 5	51.46641	39.19156 6	7.27786	106 4	4.64455 5	55.20263 4	43.26923 4	1.71726 3	9.93686 78	3.84298 58	8.67238 44	.85981 34	.61195 77.	.60498 145	.1362 46.6	0287 37.536	50.0398	4 33.15845	41.42367 0	63.12364 4	12.82561 38	8.30409 28	8.40909 32.72	841 83.68336	52.39464 4	41.60053 43	.62637 107.07	27 60.7567	6 48.31713	42.62295 1	04.9734 8	3.08051 72	2.76995 5	58.7027 46.	57398 50.397	56.54691
Hg	1.62	3.35	4.28	2.18	0.06	-0.2	0.7	-1.01	4.44	3.12	2.12	3.5	4.35	1.82	-1.3	0.98	-2.77	3 .	0.47 0.	45 3.9	9 0.72	3.12	-0.1	-0.71	3.34	3.9 -	0.36 -1.26	4.74	-0.28	2.17 0	12 2.4	4 3.46	4.34	0.83	1.43	0.83	1.66	2.35 -1.2	85
Hg Error	3.01	3.28	3.25	3.13	2.82	2.98	3.3	3.16	3.49	3.47	3.19	3.18	3.3	3.17	3.05	3.06	3	3.27	2.93 2.	95 3.4	2 3.21	3.12	3.13	2.98	3.48	3.24	3.06 3.05	3.24	3.14	3.34 3	16 3.2	4 3.28	3.65	3.18	3.24	2.93	3.32	3.19 2.1	35
%error	185.8025	97.91045	75.93458	143.578	4700	-1490 4	71.4286 -	312.871	78.6036 1	111.2179 1	150.4717 9	0.85714 75	5.86207 17	4.1758 -2	34.615 31	2.2449 -1	08.303	109 -623	404 655.55	56 85.7142	9 445.8333	100	-3130 -	419.718 10	04.1916 83	8.07692	-850 -242.063	68.35443	-1121.43 15	3.9171 2633.3	33 132.786	9 94,79769	84.10138 3	83.1325 2	26.5734 3	353.012	200 135	5.7447 -211.1	1 510.9697
Zn	400.76	489.89	235.18	183.58	157.89	222.75	81.64	73.73	113.65	141.33	149.57	154.55	167.07	174.67	37.63	41.97	111.65	34.45 15	3.98	95 219.9	7 187.43	151.27	214.07	184.1	215.97	119.86 8	3.34 164.58	226.04	327.72	478.42 271	18 274.0	4 350.83	452.07	279.47	384.48	141.26	152.91 1	14.55 112/	36
Zn Error	20.15	22.88	16.74	15 21	13.6	16.26	12.68	12.25	13.87	15.01	14 53	14.79	14 91	15.18	10.24	10.08	13.46	9.92 1	4.18	12 17.1	1 16.02	13.9	16.7	15 36	17 37	13.74 1	2 07 15 19	16 38	19.79	23.2 18	44 18 3	4 19.98	23.81	18 49	21.1	13 33	15.21	13.21 12	2 Zn
%error	5 027947	4 670436	7 117052 8	2 285216	8 613597 7	200663	15 5316 1	6 61468 1	12 20414 1	10.62053 9	714515 0	246100 8	974403 8	690674 23	7 21 233 24	01716 12	05553 28	79536 9 20	8088 17 631	58 7 77833	8 547101	9 188868	7 801187 8	343707 8	042784 11	04622 14.48	284 9 229554	7 246505	5.038697 4	249796 6 7990	11 6 65596	3 5 695066	5 266883 6	616095 5	487937	9.4365 9	947078 11	53208 11.1	10 18325
Cu	46.73	60.98	36.62	23.03	35.71	46.65	34.01	79.79	36.03	31.76	62.78	61.3	43.91	51.58	30.76	15.25	41.45	27.5	4.76 3/	1 74	1 56.83	49.72	70.4	56.47	67.85	35.16 3	7 56 75 78	33.14	41.71	50.12 //7	79 53	6 55.25	53.87	39.75	58.4	32.68	18.42	21.44 26	26
CuError	17.41	12.60	17.2	11.65	11 51	12 71	12.2	12.02	12 22	12.76	12.00	12.42	12.06	12.2	13.62	11.24	12.70	13.24	17.6 11	14.9	1 12.05	12 72	14.49	12.47	14.00	12.42 1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	17.12	12.7	12.7 1	12 12 12 12 1	0 125	14 66	12.02	12.05	11 6 4	13.19	11.71 11	
e cu cirior	76 55 697	13.05	22 5 6 6 7 5	11.03	11.31	7 74544 2	13.3	2 40292 2	13.33	41 75052 3	13.03	100000 00	12.50	13.3	12.03	26066 2	13.20	12.34	12.0 11.	72 14.0	* 13.90	75 50277	14.40	13.47	2 00 295 25	12.42 1	2.77 12.27	26 60220 3	15.2	7 2244 20 45	0.0 15	1 74 42420	14.00	2 17107 2	2 00411 25	11.04	12.10	617EA A2 920	22 8440
/serror	20.33082	22.44998	35.3662	15 17	32.23187 2.	24344 3	5.10013 4	3.40383 3	50.99093	41.73003 2	20.75	1.89233 2:	7.31492 23	52.07		.30000 3.	2.0380 44.	57275 20.1	3013 34.930	20.0209	3 24.30449	23.38327	20.30818 2	01.40	2.09283 33	5.32423 33.95	48.33039	50.00225	17.05	13 53 20.437	34 23.3734	1 24.43439	27.21300 3	5.1/15/ 2.	3.50411 33	0.01812 00	J.12378 34.	31734 43.8303	33.0449
NI I	01.41	37.71	25.75	45.47	22.42	27.05	60.77	45.27	67.52	42.30	30.75	31./3	/0.15	53.07	41.43	30.9	18.12	44.90 0	0.85 46.	53 34.0	9 22.43	32.58	35.49	81.49	40.48	00.08 4	8.80 35.07	04.15	47.05	42.53 88	31 00	5 35.05	35.73	50.45	44.55	10.10	15.71	20.56 24.8	55
Ni Error	27.08	28.23	25.97	26.54	23.91	25.54	29.28	28.68	29.71	28.97	26.5	26.17	27.55	26.96	2/	26.35	26.41	26.58	26.9 25.	/6 27.6	5 26.76	25.32	27.45	28.46	28.68	27.23 2	7.07 27.37	27.57	29.15	28.89 30	13 28.9	3 28.03	30.33	29.12	29.07	24.06	26.72	25.74 24.9	34
%error	44.09705	74.86078	100.8544 5	58.36815	106.6459 94	4.41774 4	8.18167 6	3.35321 4	44.00178 6	68.38999 8	36.17886 8	2.47715 36	5.17859 50	0.80083 65	5.17017 71	.40921 14	5.7506 59.:	11922 44.2	0707 55.362	13 81.0501	5 119.3045	77.71639	77.34573 3	34.92453 7	70.8498 44	1.87475 55.40	0319 78.04391	42.9774 (51.17524 67	.92852 34.118	45 43.4384	4 78.62553	84.88665 5	1.58547 6	5.25253 14	8.8861 17	70.0827 125	.1946 100.44	3 74.14124
Co	68.39	223.69	84.45	29.86	82.65	87.4	54.5	139.08	114.84	130.86	72.7	176.67	-41.13	22.84	53.44	137.12	121.63	34.82 4	19.36 50.	28 96.6	9 101.65	68.36	132.09	123.55	160.33	64.71 5	7.61 64	100.94	226.85	142.52 35	78 101.3	1 249.43	160.27	197.18	254.05	92.72	73.54	77.52 83.6	59
Co Error	106.44	118.99	94.08	92.05	77.53	84.18	95.94	96.23	98.31	97.97	90.06	86.97	77.71	82.33	81.69	82.04	79.72	68.88 8	19.09 80.	21 96.5	1 90.4	83.74	95.16	90.65	94.64	85.23 8	4.24 98.58	96.88	115.28	117.39 111	24 108.4	7 111.14	126.08	110.5	115.11	75.49	84.99	82.4 79.?	89
%error	155.6368	53.19415	111.4032 3	308.2719	93.8052 9	5.31579 1	76.0367 6	9.19039 8	35.60606 7	74.86627	123.879 4	9.22737 -1	188.938 36	60.4641 1	52.863 59	.83081 65.	.54304 197	.8173 180.	4903 159.52	67 99.8138	4 88.93261	122.4985	72.04179	73.3711 59	9.02825 13	31.7107 146.2	246 154.0313	95.97781	50.81772 82	.36739 310.89	99 106.646	3 44.55759	78.66725 5	6.04017 4	5.30998 81	1.41717 11	15.5698 100	.2951 94.861	99 118.5711
Fe	24922.02	28117.29	17857.47 1	17507.35	13209.57 14	4174.58 1	6601.45 1	6351.25 1	17245.48 1	16608.46 1	15578.21 1	4626.23 12	2249.27 13	385.82 1	2463.3 12	709.89 11	011.39 87	45.63 1645	2.15 13313.	53 17134.8	8 14923.18	14769.63	16851.41 1	16016.21 15	5247.48 14	351.13 136	81.2 18596.54	19197.68	24903.32 2	6497.6 2401	8.7 22998.6	8 23742.51	27750.67 2	3052.74 2	4777.59 11	1910.16 12	2433.61 123	71.07 12836.7	87
Fe Error	270.4	297.87	236.94	233.91	193.76	210.62	242.41	239.48	246.14	244.29	226.53	214.05	199.5	208.41	205.1	202.25	195.91 1	.71.97 22	5.31 201.	91 242.2	4 225.83	210.53	237.34	226.09	233.94	214.23 21	1.84 249.37	243.89	287.48	296.02 283	86 274.2	4 276.02	317.69	275.88	286.09	187.55	212.42	.06.01 198.7	22 Fe
%error	1.084984	1.059384	1.32684 1	1.336067 1	1.466815 1.	485899 1	.460174 1	.464598 1	1.427273 1	1.470877 1	1.454147 1	.463467 1.	628668 1.	556946 1.	645632 1	.59128 1.7	79158 1.9	56353 1.36	9487 1.5165	56 1.41372	5 1.513283	1.425425 :	1.408428 1	.411632 1.	534286 1.4	492774 1.548	402 1.340948	1.270414 :	1.154384 1.	17158 1.1820	75 1.19241	6 1.162556	1.144801 1	.196734 1.	154632 1.5	574706 1.	708434 1.6	13099 1.54426	1.420456
Mn	762.55	849.7	591.98	641.65	479.38	550.84	464.38	503.29	603.92	527.38	494.86	500.5	405.32	400.53	307.83	295.39	208.65 1	82.33 49	3.14 462.	91 449.7	3 438.07	459.41	516.38	522.99	367.34	384.29 43	1.88 666.18	783.69	838.78	911.58 1230	35 1070	6 924.59	957.34	824.26	873.81	426.31	450.55	53.11 522.1	18
Mn Error	78.05	85.37	72.49	73.98	62.75	68.88	71.34	72.53	76.98	74,74	69.29	67.44	63.77	64.46	60.8	58.78	55.77	52.48 E	7.96 64	.5 70.1	5 68.26	64.65	71.3	69.43	67.18	63.67 6	5.82 77.63	78.65	85.96	88.65 9	.4 91.2	6 86.57	94.78	84.64	86.57	61.41	69.34	70.16 66.	71 Mn
%error	10.23539	10.04708	12.24535 1	11.52965 1	13.08982 1	2,50454 1	5.36242 1	4.41117 1	12.74672 1	14.17194 1	4.00194 1	3.47453 15	5.73325 16	09368 19	0.75116 19	89912 26	72897 28.	78298 13.7	8108 13.933	59 15.5982	5 15,58198	14.0724	13.80766 1	13.27559 18	8.28823 16	5.56822 15.24	034 11.65301	10.03586	10.24822 9.	24873 7.9164	47 8.52419	2 9.363069	9,900349	10.2686 9.	907188 14	40501 15	5.39008 12.	68464 12.775	13.8989
Cr	42,61	123,47	87.86	109.3	63.56	32.61	56.87	74.73	92.18	108.85	52.16	64.39	70.46	114.98	63.33	50.22	10.78	55.89 15	1.66 54	37 121.8	7 82.15	85.48	47.54	46.58	83.34	108.5 5	8.59 58.95	37.1	118.49	95.17 52	77 58.0	1 92.94	61.36	135.94	61.62	71.05	54.33	-1.17 83/	11
Cr Error	60.6	69.05	67.13	63.04	55 27	56.87	64.06	64.6	66.74	67.73	60.78	59.02	59.34	62.57	60.31	57.83	56.9	57 58 6	4 73 56	83 66.7	3 63 15	59.17	61.44	50 10	65.19	62.01 5	9 75 63 11	59.45	69.79	68.95 6	7 64	7 66.12	71.76	69.15	66.04	56.25	61.73	55.52 58	12
er ciror	142 2201	SE 04717	70 71 477 5	7 67613	96 05721 1	74 2044 1	12 6420 8	C 44452 7	71 950.41 6	67.75	115 5675	01 6602	94 319 54	11916 05	22122 11	E 1E22 E2	7 9 20 2 10 2	0728 47.2	E121 104 E2	46 64 7550	7 76 07150	60 22087	120 2295 1	127 0717 79	9 22174 57	15207 1010	107.0559	160 2426	EQ 477E1 7	2 4402 124 50	76 111.13	6 71 14367	116 1242 6	0 96 90 2	107 172 7	20 1606 11	12 6205	745 2 70 204	212 212 2002
ACTION -	142.2201		10.71477 3		00.33721 1.	4.3344 1	AL.0423 8	w.44435 /.	1.03341 0	VE.22324 1	49.3075	Ja.0002	V-210 34	.+1010 95		9.4333 32			104.32	-0 34.7350	10.0/108	0.22001	1.2303 1	1.0/1/ /8	0.221/4 5/		107.0308	100.2420	-4//31 /			11.1420/	**0.1343° D	v.v0005	107.173 7	5.1050 11	-3-3203 ···	·····3 /0.3044	£12./072

Appendix 3 Exact coring and sampling locations

Name	Date	e Position	N dd	E dd Altitudo	Boring	Kernen	Lossa monstars	Opmerking
Name	Date	e Posición	Nuu	L'uu Annuue	voor horing: zie hoorstaat	Kernen		Opmerking
1	1 24	4-10-11 1·54 PM N49 48 24 5 F6 44 26 9	49 8068	6 74079 123 m	zie loc 2			Zelfde als 2
2	2 2	4-10-11 1:54 PM N49 48 24 5 E6 44 26 9	49.8068	6 74079 125 m	horing			Palaeo restgeul van Moezel: Geen kern genomen vanwege veel
-			1510000	0.71075 121111	501115			inspoelingsmateriaal (bontzandsteen) vanaf nabijgelegen helling
3	3 24	4-10-11 4:50 PM N49 48 26.3 F6 43 55.8	49,8073	6.73217 117 m	boring	KENN1 (0	- KENN 5 (1.1-1.2 m): KENN6 (1.2-1.3 m): KENN7 (1.4-1.5	Palaeo restgeul van Moezel: Losse monsters KENN5 - 12 zijn genomen omdat het
					8	0.6 m):	m): KENN8 (1.5-1.6 m): KENN9 (1.6-1.7 m): KENN10 (1.7-	door de hardheid van het bodemmateriaal niet mogelijk was de brede guts meer
						KFNN2-3-	1.8 m): KENN11 (1.9-2.0 m): KENN12 (2.0 -2.2 m)	dan ca. 10 cm de bodem in te krijgen. KENN12 en KENN13 zijn met de smalle guts
						4:		bemonsterd.
						KENN13		
4	4 24	4-10-11 5:15 PM N49 48 45.8 E6 44 27.3	49.81272	6.7409 120 m			KENN levee 1 (0.1-0.2 m): KENN levee 2 (0.2-0.3 m)	Oeverafzettingen in rietveld nabij oever van Moezel: alleen opp. Monster
5	5 24	4-10-11 5:34 PM N49 48 47.4 E6 44 11.1	49.81316	6.7364 121 m			KENN pointbar 1 (0.1-0.2 m); KENN pointbar 2 (0.2-0.3	Pointbarafzettingen op iets grotere afstand van de Moezel dan loc. 4; alleen opp.
							m)	Monsters
e	5 25-	-10-11 11:51 AM N50 03 34.2 E8 57 22.6	50.05951	8.95627 109 m	boring		,	Palaeo restgeul van de Main: Monstername afgebroken op bevel van boswachter
								(geen vergunning om in Naturschtutzgebiet te boren)
7	7 25	-10-11 12:43 PM N50 03 43.4 E8 57 33.9	50.06204	8.95941 104 m	boring			Palaeo restgeul van de Main; Geen kern gestoken omdat de restgeulopvulling
								vrijwel uit niet-klastisch materiaal bestond (veen en gyttja)
								,
8	8 2	5-10-11 3:28 PM N50 04 32.1 E8 57 33.6	50.07557	8.95932 103 m	boring	KK1 (1.2-		Palaeo restgeul van de Main bij Klein Krotzenburg;
						2.2 m);		
						KK1 (2.2-		
						3.2 m)		
9	9 2!	5-10-11 3:56 PM N50 04 41.3 E8 58 33.3	50.07813	8.97593 99 m			KK2 (0.1-0.2 m); KK2 (0.2-0.3 m)	Oeverafzetting van de Main bij Klein Krotzenburg; ca 30 m vanaf oever
10	0 26-	-10-11 11:43 AM N49 03 45.0 E9 09 10.5	49.06251	9.15291 161 m	boring	Lauffen I		Palaeo restgeul (Holoceen) van de Neckar
						(1.0-1.9		
						m)		
11	1 20	6-10-11 1:57 PM N49 05 44.4 E9 09 27.8	49.09566	9.15772 163 m			Neckar floodplain hoog (0.1-0.2 m) (0.2-0.3 m)	hooggelegen recente overbank/floodplain afzettingen langs de Neckar nabij
								Horkheim
12	2 20	6-10-11 2:05 PM N49 05 43.4 E9 09 36.4	49.09538	9.16011 160 m			Neckar floodplain laag (0.1-0.2 m) (0.2-0.3 m)	laaggelegen recente overbank/floodplain afzettingen (geul langs de Neckar nabij
								Horkheim; In de Geul grondwaterputten (t.b.v. oeverinfiltratie?)
13	3 20	6-10-11 4:53 PM N49 28 15.4 E8 35 54.7	49.47095	8.59852 93 m			Edingen (0.1-0.2 m) (0.2-0.3 m)	overbank afzettingen ca. 15 m vanaf oever Neckar bij Neckarhausen (naam
								Edingen zou eigenlijk Neckarhausen moeten zijn)
14	4 20	6-10-11 5:31 PM N49 28 36.7 E8 32 45.0	49.47685	8.54582 90 m			Mannheim (0.1-0.2 m) (0.2-0.3 m)	floodplainafzetting van de Neckar bij Mannheim. Floodplain is hooggelegen (ca.4-5
								m) boven waterniveau van Neckar/ rivier ligt diep t.o.v. floodplain
15	5 27.	-10-11 10:55 AM N/0 15 /0 0 E8 22 12 2	10 2626	8 28674 90 m	boring	Römerher		Palaeo restreul van Oberrhein hij Mechtersheim/Pömerherg
1.	5 27-	-10-11 10.55 AW W49 15 49.0 18 25 12.2	45.2050	8.38074 50 11	bornig	a1 (1 A.		ralaeo restgeur van obermein bij wechtersnein/Komerberg
						2.4 m)		
						(2.4-3.1		
						m)		
16	5 27.	-10-11 12:24 PM N49 15 29.1 E8 25 33.5	49.2581	8.42596 98 m		,	Römerberg2 (0.1-0.2 m) (0.2-0.3 m)	recente floodplainafzetting langs de Oberrhein; relatief hooggelegen en
							,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	zandig/zavelig sediment
17	7 27.	-10-11 12:28 PM N49 15 29.3 E8 25 35.3	49.25814	8.42648 97 m			Römerberg3 (0.1-0.2 m) (0.2-0.3 m)	recente floodplainafzetting langs de Oberrhein; relatief laaggelegen en kleiig
								sediment uit moerasbosje langs waterkant
18	8 2	7-10-11 3:04 PM N50 03 45.0 E8 31 11.6	50.06251	8.5199 85 m	boring	Sindlingen	Sindlingen1 (0.1-0.2 m) (0.2-0.3 m)	Oude geul langs huidige loop Main op ca. 70 m van oever. Op ca. 80 cm -mv
						(1.2-1.8)		humeus materiaal ruikt olie-achtig (zie boorstaat). Op ca. 1 m -mv grindlaag
								(gestort of fluviatiel afgezet?)
19	9 28	8-10-11 9:28 AM N49 42 11.2 E8 21 58.6	49.70311	8.36628 85 m			Rheindürkheim1 (0.1-0.2 m) (0.2-0.3 m)	laagte op floodplain tussen levee en kade/terrasrand
20	28	8-10-11 9:32 AM N49 42 12.3 E8 22 04.1	49.70342	8.3678 86 m			Rheindürkheim2 (0.1-0.2 m) (0.2-0.3 m)	levee
21	1 28-	-10-11 10:57 AM N49 59 48.0 E8 01 46.6	49.99667	8.02961 75 m			Ingelheim1 (0.1-0.2 m) (0.2-0.3 m)	net over levee
22	2 28-	-10-11 11:05 AM N49 59 39.5 E8 01 31.2	49.99429	8.02532 76 m			Ingelheim2 (0.1-0.2 m) (0.2-0.3 m)	zandiger sediment da Ingelheim1
23	3 28-	-10-11 12:35 PM N50 16 47.6 E7 27 34.4	50.2799	7.45955 64 m			Alken1 (0.1-0.2 m) (0.2-0.3 m)	Smalle strook floodplain langs Moezel
24	4 28-	-10-11 12:40 PM N50 16 57.2 E7 27 29.3	50.28256	7.45814 63 m			Alken2 (0.1-0.2 m) (0.2-0.3 m)	Smalle strook floodplain langs Moezel
							Alken3 (0.1-0.2 m) (0.2-0.3 m)	Smalle strook floodplain langs Moezel; op ca 10 m van oever; maaiveld ca. 3 m dan
25	5 28-	-10-11 12:43 PM N50 16 58.0 E7 27 28.6	50.28279	7.45796 63 m				waterpeil Moezel
26	5 28	8-10-11 1:35 PM N50 26 18.6 E7 26 23.1	50.4385	7.43974 56 m			Andernach1 (0.1-0.2 m) (0.2-0.3 m)	Locatie aan het einde van smalle floodplain langs Rijn
27	7 28	8-10-11 1:41 PM N50 26 10.4 E7 26 31.6	50.43623	7.44211 55 m			Andernach2 (0.1-0.2 m) (0.2-0.3 m)	Laagte (ca. 20 cm lager dan omgeving) midden in smaale strook floodplain
28	8 28	8-10-11 4:10 PM N50 46 10.6 E7 03 52.8	50.76962	7.06468 43 m			Bonn1 (0.1-0.2 m) (0.2-0.3 m)	Levee ca. 5 m boven waterpeil Rijn
							Bonn2 (0.1-0.2 m) (0.2-0.3 m)	Hoger gelegen distaler deel van floodplain halfweg tussen oever en dijk. Op 0.2-0.3
29	9 28	8-10-11 4:14 PM N50 46 09.2 E7 03 46.7	50.76923	7.06297 44 m				m duideljik zandiger sediment dan toplaag.

Bienen cores: Bienen III - Bi	Norma ienen >	lized count	of selected	elements (w	rith plots)									Bie	nen III - Bien	en X Denth												
167	1 ⁶	Si	K	Ca	Ti 9.65E-05	Mn	Fe I	Rb	Sr 0.037866	Zr 0.05685	Pb 2	Zn 0.002519	AI	Dej	545	531	Si 0.00561	K 0.043011	Ca	Ti I	Mn F	e F	Rb :	5r 0.042437	Zr 0.053026	Pb 2	n 0.011695	0.000255
169	15	8 0.0001	9 0.000162	0.000377	0.000118	0.000227	0.016086	0.024825	0.040478	0.056524	0.005921	0.00304	0.000207		547	533 536	0.007632	0.064257	0.174596	0.054039	0.052594	2.233237	0.040293	0.046927	0.047909	0.004049	0.013599	0.000318
173	16	3 0.00173	9 0.01953	0.095571	0.018292	0.014941	0.907153	0.028881	0.042798	0.046441	0.003744	0.00703	0.000306		551	538 541	0.006134	0.054663	0.188576	0.047078	0.066209	2.273866	0.038002	0.048936	0.04542	0.003393	0.011308	0.000328
177	16	8 0.00373	1 0.046066	0.175555	0.039656	0.031966	1.81788	0.033951	0.044993	0.044753	0.005684	0.012931	0.000227		555	543 545	0.006766	0.061512	0.191038	0.052218	0.075028	2.443062	0.039924	0.046363	0.041395	0.003418	0.011853	0.000456
181	17	2 0.00452	6 0.049414	0.188828	0.043467	0.033969	1.9022	0.036476	0.047638	0.045841	0.004854	0.012975	0.000213		559	548	0.006491	0.058994	0.212446	0.048677	0.056067	2.277952	0.037761	0.048104	0.041657	0.003142	0.011069	0.000274
185	17	7 0.00530	8 0.05230: 4 0.04847/	0.170615	0.048053	0.033274	1.922396	0.038339	0.045263	0.050971	0.006139	0.014089	0.000291		563	552	0.006767	0.061137	0.227967	0.050904	0.063054	2.395824	0.037883	0.049201	0.042675	0.003922	0.011504	0.000445
189	18	1 0.00448	1 0.05238	0.111691	0.04718	0.047325	2.247678	0.040034	0.041051	0.045513	0.005315	0.01385	0.000266		567	557	0.006903	0.061741	0.182971	0.053493	0.046095	2.291696	0.039626	0.048064	0.045442	0.003889	0.011856	0.000488
193	18	6 0.00461	3 0.053019	0.176571	0.044828	0.059097	2.281702	0.036783	0.046712	0.044997	0.005718	0.014795	0.000279		571	562	0.007268	0.059347	0.256994	0.051638	0.061136	2.101957	0.036905	0.055929	0.048645	0.003894	0.010754	0.000379
197	19	1 0.00553	7 0.0532	0.167231	0.048277	0.043161	2.040737	0.037092	0.04638	0.050663	0.004914	0.013645	0.000291		575	567 569	0.007384	0.061064	0.193259	0.056743	0.054636	2.104424	0.038506	0.047992	0.056233	0.003551	0.011557	0.000432
201	19	5 0.00574	2 0.05372	0.168881	0.047624	0.033927	1.951515	0.038001	0.045896	0.049416	0.004995	0.014074	0.000339		579	571	0.006224	0.059596	0.182018	0.050831	0.099746	2.422016	0.039546	0.045916	0.043707	0.003347	0.012072	0.000373
205	20	0 0.0054	8 0.05094	0.108336	0.048422	0.038029	2.084441	0.037641	0.04	0.050056	0.00528	0.013255	0.00037		583	576	0.007642	0.062227	0.201092	0.053204	0.06999	2.354352	0.039629	0.048922	0.044516	0.004036	0.011756	0.00043
209	20	4 0.00452	5 0.04749	0.186099	0.039646	0.031782	1.860552	0.037649	0.047605	0.043078	0.003844	0.011299	0.000256		587	581	0.006193	0.060771	0.182191	0.052395	0.061579	2.447283	0.040188	0.04871	0.043458	0.003203	0.011716	0.000439
213 215	20	9 0.00546	1 0.05151	0.142689	0.046057	0.033044	2.113249	0.038003	0.044749	0.044918	0.004578	0.014072	0.000317		591 593	586 588	0.006703	0.060991	0.111638	0.056042	0.055358	2.407531	0.041398	0.042662	0.046735	0.003928	0.012488	0.000351
217	21	4 0.0041	4 0.05122	0.125102	0.045294	0.056975	2.377886	0.036936	0.041929	0.041727	0.004286	0.012452	0.000285		595 597	590 593	0.006594	0.06168	0.164817	0.052745	0.067251	2.525628	0.040432	0.04565	0.044275	0.002995	0.011025	0.000524
221 223	21	8 0.00513	7 0.05193 3 0.05026	0.179028	0.043842	0.034098	1.973985	0.036523	0.046306	0.0481	0.004737	0.013037	0.000287		599 601	595 598	0.006308	0.059309	0.234784	0.048904	0.080826	2.517826	0.038725	0.052554	0.043861	0.002998	0.010688	0.000386
225 227	22	3 0.00489 5 0.00479	7 0.052469 9 0.05168	0.170863	0.045759	0.0357 0.035971	1.978362 2.023383	0.03771	0.045659 0.043921	0.048869 0.04496	0.004655 0.004472	0.012702 0.012942	0.000237		603 605	600 602	0.006931 0.007133	0.060587	0.192996 0.190636	0.050928 0.053516	0.063008	2.235072 2.332177	0.039141 0.040744	0.049238 0.04775	0.045801 0.044849	0.003307	0.011403	0.000399
229 231	22	7 0.00418 0 0.00415	3 0.05220	0.138605	0.043404	0.028039	2.042378	0.038735	0.042229	0.044235	0.004324	0.011896	0.00034		607 609	605 607	0.007453	0.06514	0.201481	0.054867	0.042392	2.266525	0.0414	0.049525	0.04557	0.003985	0.011677	0.000471
233 235	23	2 0.00470	8 0.04526	0.195757	0.039233 0.037269	0.037981 0.044621	1.691564 1.906113	0.034761 0.035732	0.049884	0.050363	0.003991 0.004416	0.011079 0.010843	0.000296		611 613	609 612	0.007357	0.065584	0.200544	0.053236	0.057968 0.061562	2.359729 2.381687	0.04199	0.048774 0.04921	0.042142 0.0421	0.002745 0.004017	0.012098	0.00051
237	23	7 0.003	5 0.043265 5 0.03455	0.151651	0.036563	0.041545	1.853367	0.035421	0.043779	0.042501	0.003893	0.009792	0.000313		615 617	614 617	0.007172 0.006919	0.061772 0.062193	0.207834 0.195872	0.053043 0.052817	0.083337	2.400696 2.378222	0.040192 0.040367	0.049244 0.048508	0.044772 0.043211	0.003285	0.011898	0.000452
267 269	24 24	1 0.00179	7 0.023562 6 0.045735	0.08944	0.021878	0.022048	0.976278	0.03108	0.038912	0.049928	0.005518	0.007778	0.0005		619 631	619 621	0.006805	0.061939	0.181406	0.051995	0.059057	2.362008	0.040388	0.047901	0.043755	0.002872	0.011779	0.000489
271 273	24 24	6 0.00246 9 0.0049	2 0.033463 3 0.04893	0.126356	0.03279	0.033843 0.060377	1.509011 1.950086	0.034872 0.034375	0.044114 0.047979	0.051592 0.050494	0.004726	0.011676 0.015002	0.000366		633 635	623 625	0.00481 0.00508	0.046222 0.048936	0.165715 0.182296	0.038584	0.036195 0.041876	1.777628 1.94657	0.036347	0.047138 0.047504	0.044443 0.042723	0.003881 0.0041	0.011103	0.000386
275 277	25 25	2 0.00522	5 0.050673 1 0.055738	0.166662	0.048147	0.051715 0.062447	1.871563 2.248271	0.036588 0.037186	0.046479 0.047253	0.057838 0.050784	0.00655	0.014735 0.014649	0.00047		637 639	628 630	0.002881 0.004024	0.028331 0.036833	0.135418 0.167418	0.024226 0.031699	0.027881 0.031847	1.214218 1.478168	0.034702 0.036919	0.044957 0.048476	0.044261 0.043771	0.004124 0.003446	0.008671	0.00017
279 281	25 26	7 0.00503 0 0.00463	1 0.05593 8 0.053252	0.156249	0.049854	0.049718	2.174358 2.097581	0.037967	0.045174	0.04741	0.005112	0.014542	0.000455		641 643	632 634	0.005232	0.050795	0.171319	0.04302	0.04373	1.946311 2.323169	0.039939	0.048966	0.044221	0.005176	0.01354	0.000221
283 285	26	3 0.00417 6 0.00447	9 0.0522	0.134425	0.046585	0.037976	2.124903 2.133111	0.038702 0.038591	0.044369 0.046011	0.044418 0.04544	0.005214 0.005872	0.012635 0.013467	0.000393		645 647	637 639	0.0029	0.051707	0.158898 0.148856	0.048575 0.051445	0.051142 0.051081	2.342085	0.041195 0.04129	0.047299 0.046836	0.043215	0.003485	0.011699	0.000254 0.000137
287 289	26	8 0.00531	8 0.05438 9 0.056636	0.162478	0.048017	0.039146	2.028293 2.303221	0.037366 0.038409	0.048884 0.048402	0.050616	0.005136	0.012422 0.01252	0.000411 0.000301		649 651	641 643	0.003357	0.053581 0.052391	0.151681 0.145426	0.050618	0.071355 0.034217	2.521093 2.249187	0.039181 0.039707	0.045031 0.044595	0.046501 0.04809	0.003569	0.011465	0.000107
291 293	27	4 0.0053 6 0.00552	5 0.058629 3 0.059847	0.169743	0.04868	0.045534	2.269989	0.040356	0.046597	0.043942	0.00381	0.011505	0.000375		653 655	645 648	0.003872	0.05476	0.164809	0.053306	0.03791	2.245284	0.040214	0.048077	0.049388	0.003769	0.011246	0.000107
295	27	9 0.0055	6 0.058819 1 0.057952	0.178698	0.049166	0.044989	2.265623	0.038585	0.046309	0.043477	0.003307	0.011031	0.000445		657	650	0.002725	0.039102	0.445842	0.038285	0.046898	1.962517	0.037444	0.048899	0.050456	0.003419	0.009573	0.000222
299 301	28	5 0.00514	3 0.053752	0.212509	0.047161	0.04211	2.013878	0.039098	0.047701 0.04841	0.047692	0.00322	0.010942	0.00029		661 663	654 657	0.004028	0.055045	0.197091	0.052735	0.074633	2.72927	0.038003	0.050473	0.048525	0.004395	0.010803	0.00019
303	29	0 0.00436	5 0.050410	0.265083	0.044098	0.034829	1.936139	0.03695	0.047909	0.046271	0.003918	0.010308	0.000233	_	665 667	659 661	0.00405	0.054491	0.207278	0.049592	0.048187	2.064542	0.038544	0.053086	0.048042	0.002972	0.010677	0.000126
307 309	29	5 0.00438	2 0.05104:	0.210017	0.044747	0.044207	2.096427	0.03725	0.046581	0.042474	0.004176	0.009499	0.000416	_	669 671	663 666	0.004426	0.053687	0.215274	0.046739	0.047195	2.038911	0.037835	0.05539	0.054945	0.003362	0.010213	0.000292
311 313	30	1 0.00415	1 0.05214	0.18334	0.045687	0.044973	2.205407	0.037243	0.046886	0.042028	0.003577	0.010191	0.000389		673 675	668 670	0.003666	0.057009	0.149998	0.05443	0.07193	2.381761	0.041496	0.047332	0.042278	0.004046	0.01239	0.000149
315 317	30	6 0.0041 9 0.00393	4 0.052792 4 0.051199	0.159175	0.046634	0.033965	2.134899	0.037825	0.045006	0.042156	0.004284	0.010078	0.000208		677 679	672 674	0.003824	0.055533	0.163457	0.056425	0.069616	2.469328	0.040259	0.047854	0.048597	0.004301	0.012029	0.000194
319 321	31	2 0.00362	7 0.045160 6 0.04157	0.221452	0.03936	0.038802	1.966498	0.036521	0.047429	0.04249	0.002757	0.009278	0.000207		681 683	677 679	0.003861	0.05577	0.163106	0.05368	0.043517	2.269444	0.040485	0.04773	0.050491 0.0516	0.004265	0.011367	0.000258
323 325	31	7 0.0036	3 0.04523	0.201255	0.038526	0.043699	1.96054	0.034878	0.048438	0.041721	0.002755	0.00949	0.00032		685 687	681 683	0.003622	0.055558	0.128429	0.05442	0.033779	2.096292	0.04057	0.04437	0.053032	0.003929	0.011718	0.00011
327 329	32	3 0.00365 5 0.00334	8 0.045065	0.220653	0.040211	0.05619	2.075638	0.034061	0.049147	0.037444	0.003899	0.008967	0.000393		689 691	686 688	0.004305	0.050033	0.204551	0.04408	0.057711 0.0529	1.995458 2.435336	0.035354	0.056074	0.049508	0.003071	0.009377	0.000181
331 333	33	8 0.00316	1 0.044452	0.203284	0.039447	0.039503	1.93254	0.034152	0.051049	0.046466	0.003091	0.009145	0.000196		693 695	690 692	0.003239	0.051875	0.102536	0.051767	0.066996	2.668062	0.039108	0.044664	0.045574	0.003788	0.011215	0.000199
335 337	33	4 0.00289 6 0.00464	9 0.035100 6 0.043703	0.164535	0.033451 0.039462	0.029216	1.618065 1.876758	0.031551 0.033731	0.049325 0.052974	0.046459 0.047332	0.0035	0.007231 0.008483	0.000215		697 699	695 697	0.003221 0.003225	0.0514	0.11727	0.051203 0.051677	0.05252	2.367479 2.43458	0.040919 0.03982	0.045585	0.044308	0.003472 0.00375	0.01136	0.000233
339 357	33	9 0.00491	5 0.045069 2 0.05144	0.22959	0.039379	0.037698	1.853006	0.035316	0.053314	0.0465	0.003794	0.009672	0.000343		701 703	699 701	0.003272 0.003163	0.050912	0.113498 0.124512	0.05179	0.037646	2.160622 2.33791	0.040429 0.041526	0.042834 0.045006	0.047234 0.044168	0.004024 0.003747	0.01114	0.000116
359 361	34 34	3 0.00614 6 0.00610	8 0.05441: 3 0.05319	0.202253	0.045956	0.038152 0.035382	2.093014 2.046219	0.035532 0.036443	0.048203 0.04501	0.042905 0.044255	0.003109 0.002962	0.010903 0.009346	0.000301 0.000421		705 707	703 706	0.003312 0.00311	0.053389 0.050737	0.155658 0.164178	0.050738 0.049106	0.051648 0.046775	2.335173 2.190373	0.041249 0.040008	0.047492 0.049443	0.045102 0.047982	0.004185 0.003649	0.011766 0.011187	0.000192 0.000144
363 365	34	8 0.00611 1 0.00586	7 0.054394 9 0.054698	0.208181	0.045829	0.038385 0.041464	2.147032 2.219632	0.035747 0.037575	0.046083 0.051004	0.041456 0.042678	0.003569 0.003867	0.010114 0.011567	0.000404 0.000293		709 711	708 710	0.002722 0.002722	0.053537 0.054545	0.128734 0.127649	0.051163 0.051678	0.051436 0.053758	2.418057 2.46496	0.041788 0.04197	0.046797 0.045294	0.043888 0.040882	0.004111 0.003689	0.011568 0.012658	0.000153 8.3E-05
367 369	35	3 0.00554 6 0.00571	6 0.0540 1 0.055713	0.136469	0.048468	0.043438 0.04564	2.326195 2.271703	0.037904 0.038174	0.046956 0.047322	0.041287 0.042596	0.003574 0.002592	0.010931 0.011369	0.000372 0.000272		713 715	712 715	0.003178 0.003783	0.059932 0.056186	0.163791 0.17879	0.055307 0.052519	0.062164 0.077994	2.61068 2.50128	0.043726 0.039755	0.046023 0.046193	0.04235	0.004305 0.004964	0.012926 0.012482	0.000118 0.000119
371 373	35 36	8 0.00604 1 0.00649	7 0.056356 1 0.055018	0.232629	0.04787	0.049508 0.043949	2.117058 1.973297	0.036656 0.036104	0.05152 0.051271	0.045378 0.045644	0.003403 0.002851	0.011466 0.01057	0.000259 0.000295		717 719	717 719	0.004388 0.007484	0.044794 0.057145	0.119969 0.174531	0.039558 0.048794	0.043364 0.051087	1.877545 2.075091	0.040046 0.04078	0.046543 0.050126	0.046299 0.047837	0.003036 0.00371	0.010425	0.000402 0.000528
375 377	36	3 0.00591 5 0.00658	6 0.057125 9 0.055476	0.189529	0.049005	0.045558 0.058437	2.121661 2.312465	0.036983 0.036321	0.050919 0.046129	0.042863 0.043816	0.00339 0.003403	0.011244 0.010329	0.000388 0.000351		737 739	721 723	0.005012 0.007964	0.043146 0.062313	0.173652 0.233358	0.038288 0.051	0.035092 0.076165	1.593198 2.344111	0.035642 0.039776	0.046696 0.050001	0.045328 0.043369	0.004067 0.003643	0.008666	0.000245 0.000576
379 381	36	8 0.00666 0 0.00654	3 0.056528 1 0.054919	0.15923	0.049773	0.03848 0.037337	2.207202 1.991923	0.036722 0.035683	0.046626 0.054195	0.044595 0.047938	0.00335	0.010833 0.010513	0.000322 0.000354		741 743	726 728	0.006935	0.05779	0.270814 0.240685	0.047542 0.04795	0.052401 0.05606	2.129286 2.057781	0.038036 0.039103	0.049323 0.048961	0.041106 0.041262	0.004869 0.005045	0.010989 0.012458	0.000219 0.000408
383 385	37	3 0.00676 5 0.006	1 0.051882 1 0.055058	0.24342	0.044709	0.040822 0.0459	1.980441 2.187119	0.035 0.0372	0.054956 0.050965	0.048653 0.043003	0.002822 0.003528	0.010143 0.012027	0.000385		745 747	731 733	0.008247 0.007473	0.065316 0.063293	0.207154 0.152625	0.05446 0.054953	0.056879 0.060172	2.305637 2.308946	0.040816 0.041542	0.049291 0.046833	0.043136 0.043972	0.004733 0.005693	0.013568 0.013848	0.000443 0.000508
387 389	37 38	8 0.00555 0 0.00670	3 0.05343: 6 0.053158	0.247461	0.044959	0.077411 0.05539	2.2619 1.952927	0.035552 0.037197	0.053121 0.053778	0.042208 0.044728	0.003273 0.003246	0.010843 0.010872	0.000282 0.000415		749 751	735 738	0.007213 0.007925	0.064817 0.064571	0.141809 0.191455	0.058573 0.0578	0.076733 0.057765	2.646999 2.300706	0.04244 0.042598	0.046899 0.049513	0.040011 0.04095	0.005109 0.004339	0.012893 0.013344	0.000419 0.000557
391 393	38 38	3 0.00643 5 0.00565	3 0.051735 5 0.047693	0.255658	0.042927	0.065667 0.044856	1.955924 1.786678	0.033725 0.034535	0.055817 0.054544	0.045705 0.044305	0.003472 0.003075	0.010235 0.009846	0.000358 0.000297		753 755	740 743	0.007603 0.007166	0.063008 0.063584	0.192495 0.183198	0.054406 0.054704	0.050351 0.068222	2.318309 2.530574	0.042486 0.041588	0.050216 0.047382	0.041211 0.040093	0.004225 0.00423	0.012414 0.011937	0.000521 0.000385
395 397	38	7 0.00550 0 0.00530	8 0.05561: 2 0.052212	0.202786	0.047421	0.049098 0.054857	2.157289 2.001506	0.03768 0.035169	0.050748 0.052035	0.04308 0.043791	0.003697 0.003393	0.010712 0.010769	0.000221 0.000267		757 759	745 747	0.007266 0.007517	0.062399 0.06428	0.178299 0.156964	0.055799 0.059777	0.072811 0.066203	2.482486 2.337966	0.041019 0.042516	0.046698 0.045942	0.039248 0.043454	0.00414 0.004217	0.012609 0.013525	0.000432 0.000523
399 401	39	2 0.00517 5 0.00500	2 0.052130 2 0.047135	0.219568	0.042327	0.039813 0.04691	2.058546 1.972471	0.036573 0.033274	0.049102 0.0529	0.041086 0.043732	0.003234 0.003584	0.010341 0.010603	0.000235 0.00031		761 763	750 752	0.007807 0.007159	0.06723	0.160451 0.19176	0.06086	0.048718 0.067807	2.391024 2.799709	0.043537 0.045338	0.046806	0.045539 0.033546	0.004764 0.004099	0.012856 0.012093	0.000435 0.000461
403 405	39 40	7 0.00411 0 0.00511	5 0.043854 5 0.049683	0.19862	0.039472	0.048009 0.045793	1.952996 2.040229	0.034445 0.036512	0.050747 0.050546	0.042474 0.041895	0.003833 0.003799	0.009762 0.010929	0.000253 0.000287		765 767	755 757	0.00765	0.072462 0.061423	0.168818 0.152852	0.054555 0.051338	0.048744 0.038498	2.503838 2.20958	0.045337 0.042815	0.045433 0.04617	0.038487 0.03931	0.003465 0.003579	0.012003 0.012239	0.000431 0.000445
407 409	40 40	2 0.00488 5 0.00590	3 0.047917 8 0.045788	0.272782	0.040727	0.077277 0.046951	2.153371 1.808467	0.034066 0.035025	0.056475 0.055467	0.038679 0.060397	0.003203 0.002871	0.010533 0.009798	0.000244 0.000304		769 771	759 762	0.006401 0.006718	0.062738 0.061401	0.215201 0.183645	0.049868 0.052316	0.073723 0.044189	2.520933 2.360954	0.041792 0.041258	0.052171 0.050647	0.036 0.037499	0.003755 0.004273	0.011701 0.012098	0.000299 0.000455
411 413	40 40	9 0.00549	5 U.045354	0.239381	0.039003	0.049819	1.860823	0.034356	0.055546	0.041596	0.002912	0.010378	0.000224		/73 775	764 767	0.006615	0.059128	0.238337	0.050574	0.07023	2.480954 2.451482	0.040933 0.039473	0.051677	0.036893	0.003904	0.011292	0.000348
415 417	41	2 0.00535 4 0.00550	9 U.U47252 5 0.049265	0.216219	0.041553	0.056654	1.96017	0.035988	0.052468	0.042779	0.002966	0.010605	0.000369		779	769 771	0.006745	0.057186	0.269392	0.0469 0.046886	0.05/141	2.1/U074 1.915111	0.040102	0.056661	0.035971	0.003168	0.011221	0.000338
419 421	41	9 0.00674	9 0.052034	0.237372	0.043492	0.053622	2.041709	0.03/251	0.04/892	0.043083	0.003426	0.011168	0.000315		781 783	776	0.006737	0.058208	0.239678	0.04621	0.055824	2.339004 2.181142	0.040404	0.055485	0.034392	0.00314	0.011479	0.000443
423	43	4 0.00647	o 0.052603 5 0.052943	0.228924	0.045628	0.047778	2.109326	0.036652	0.050184	0.045737	0.003027	0.011408	0.000261		787	781	0.007629	0.066883	0.262598	0.050149	0.04954/	2.32349/ 2.314393	0.040593	0.055848	0.036445	0.003586	0.011997	0.000483
42/ 429	43	9 0.00822	6 0.06042	0.194657	0.053213	0.051913	2.795288	0.030341	0.051662	0.044342	0.003838	0.011153	0.000376		791	786	0.007467	0.054863	0.204421	0.049633	0.06839	2.451331	0.039416	0.053573	0.037075	0.003064	0.012202	0.000436
453	43	4 0.00243	6 0.022143	0.1068/8	0.021617	0.020865	1.375094	0.031329	0.041/54	0.052438	0.002018	0.006521	0.000279		793 795	791	0.007224	0.06257	0.241094	0.05154	0.057491	2.312811	0.040942	0.058209	0.03726	0.003835	0.012905	0.000314
457 459 Ac1	43	9 0.0028	7 0.034055 7 0.037623	0.185191	0.033293	0.036562	1.871509	0.035531	0.04761	0.045993	0.002910	0.009828	0.000212		799 801	793 795 799	0.007176	0.062565	0.237392	0.051183	0.040839	2.255607	0.040894	0.054525	0.03983	0.004379	0.012409	0.000410
463	44	4 0.0025	6 0.03306	0.151002	0.035643	0.031111	1.549826	0.033084	0.049999	0.055994	0.002545	0.008613	0.000283		803	800	0.007834	0.070428	0.251871	0.054992	0.03909	2.358852	0.043252	0.056362	0.037767	0.003841	0.011733	0.000539
467	44	9 0.00304	6 0.035315 8 0.03232	0.161835	0.03294	0.032283	1.531051	0.032606	0.0474	0.052387	0.003813	0.008121	0.000234		807	805 807	0.008718	0.06368	0.267946	0.053753	0.06591	2.402204	0.039817	0.056061	0.042437	0.004298	0.011989	0.000479
471	49	4 0.00236	9 0.034123	0.179882	0.033055	0.049009	1.722095	0.03223	0.047723	0.043348	0.003147	0.009137	0.000232		811	810	0.009181	0.055885	0.330244	0.046273	0.052974	1.85898	0.036257	0.063625	0.04766	0.004088	0.011098	0.000458
475	45	9 0.00181	8 0.031393 6 0.03090	0.169077	0.030767	0.08172	1.747327	0.032356	0.047	0.04175	0.00314	0.008186	0.000168		815	815	0.009047	0.06148	0.330276	0.048457	0.050528	2.061585	0.036271	0.058886	0.041894	0.004577	0.015149	0.000423
479	46	5 0.00149	4 0.027067	0.136505	0.028847	0.03922	1.477465	0.032868	0.042492	0.044319	0.003198	0.008783	0.000164	_	819	819	0.006477	0.05333	0.167933	0.047245	0.056338	2.089301	0.036411	0.045868	0.047268	0.003505	0.010516	0.000201
483	47	0 0.00197	5 0.032568	0.133882	0.033591	0.044242	1.836048 1.821808	0.034543	0.044424	0.04407	0.002328	0.008589	0.00016		823 825	823	0.005957	0.051351	0.235237	0.044269	0.052458	2.013875	0.034424	0.054448	0.043364	0.003328	0.010294	0.000353
487	47	5 0.00254	6 0.03238	0.147868	0.033648	0.035374	1.651799	0.034289	0.046132	0.048702	0.00282	0.009004	0.000221		827	827	0.006617	0.053789	0.404387	0.043771	0.04898	2.00262	0.034246	0.069705	0.042882	0.002983	0.009895 0.008175	0.000373
491	48	0 0.00269	9 0.03876	0.151637	0.037771	0.049686	1.894144	0.035879	0.044848	0.045464	0.003666	0.010455	0.000138		831 833	831 833	0.006841	0.057558	0.300915	0.047642	0.039609	1.836755	0.037588	0.061345	0.048762 0.038841	0.004083	0.010421	0.000295
495	48	5 0.0035	2 0.043044	0.145874	0.04071	0.062914	2.106777	0.035003	0.042478	0.044622	0.003765	0.00978	0.000423		835 837	835 837	0.006479	0.052917	0.503996	0.039687	0.051514	1.858582	0.032367	0.080483	0.041609	0.002984	0.009849	0.000256
499	49	0 0.00359	1 0.046258	0.193741	0.041625	0.043888	1.966444	0.036341	0.050249	0.048927	0.00354	0.009714	0.000381		839 841	839 841	0.006976	0.049074	0.417582	0.035836	0.049863	1.788097	0.030407	0.067656	0.040993	0.003112	0.008657	0.000284
503	49	5 0.00375	9 0.050029	0.203465	0.044823	0.06835	2.397613	0.035737	0.049621	0.044734	0.004268	0.00962	0.000218		843 845	843 845	0.007283	0.054146	0.371387	0.043952	0.040812	1.775632	0.035005	0.066351	0.050729	0.003151	0.010457	0.000301
507	-+: 50 50	1 0.00353	6 0.050179 1 0.049514	0.17232	0.046217	0.057126	2.23808	0.038952	0.044627	0.045039	0.003984	0.010891 0.011087	0.000301		847 849	847 849	0.007475	0.056643	0.399551	0.043886	0.038514	1.832444	0.034389	0.068279	0.044344	0.003648	0.010414	0.00042
511 513	50	6 0.00291	4 0.04681	0.156238	0.044615	0.047566	2.139168	0.039607	0.045955 0.0473R4	0.046796	0.003962	0.011237	0.000167															
515 517	51	1 0.00267	9 0.03971	0.151133	0.039759	0.040391	1.86745	0.036006	0.045771 0.04715	0.045016	0.003654	0.009763	0.000277															
519 521	51	6 0.00298 9 0.00286	4 0.04668 7 0.04319	0.161419	0.044339	0.076026	2.357035	0.036582	0.045647	0.047424	0.0035	0.010849 0.01102	0.000186															
523 525	52	1 0.00236	8 0.039113 3 0.032829	0.141959	0.04087	0.050252 0.036141	1.971985 1.671128	0.037641 0.035006	0.046034 0.047119	0.050371 0.050998	0.004891 0.002723	0.010426 0.009133	0.000252															
527	52	6 0.00212	1 0.032992	0.158759	0.034046	0.055899	1.767259	0.034113	0.05043	0.052435	0.003028	0.009837	0.000138															

Appendix 2

Appendix 12 Geological map of the Rhine catchment

Geological map of the Rhine catchment. After Van Andel, 1950



Appendix 13 Distributive regions of the Rhine catchment

Map of the distributive regions of mineral assemblages of the Rhine catchment. After Van Andel, 1950

